

CISM Summer School, Udine Italy, June 22-26 2009.
Electrokinetics and Electrohydrodynamics of Microsystems

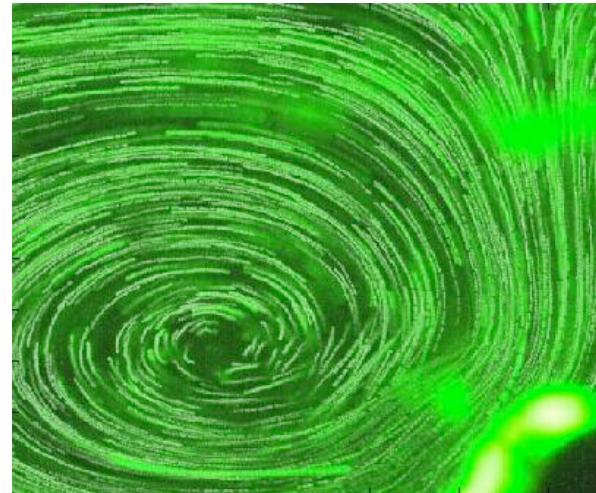
Induced-Charge Electrokinetic Phenomena

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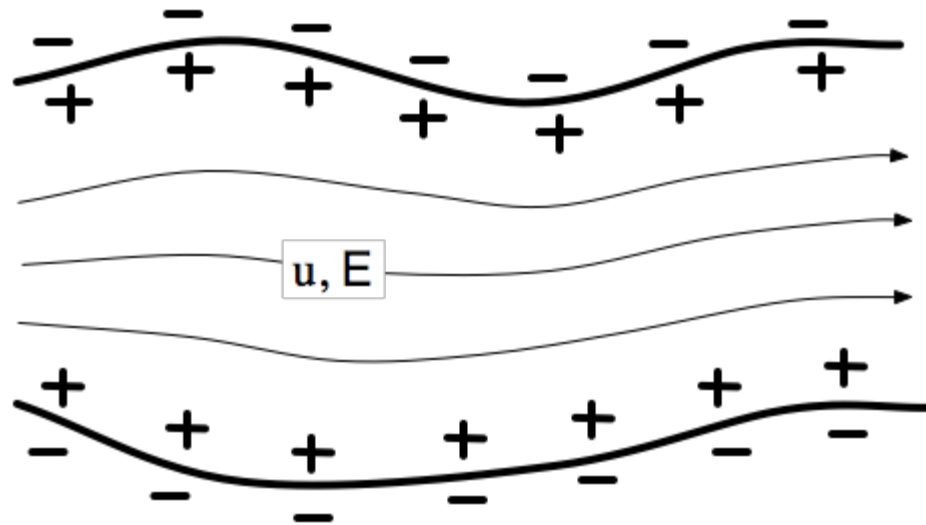
Lectures

1. Introduction
2. Low-voltage theory
3. Particle motion
4. Fluid motion
5. Large-voltage theory



Linear (DC) Electrokinetic Microfluidics

Electro-osmosis



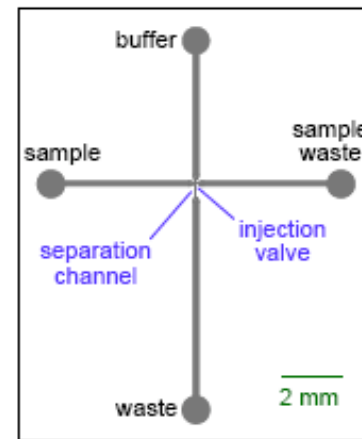
Slip: $\vec{u}_s = -\mu_e \vec{E}_t, \quad \mu_e = \frac{\varepsilon \zeta}{\eta}$

Potential / plug flow for uniformly charged walls:

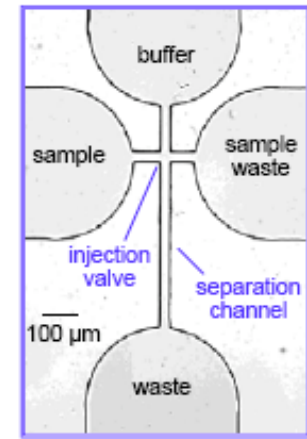
$$\vec{u} = \mu_e \nabla \phi, \quad \nabla^2 \phi = 0$$

Electro-osmotic Labs-on-a-Chip

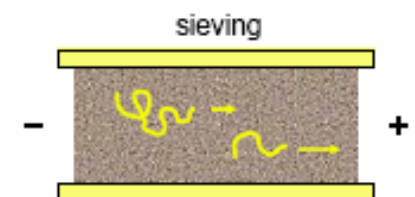
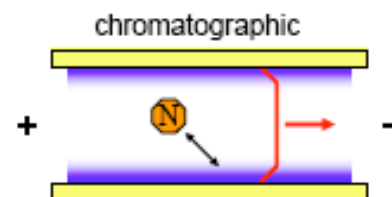
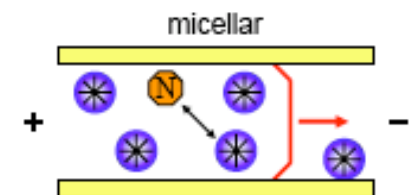
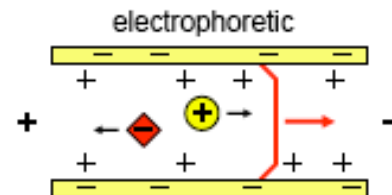
- Apply E across chip
- Advantages
 - EO plug flow has low hydrodynamic dispersion
 - Standard uses of in separation/detection
- Limitations:
 - High voltage (kV)
 - No local flow control
 - “Chip in a Lab”



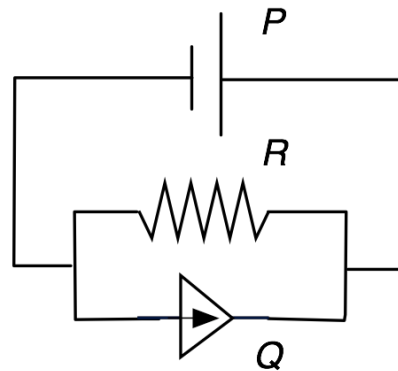
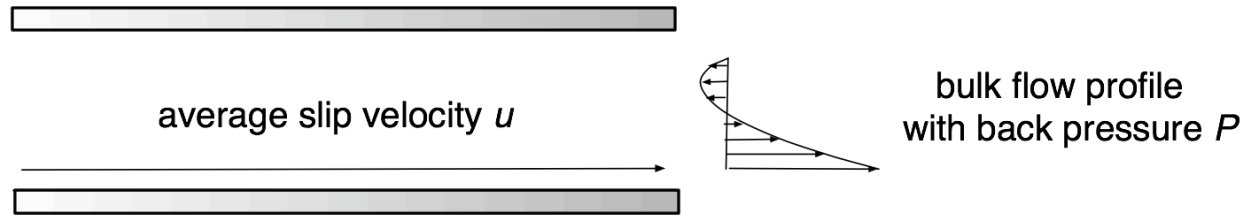
Anal. Chem. 70, 3476-3480, 1998.



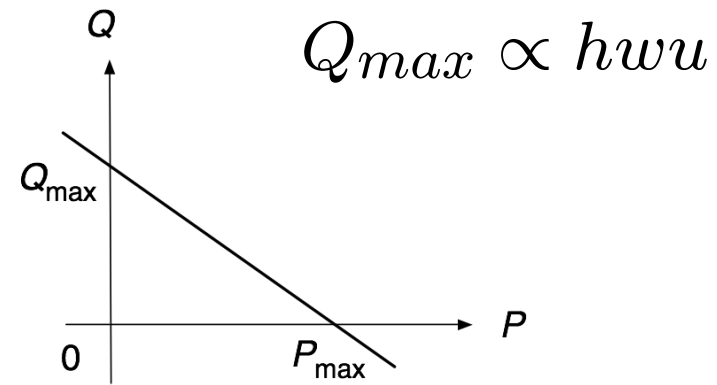
separation channel: 500 μm
narrow channel: 26 μm
wide channel: 440 μm



Pressure generation by slip



equivalent circuit



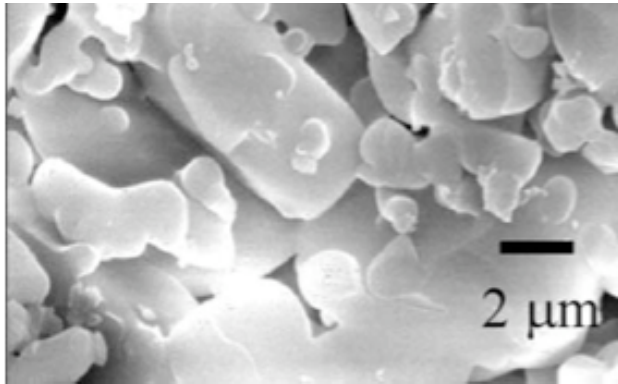
flow rate versus back pressure

$$P_{\max} = R_H Q_{\max} \propto \frac{\eta u L}{h^2}$$

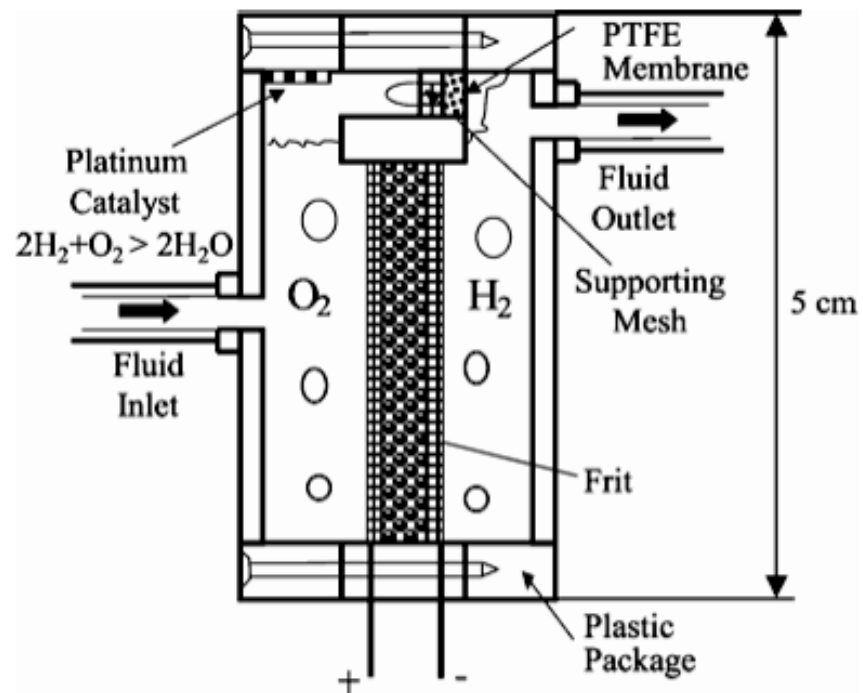
Use small channels!

DC Electro-osmotic Pumps

- Nanochannels or porous media can produce large pressures (0.1-50 atm)
- Disadvantages:
 - High voltage (100 V)
 - Faradaic reactions
 - Gas management
 - Hard to miniaturize



Porous
Glass



Yau et al, JCIS (2003)
Juan Santiago's group at Stanford

Electro-osmotic mixing

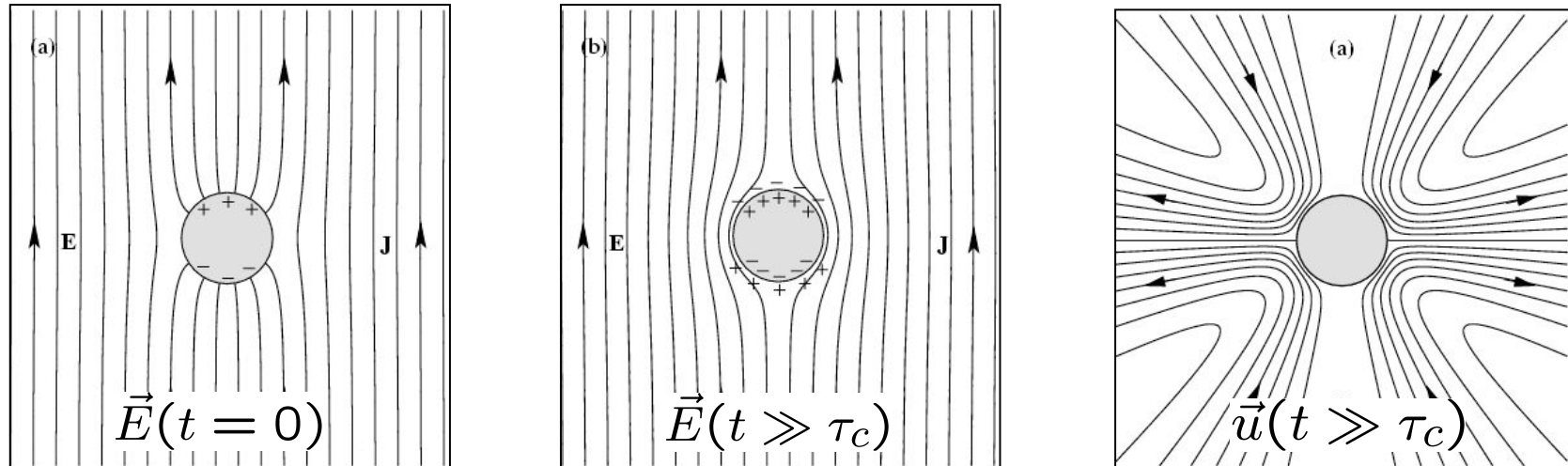
- Non-uniform zeta produces vorticity
- Patterned charge + grooves can also drive transverse flows (Ajdari 2001) which allow lower voltage across a channel
- BUT
 - Must sustain direct current
 - Flow is set by geometry, not “tunable”

Induced-Charge Electro-osmotic Microfluidic Devices

Microfluidic Applications of Induced-Charge Electro-osmosis

Bazant & Squires, Phys, Rev. Lett. (2004)

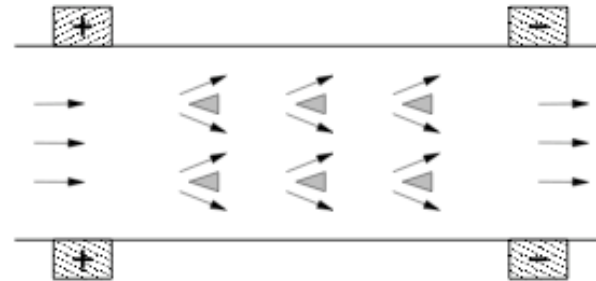
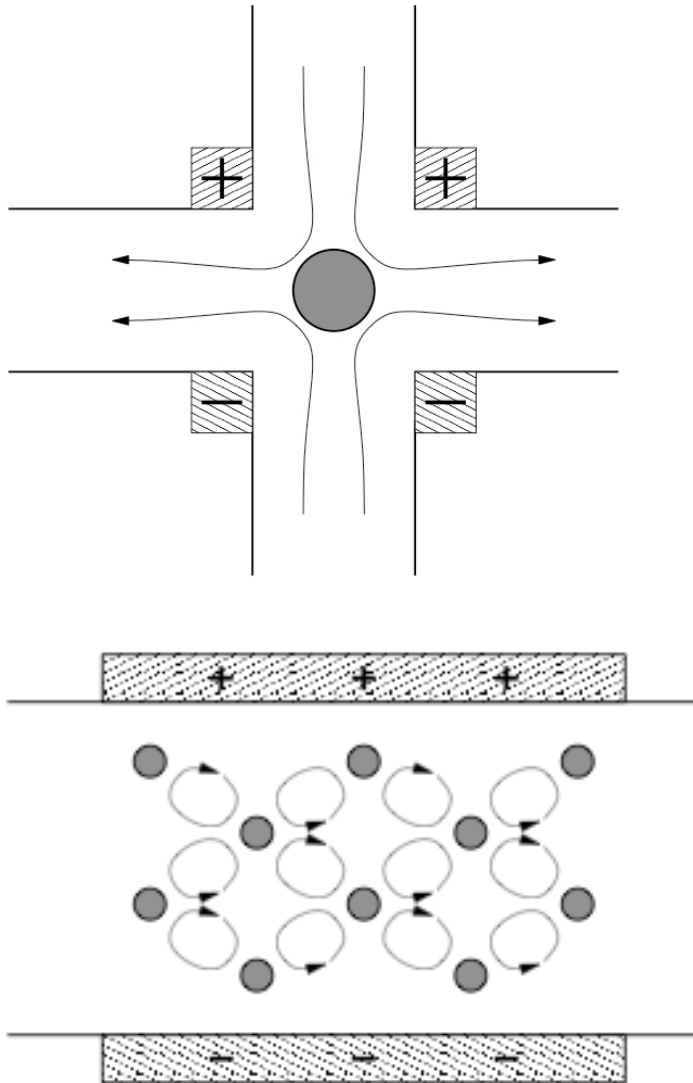
Example: An uncharged metal cylinder in a DC (or AC) field



$$u_s = \frac{\varepsilon \zeta}{\eta} E_t, \quad \zeta - \zeta_0 \sim ER \Rightarrow u \sim \frac{\varepsilon R E^2}{\eta}$$

Can control local vorticity and pressure with low AC voltages.

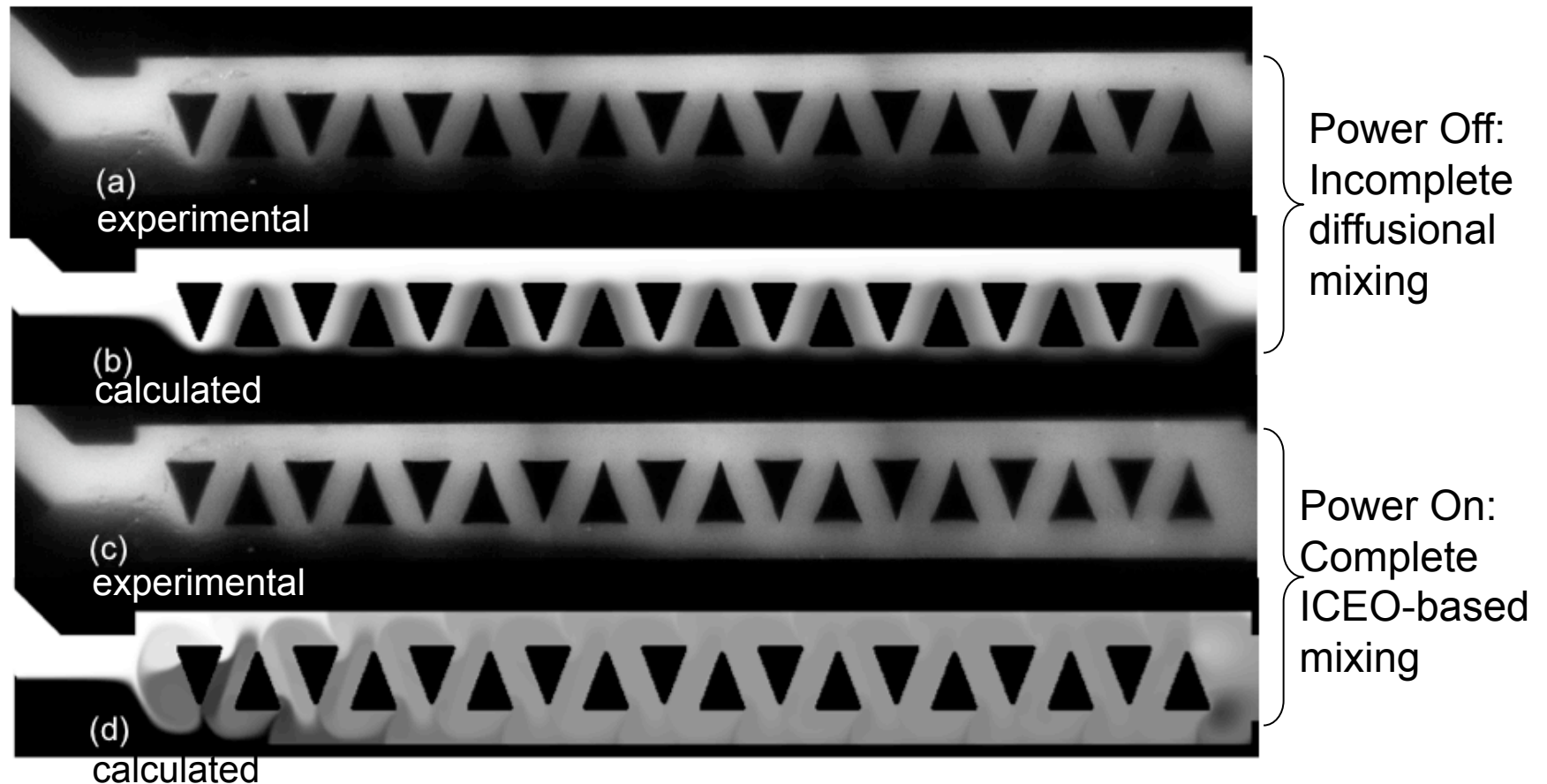
ICEO Mixers, Switches, Pumps...



- Advantages
 - tunable flow control
 - 0.1 mm/sec slip
 - low voltage (few V)
- Disadvantages
 - small pressure ($< \text{Pa}$)
 - low salt concentration

ICEO-based microfluidic mixing

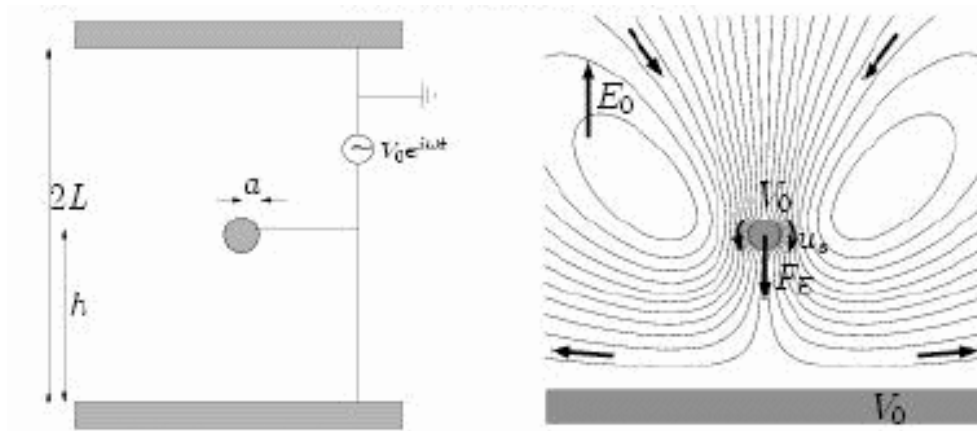
C. K. Harnett et al. Lab on a Chip (2008)



Comparison of experimental (a,c) and calculated (b,d) results during steady flow of dyed and un-dyed solutions ($2 \mu\text{l}/\text{min}$ combined flow rate) without power (a,b) and with power (c,d). Flow is from left to right. $10 V_{pp}$, 37 Hz square wave applied across $200 \mu\text{m}$ wide channel. Left-right transit time $\sim 2 \text{ s}$.

“Fixed-Potential ICEO” / AC “Flow FET”

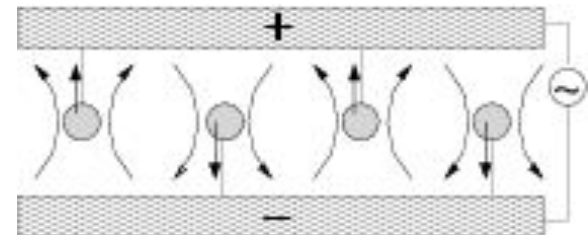
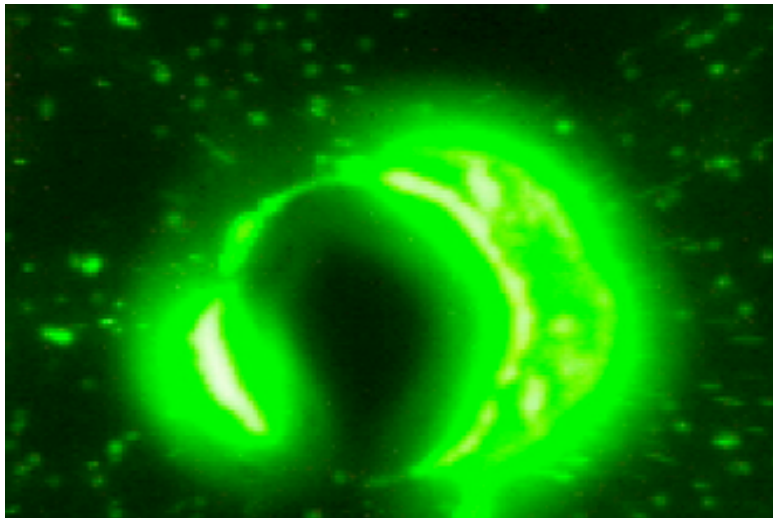
Squires & Bazant, J. Fluid Mech. (2004)



Idea: **Vary the induced total charge in phase with the local field.**

Generalizes “flow field-effect transistor”
Ghowri & Gale, J. Chromatogr. (1991)

Example: metal cylinder grounded to an electrode supplying an AC field.



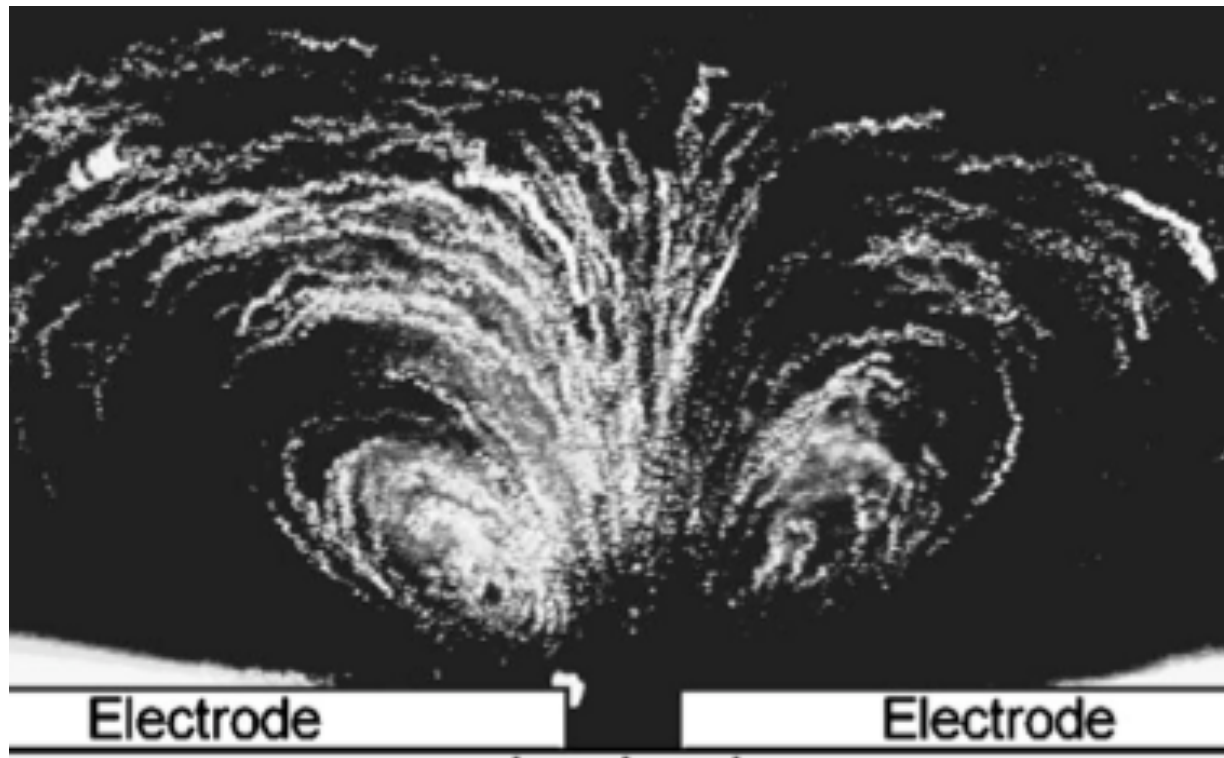
Fixed-potential ICEO mixer

Flow past a 20 micron electroplated gold post
(J. Levitan, PhD Thesis 2005)

AC Electro-osmotic Electrode-array Micropumps

AC electro-osmosis

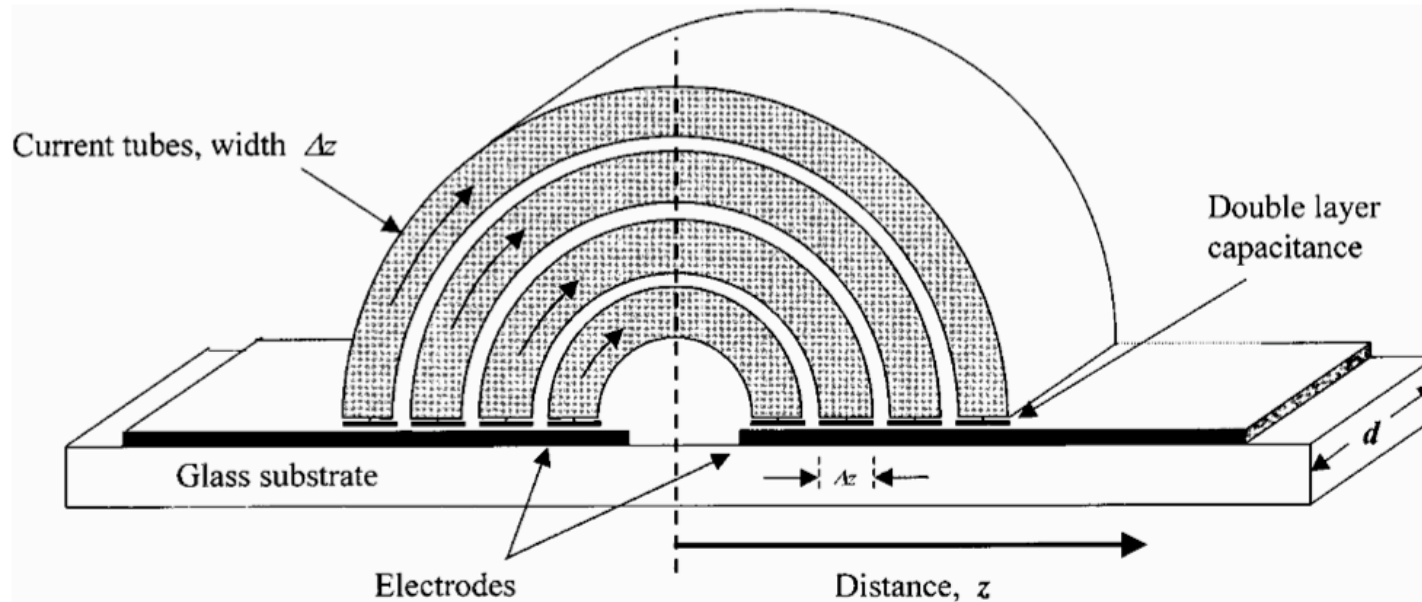
A. Ramos, A. Gonzalez, A. Castellanos (Sevilla), N. Green, H. Morgan (Southampton), 1999.



$$u \propto \frac{\epsilon V^2}{\eta L} \left[(\omega \tau)^2 + (\omega \tau)^{-2} \right]^{-1}$$

Circuit model

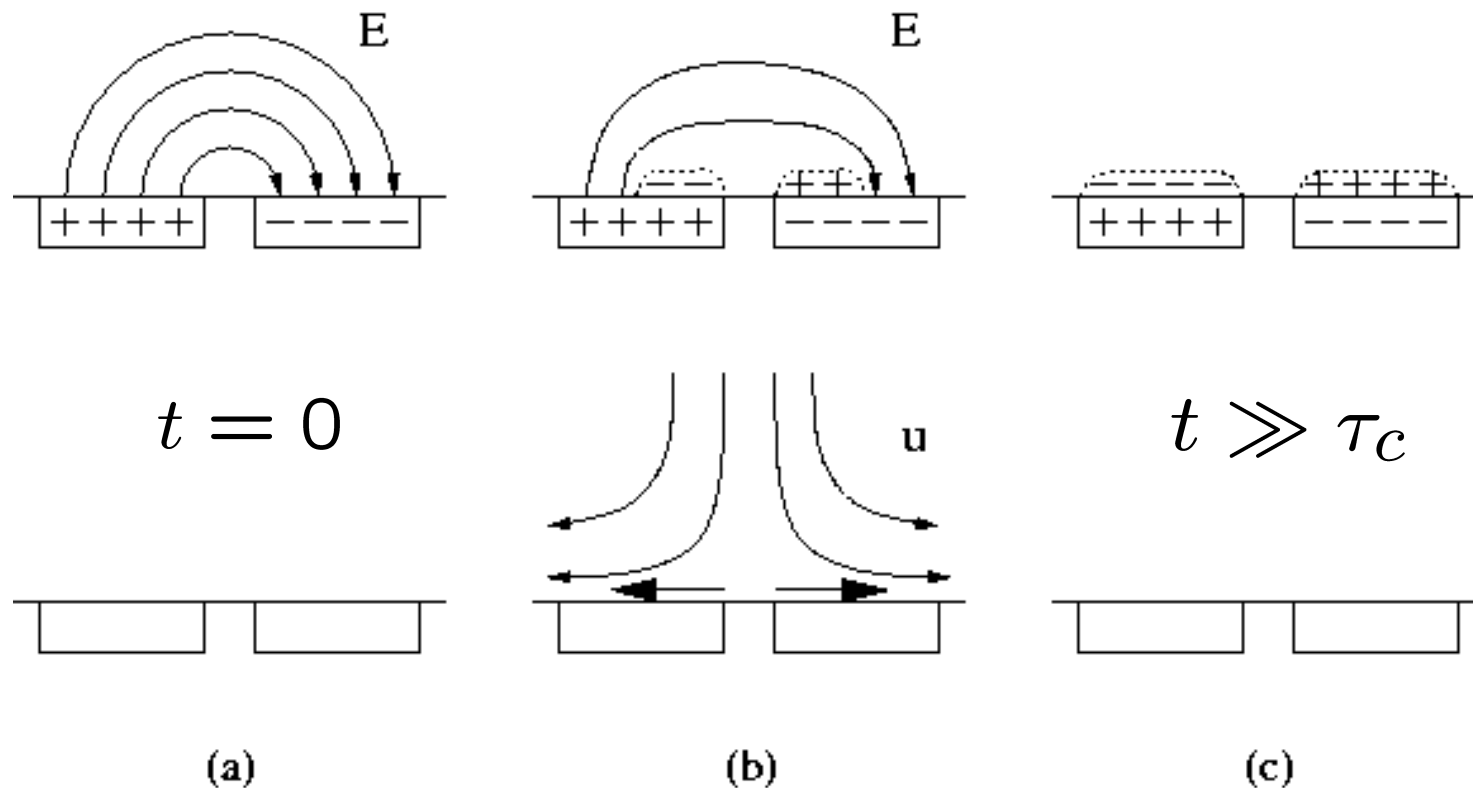
Ramos et al. (1999)



“RC time”
$$\tau(r) = \frac{2\pi r \varepsilon}{\sigma \lambda} \propto \frac{\lambda r}{D} = \tau_D \frac{r}{\lambda}$$

Debye time:
$$\tau_D = \frac{\varepsilon}{\sigma} = \frac{\lambda^2}{D}$$

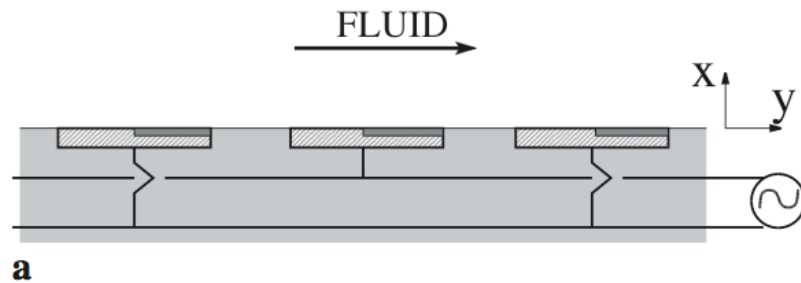
Flows induced over electrodes



- Example: “ICEO” flow in response to a sudden DC voltage
- With AC voltage, flow peaks if period = charging time
- ACEO maximizes flow/voltage due to large local field

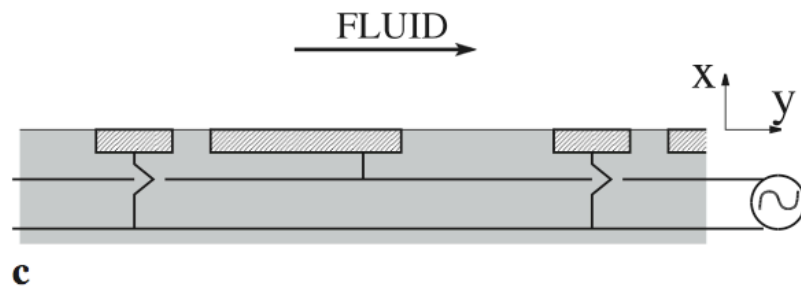
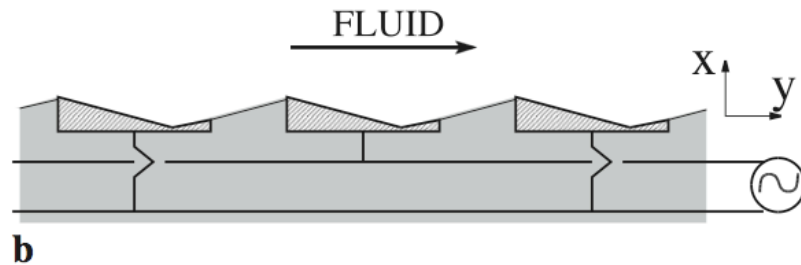
AC electro-osmotic pumps

Ajdari (2000)



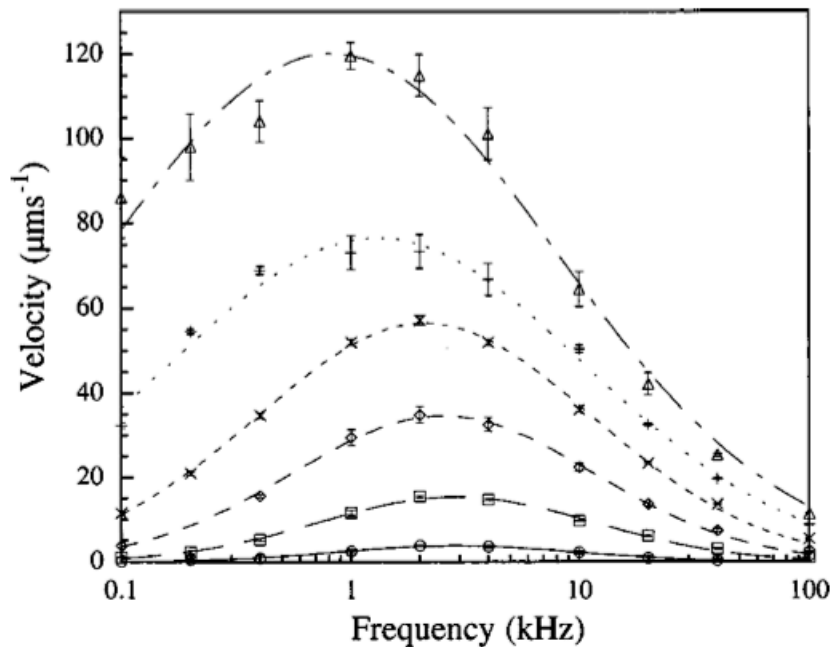
“Ratchet” concept inspired by molecular motors:

Broken local symmetry in a periodic structure with “shaking” causes pumping without a global gradient.

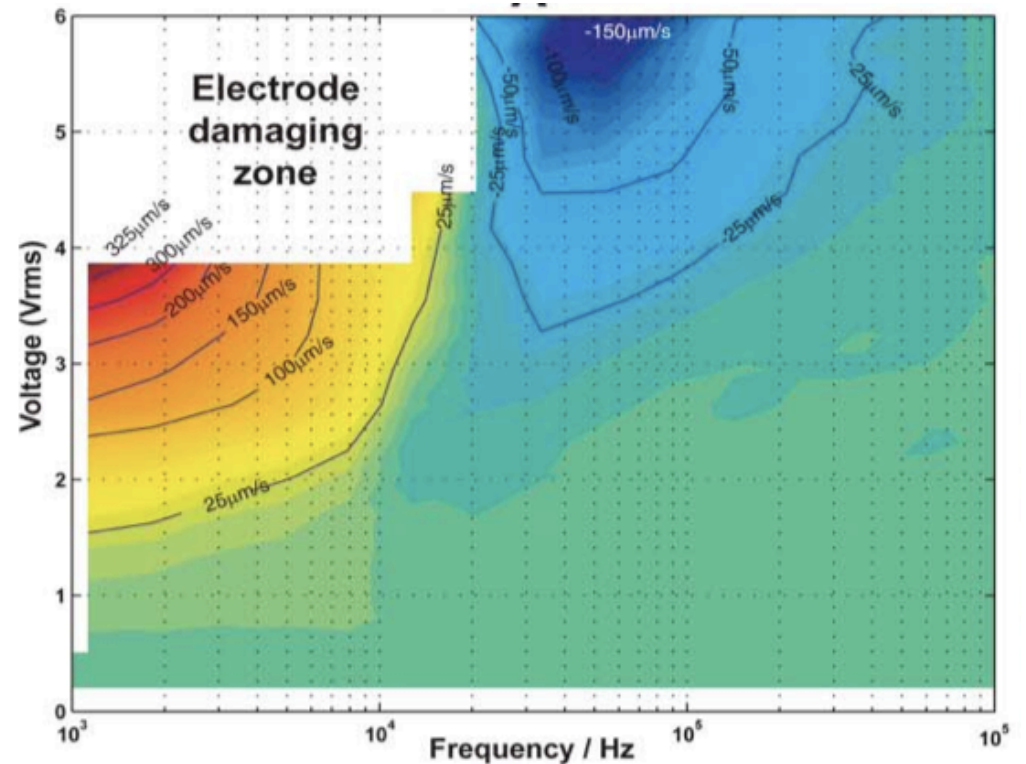


Brown, Smith, Rennie (2001): asymmetric planar electrodes

ACEO Experiments



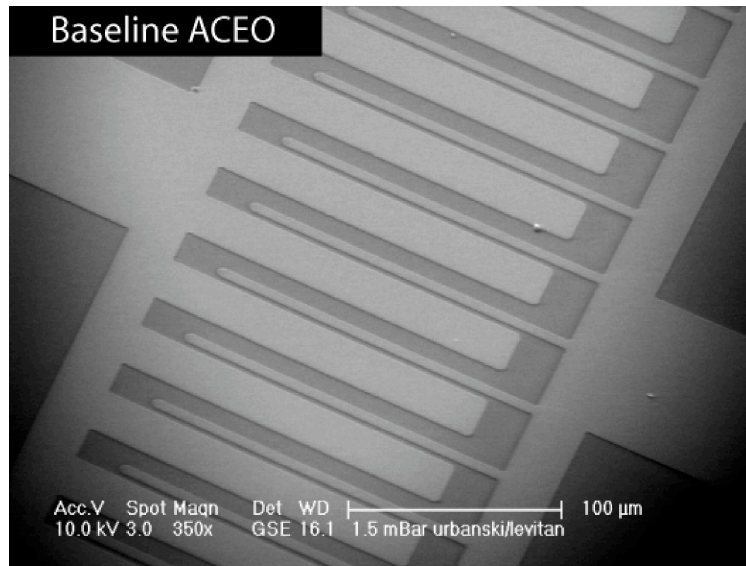
- Brown et al (2001), water
- straight channel
 - planar electrode array
 - similar to theory (0.2-1.2 V_{rms})



- Vincent Studer et al (2004), KCl
- microfluidic loop, same array
 - flow reversal at large V , freq
 - no flow for $C > 10\text{mM}$

More data for planar pumps

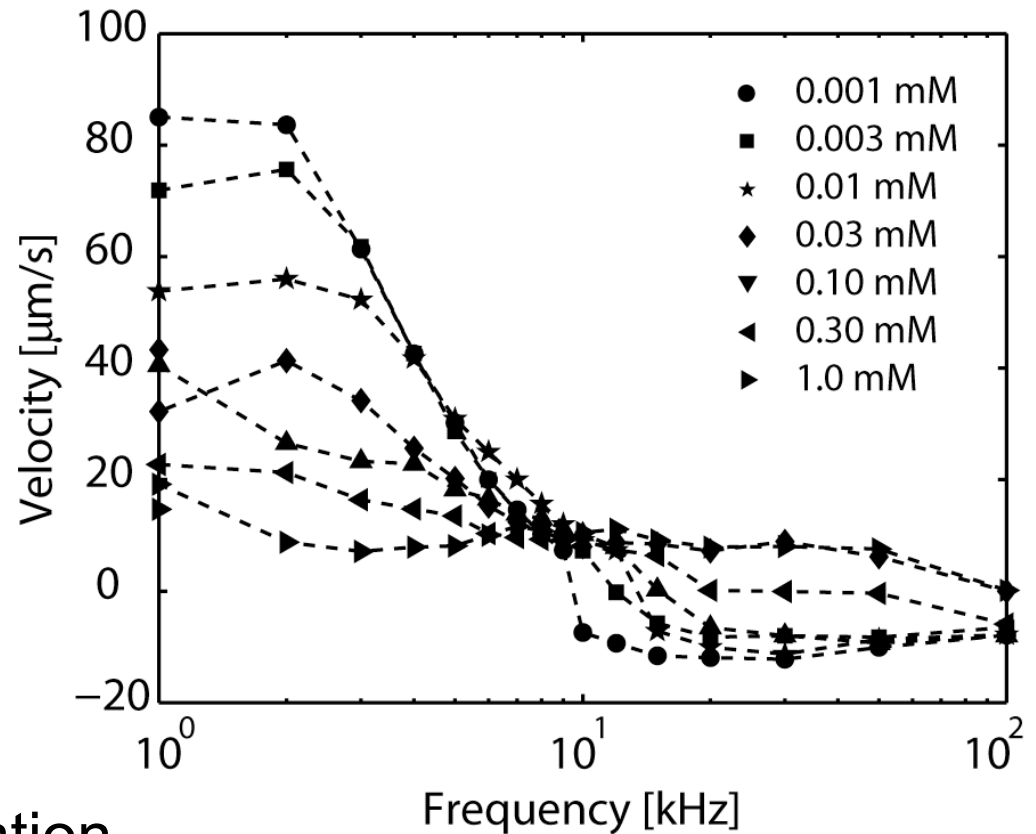
Urbanski et Appl Phys Lett (2006); Bazant et al, MicroTAS (2007)



Puzzling features

- flow reversal
- decay with salt concentration
- ion specific

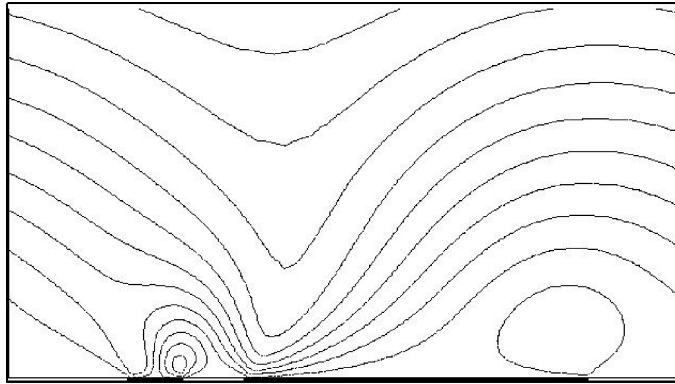
Can we improve performance?



KCl, 3 Vpp, loop chip 5x load

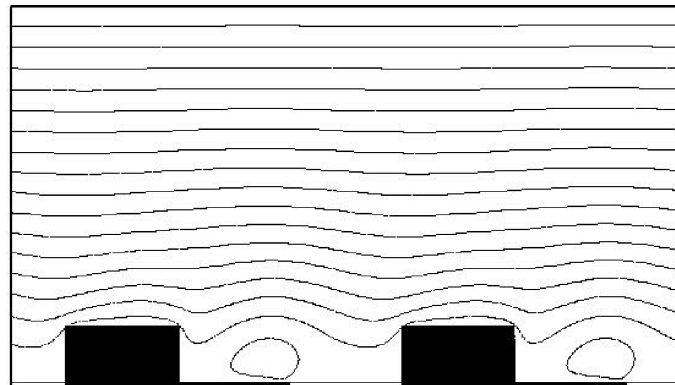
Fast, robust “3D” ACEO pumps

Bazant & Ben, Lab on a Chip (2006); Burch & Bazant, Phys Rev E (2008)

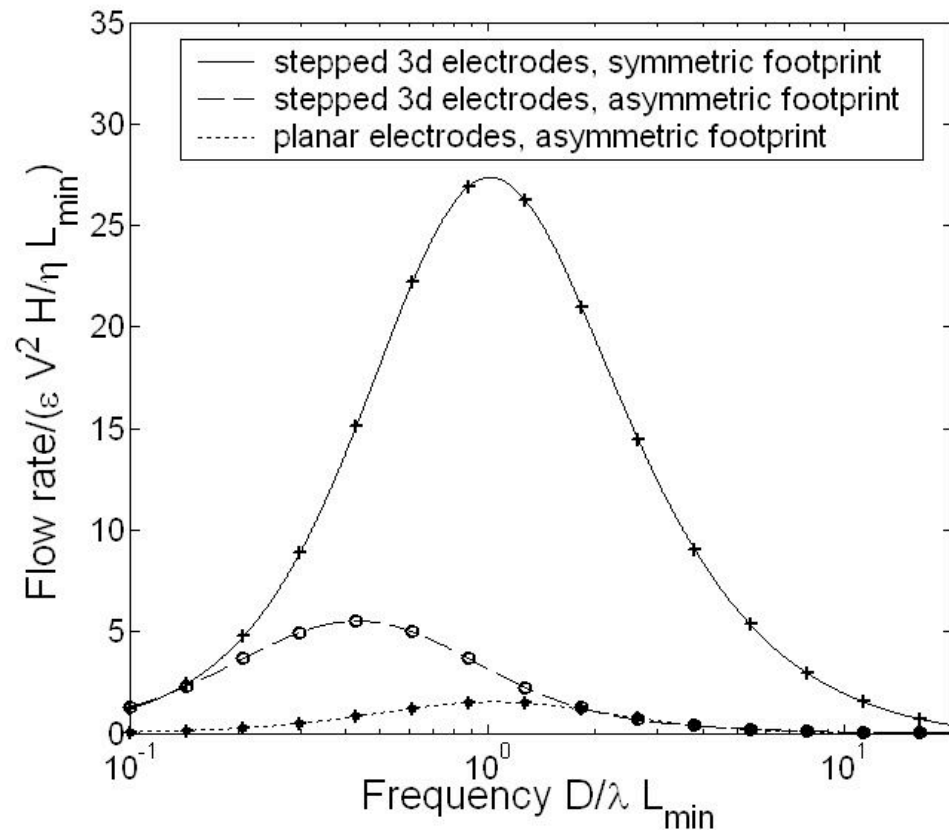


Fastest planar ACEO pump

Brown, Smith & Rennie (2001). Studer (2004)

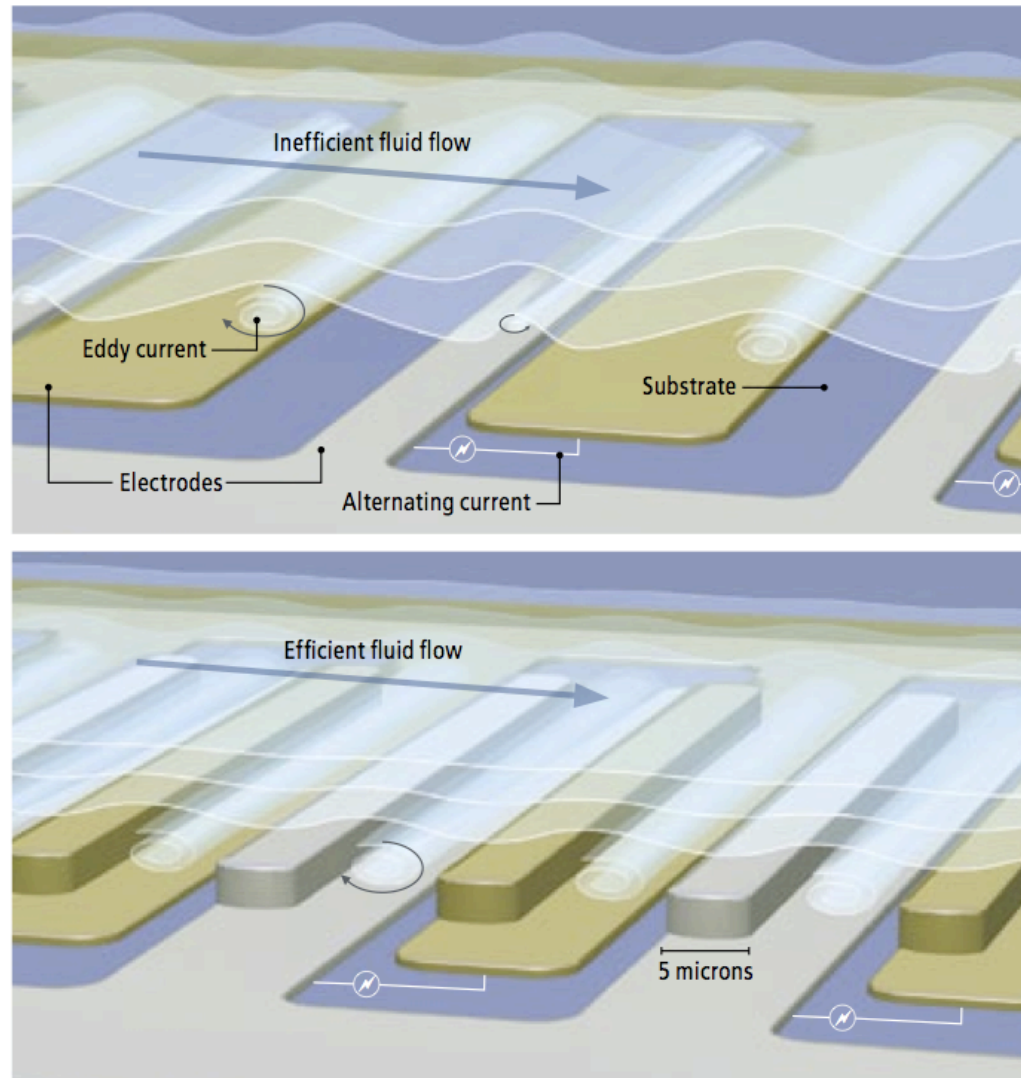


New design: electrode steps create a “fluid conveyor belt”



Theory: “3D” design is 20x faster ($>mm/sec$ at $1 V_{rms}$) and should not reverse

The ACEO “Fluid Conveyor Belt”



CQ Choi, "Big Lab on a Tiny Chip", *Scientific American*, Oct. 2007.

High-pressure ACEO pumps

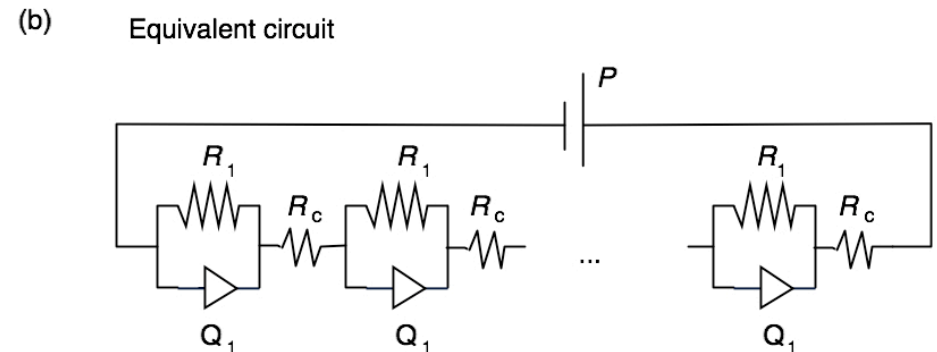
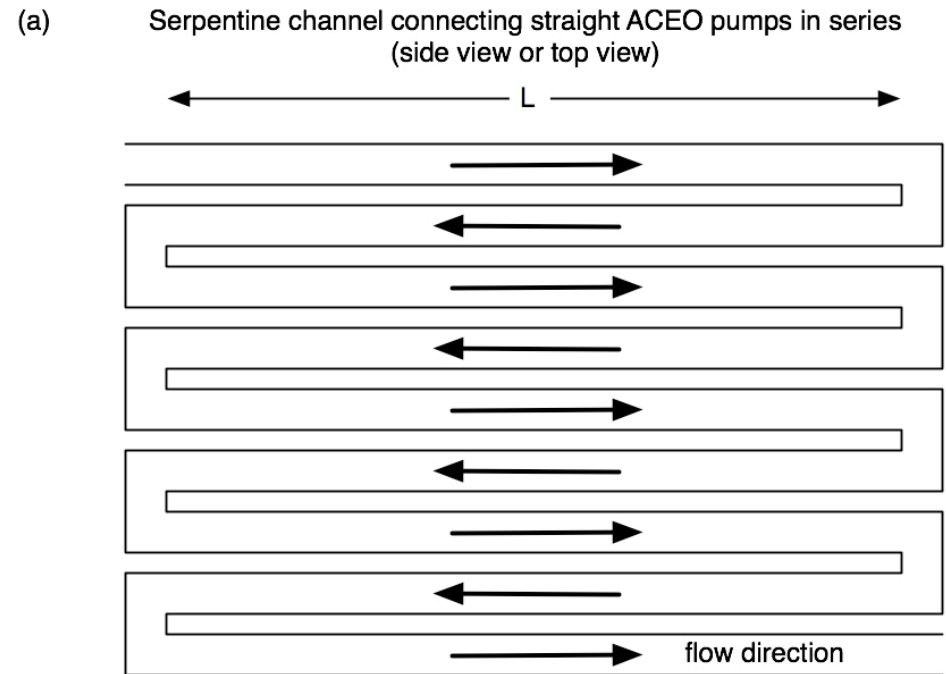
$$P_{max} = R_H Q_{max} \propto \frac{\eta u L}{h^2}$$

Need $h > \text{micron}$ BUT with **serpentine channels**

$L = 10\text{m}$ is possible in mL chip volume, so $P = \text{atm}$ is possible at few volts AC!

In a fixed device volume, sacrifice Q for P

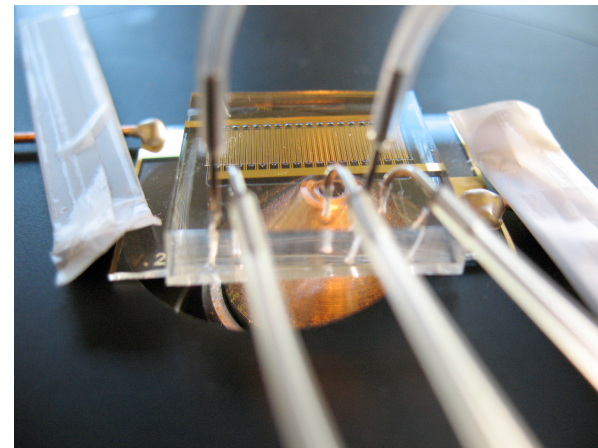
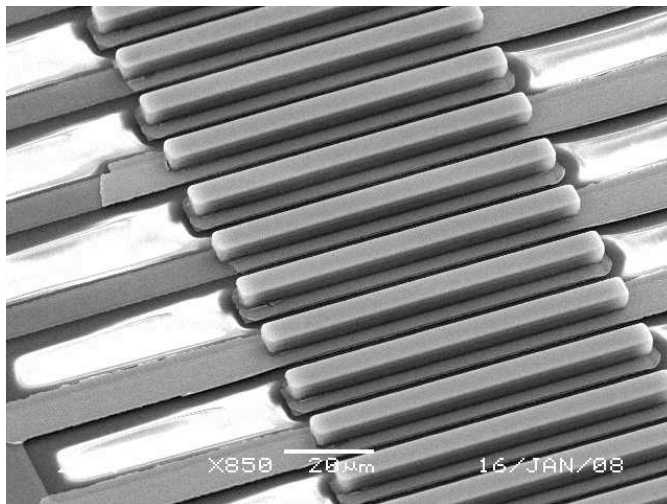
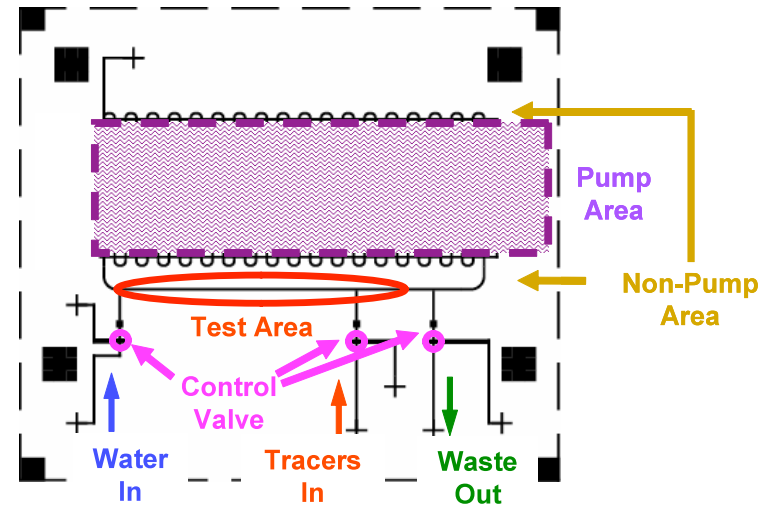
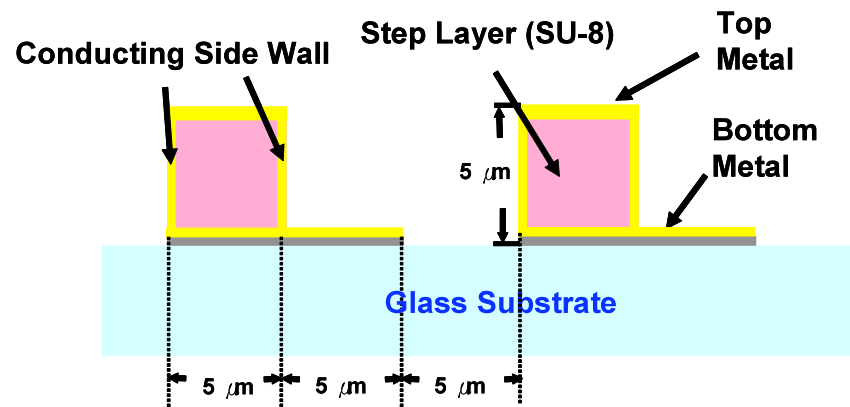
$$P_{max} Q_{max} \propto \frac{u^2 V}{h^2}$$



High-Pressure Ultrafast ACEO Pumps

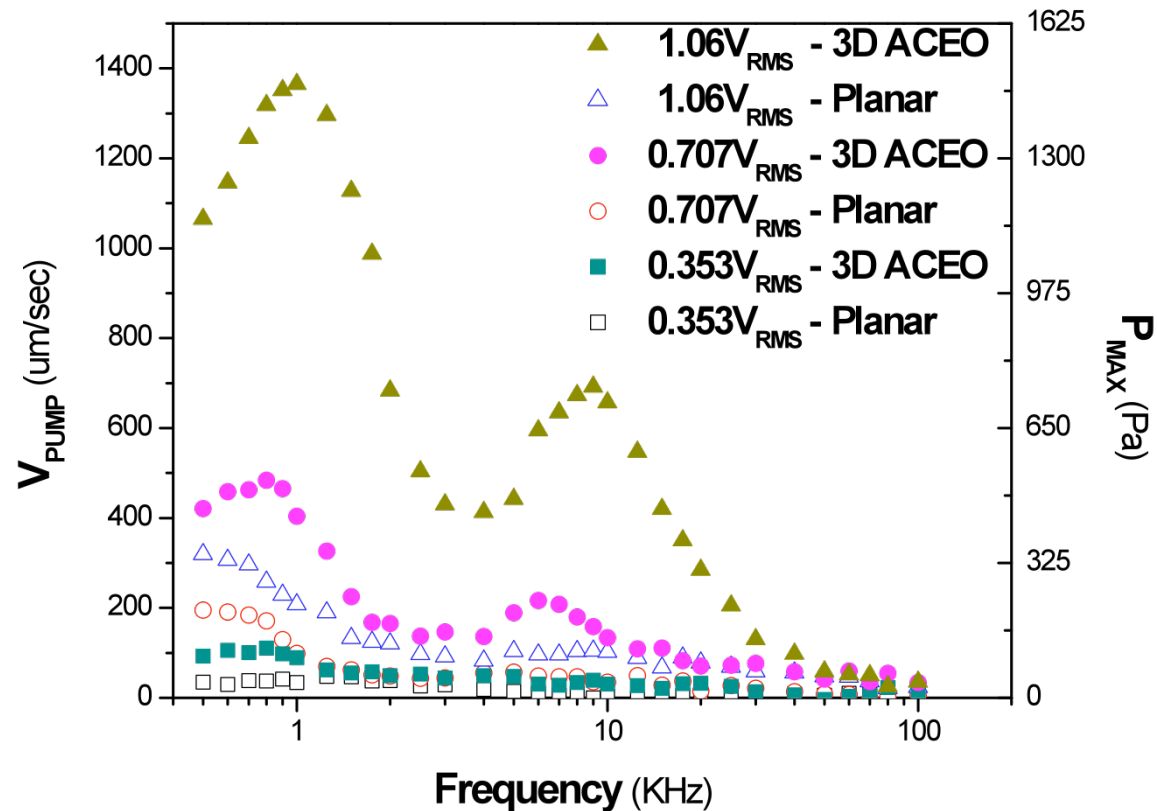
JP Urbanski, JA Levitan, MZB & T Thorsen, Appl. Phys. Lett. (2006)

CC Huang, MZB & T Thorsen, submitted (2009)



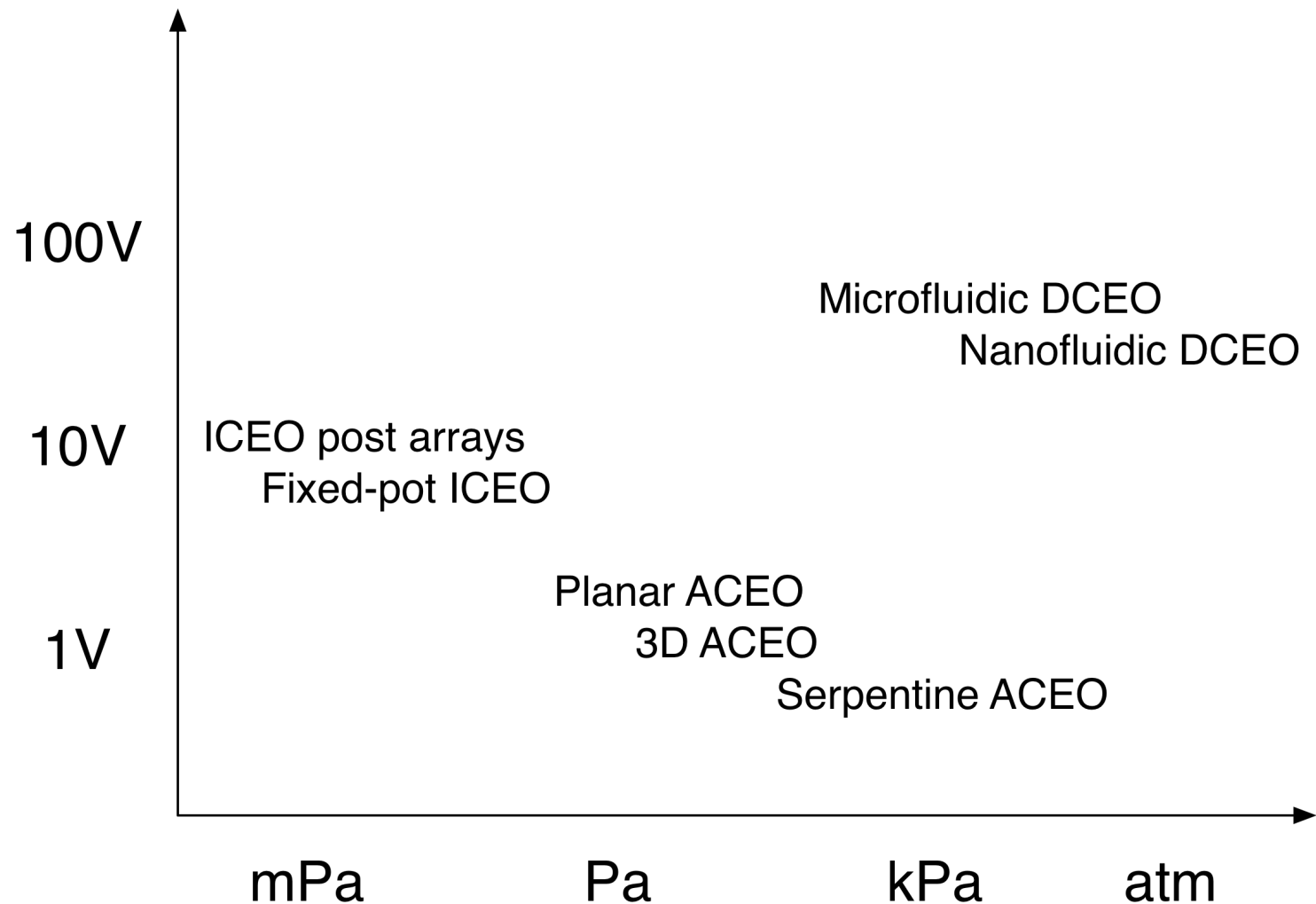
3D ACEO pumping of water

CC Huang, MZB & T Thorsen, submitted (2009)

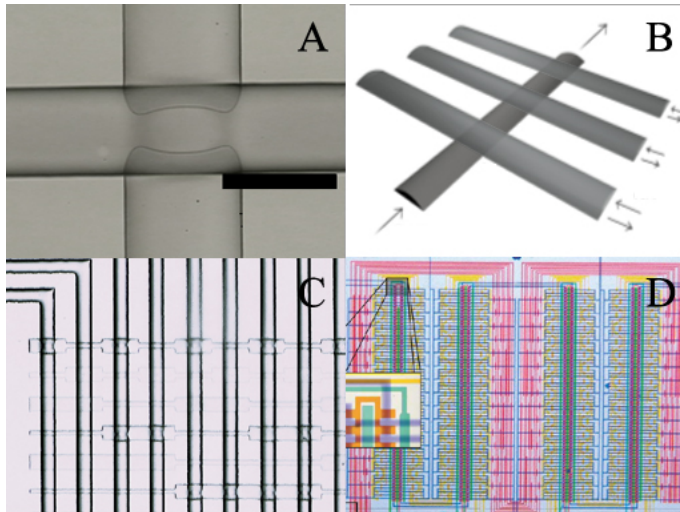


- mm/sec velocity, $> 1\%$ atm pressure at 1 Volt rms
- 5 mW power consumption, 3.5 mA current
- Can run for days on small Li-ion battery
- Demonstrated portable DNA microarray chip

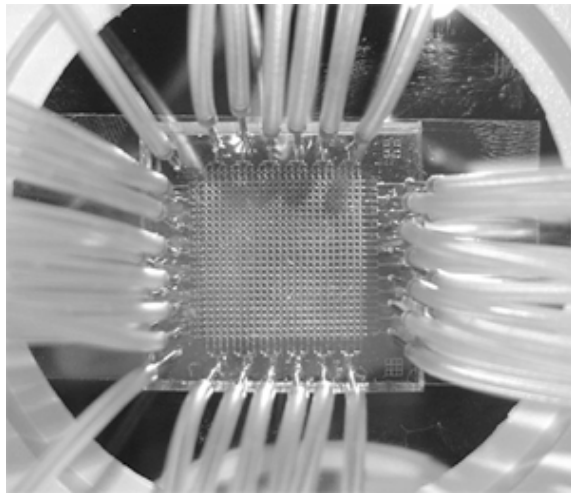
AC vs. DC Electro-osmotic Pumps



A platform for *portable* microfluidics?



<http://www.physics.ubc.ca/~chansen/>



Fluidigm Topaz System

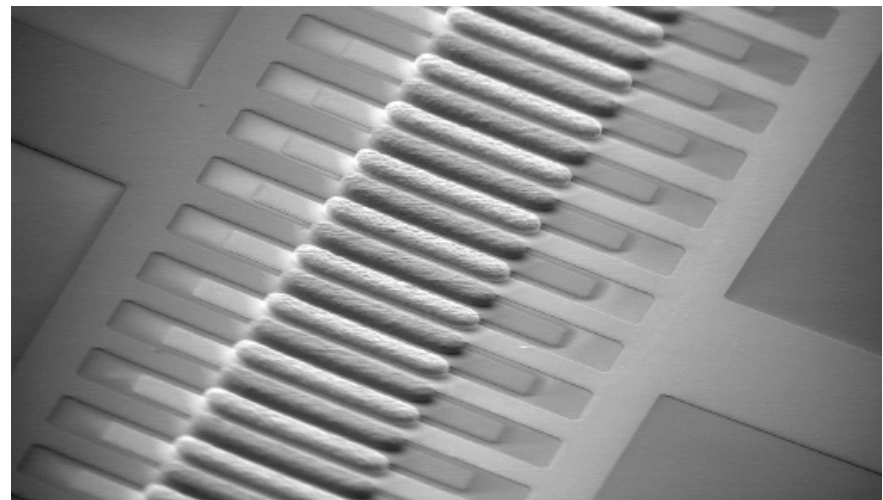
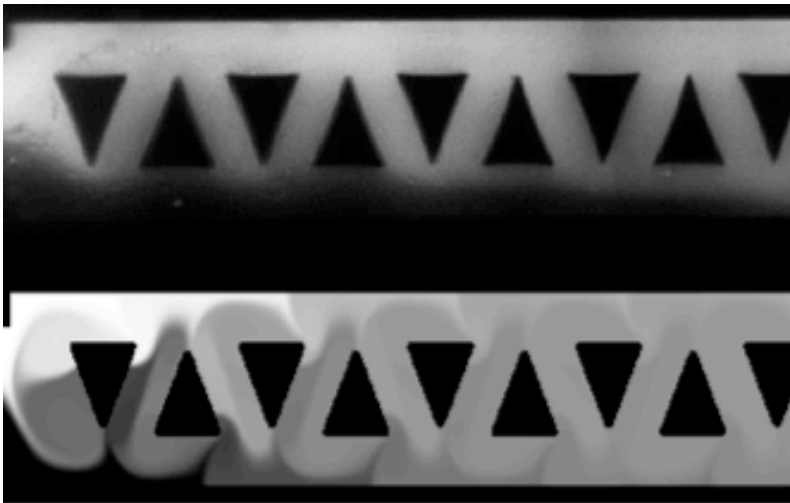
Thorsen/Quake LSI

- elastomeric valves
- 1000s of channels
- pressure-driven flows
- “Chip in a Lab”

Can we replace external plumbing with low-voltage ACEO pumps, mixers, switches, etc.?

Conclusion

- Induced-charge AC electro-osmotic flows enable local manipulation of particles and fluids in portable microfluidic devices
- ... but limited to dilute electrolytes
- Why? Lecture 5...



Papers, slides... <http://web.mit.edu/bazant/www/ICEO>