Degenerate four-wave mixing in triply resonant Kerr cavities

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We demonstrate theoretical conditions for highly efficient degenerate four-wave mixing in triply resonant nonlinear (Kerr) cavities. We employ a general and accurate temporal coupled-mode analysis in which the interaction of light in arbitrary microcavities is expressed in terms of a set of coupling coefficients that we rigorously derive from the full Maxwell equations. Using the coupled-mode theory, we show that light consisting of an input signal of frequency $\omega_0 - \Delta \omega$ can, in the presence of pump light at $\omega_p$, be converted with quantum-limited efficiency into an output shifted signal of frequency $\omega_0 + \Delta \omega$, and we derive expressions for the critical input powers at which this occurs. We find the critical powers in the order of 10 mW, assuming very conservative cavity parameters (modal volumes $\sim 10$ cubic wavelengths and quality factors $\sim 1000$). The standard Manley-Rowe efficiency limits are obtained from the solution of the classical coupled-mode equations, although we also derive them from simple photon-counting “quantum” arguments. Finally, using a linear stability analysis, we demonstrate that maximal conversion efficiency can be retained even in the presence of self- and cross-phase modulation effects that generally act to disrupt the resonance condition.

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I. INTRODUCTION

For many years, researchers have used confinement of light for a long time in a small volume (resonant cavities) to enhance light-matter interactions such as optical nonlinearities, recently entering the integrated-optics regime of smaller and smaller cavities with limited sets of interacting modes. In such systems, careful design is required to maximize the efficiency and minimize the power of a given nonlinear process such as frequency conversion [1–17], and the use of cavities can also lead to qualitatively new phenomena such as bi- or multistability [1,3,18–31]. While the use of cavities is known to enhance nonlinear effects, every distinct nonlinear process requires a new analysis. In this paper, we consider the problem of intracavity degenerate four-wave mixing (DFWM): an electromagnetic cavity resonant at three frequencies $\omega_0$ and $\omega_0 \pm \Delta \omega$, in which a third-order ($\chi^{(3)}$) nonlinearity converts an input signal at $\omega_0 - \Delta \omega$ to an output shifted signal at $\omega_0 + \Delta \omega$ in the presence of an input pump at $\omega_p$. The small-$\Delta \omega$ regime corresponds, for example, to conversion between different channels in wavelength-division multiplexing (WDM), which is similar to recent experimental studies of nonlinear frequency conversion in cavities [32–40].

It allows one to exploit structures such as ring resonators [3] or photonic-crystal cavities [41] that support closely spaced resonances; in Sec. IV A, we show that this regime supports stable quantum-limited conversion at low signal powers for a critical pump power. Conversely, we show that the $\Delta \omega > \omega_p$ regime generalizes our previous work on intracavity third-harmonic generation (THG) [1,2]; in Sec. IV B, we show that this regime supports stable conversion with 100% efficiency at a critical pump and signal power. For example, with a typical nonlinear material such as gallium arsenide (GaAs) and reasonable cavity parameters (volume $\sim 10$ cubic wavelengths and quality factors $\sim 1000$), we obtain critical powers in the milliwatts (on the order of 10 mW) for both $\Delta \omega$ regimes. The standard Manley-Rowe efficiency limits are considered from both a simple photon-counting “quantum” argument [42,43] and are also derived from purely classical coupled-mode equations [44,45] (Sec. III), where the latter also yield stability information, critical powers, and other dynamics (Secs. IV A and IV B). The coupling coefficients in these equations are derived explicitly from the full Maxwell equations for arbitrary microcavities (Sec. II). We also show that the nonlinear dynamics leads to additional phenomena, such as multistability and limit-cycle (self-pulsing) solutions, similar to phenomena that were previously shown for other nonlinear systems [1,18,46,47] (Secs. IV A and IV B). Finally, in Sec. IV C, we consider the effects of self- and cross-phase modulation (SPM and XPM), which induce nonlinear shifts in the cavity frequencies; these must be compensated by preshifting the resonances and they also affect the stability analysis (as we previously found for THG [1]).

Although nonlinear effects in electromagnetism are weak, it is well known that confining light in a small volume and/or for a long time, as in a waveguide or cavity, can both enhance the strength and modify the nature of nonlinear phenomena [48,49]. Much previous work in nonlinear frequency conversion has studied $\chi^{(2)}$ processes (where there is a change in the susceptibility that is proportional to the square of the electric field) such as second-harmonic generation (SHG) [2,4,17,46,50–59], sum/difference-frequency generation (SFG/DFG) [5,6,60–63], and optical parametric amplification (OPA) [64–66]. Studies of SHG in doubly resonant $\chi^{(2)}$ cavities have demonstrated that 100% conversion efficiency is achieved at critical pump power, much lower than for SHG in singly resonant cavities [2,4,17,51–56,58,67–69]. Recent studies of DFG in triply resonant $\chi^{(2)}$ cavities also showed the existence of a critical relationship between pump and idler power that results in optimal quantum-limited conversion [61], with potential applications to terahertz generation [7,8]. The existence of quantum-limited frequency conversion can be
predicted from the Manley-Rowe relations, which govern the rates of energy transfer in nonlinear systems [48]. There has also been some recent work on intracavity \( \chi^{(3)} \) third-harmonic generation [1]. (In a \( \chi^{(3)} \) medium, there is a change in the refractive index proportional to the square of the electric field.)

As in SHG, THG in doubly resonant cavities has been shown to support solutions with 100% conversion efficiency, even when taking into account nonlinear frequency shifting due to SPM and XPM, as well as interesting dynamical behavior such as multistability and limit cycles (self-pulsing) [1], with lower power requirements compared to singly resonant cavities or nonresonant structures [9,50,59,66,70–82]. Limit cycles have been observed in a number of other nonlinear optical systems, including doubly resonant \( \chi^{(2)} \) cavities [46,83], bistable multimode Kerr cavities with time-delayed nonlinearities [84], nonresonant distributed feedback in Bragg gratings [19], and a number of nonlinear lasing devices [85].

In what follows, we extend the previous work on SHG, DFG, and THG in resonant cavities to the case of DFWM in \( \chi^{(3)} \) media. Four-wave mixing is characterized by taking input light at frequencies \( \omega_1, \omega_2, \) and \( \omega_3 \) and producing light at frequency \( \omega_4 = \pm \omega_1 \pm \omega_2 \pm \omega_3; \) degenerate four-wave mixing, however, is restricted to the case where \( \omega_1 = \omega_2 \) to generate \( 2\omega_1 - \omega_2. \) Previous work has studied FWM in the context of optical fibers [86–90], photonic crystal waveguides [91,92], and even matter waves [93], and has demonstrated the use of FWM in applications such as phase conjugation [65,94–96] and generation of two-photon coherent states [86,97,98]. While there has been recent experimental work on intracavity FWM in \( \chi^{(3)} \) media (degenerate or otherwise) [32–40,99–101], we are not aware of any detailed studies of the underlying theoretical phenomena in general cavities. As we shall see DFWM in triply resonant cavities shares many qualitative features with SHG, DFG, and THG, including the existence of critical powers at which optimal conversion efficiency is achieved as well as interesting nonlinear phenomena such as limit cycles and multistability. As in DFG, and unlike SHG or THG, there exist Manley-Rowe limitations on the overall conversion efficiency. In Sec. III, we discuss the corresponding relations governing four-wave mixing and illustrate their implications for conversion efficiency. These relations can be obtained classically through temporal coupled-mode theory [44,45], but they are more easily motivated and understood from a quantum perspective [42,43]. Such arguments have been employed before in the context of lasing [102,103], RF circuits [104], and other nonlinear optics phenomena [48]. In the case of intracavity frequency conversion, we show how both perspectives yield limits on conversion efficiency.

Several different approaches can be used to study nonlinear optical systems. Most directly, brute-force numerical simulations by a variety of methods, such as finite-difference time-domain (FDTD) [41,105], offer the most general and flexible technique, in that they can characterize phenomena involving many degrees of freedom and going beyond the perturbative regime; however, such simulations are relatively slow and allow one to study only a single geometry and excitation at a time. More abstract analyses are possible in many problems because confinement to a waveguide or cavity limits the degrees of freedom to the amplitudes of a small set of normal modes, combined with the fact that optical nonlinearities are typically weak (so that they can be treated as small perturbations to the linear modes). For example, many nonlinear phenomena have been studied in the context of co-propagating plane waves, in which the amplitudes of the waves can be shown to satisfy a set of simple ordinary differential equations (ODEs) in space (the slowly varying envelope approximation) [48]. More generally, however, it can be shown that all nonlinear problems coupling a finite set of modes and satisfying certain fundamental principles such as conservation of energy, regardless of the underlying wave equation (e.g. electromagnetic or acoustic waves), can be described by a universal set of ODEs characterized by a small number of coefficients, determined by the specific geometry and physics. This approach, which has come to be known as temporal coupled-mode theory (TCMT), dates back several decades [44,106] and has been applied to a number of problems, including microwave transmission systems [104], active media microphonic structures [107], and the nonlinear intracavity problems mentioned above [1,2,61,106]. Likewise, we employ TCMT in this paper to characterize the most general possible behavior of intracavity DFWM systems, regardless of the nature of the cavity. As reviewed elsewhere [44], TCMT begins with the purely linear system and breaks it into abstract components such as input and output channels (e.g. waveguides or external losses) and cavities, characterized by resonant frequencies and coupling rates that depend on the geometry. It then turns out that the ODEs describing such a system are completely determined by those parameters once the constraints of conservation of energy, linearity, time-invariance, and reciprocity (or time-reversal invariance) are included, under the key assumption that coupling rates are slow compared to the frequencies (i.e., strong confinement) [41,44]. Nonlinearities can then be introduced as additional terms in these equations, without disturbing the previously derived relationships, as long as the nonlinear processes are also weak (i.e., nonlinear effects occur slowly compared to the frequency), which is true in nonlinear optics [48]. Using these ODEs, the general possible behaviors can be obtained (including the Manley-Rowe relations mentioned above); but, to obtain the specific characteristics of a particular geometry, one then needs a separate calculation to obtain the cavity parameters. Properties of the linear modes, such as frequencies and lifetimes (\( Q \)), can be obtained by standard computational methods [41,44]. It turns out that the nonlinear coefficients can also be obtained from the linear calculations, thanks to the fact that the nonlinearities are weak; using perturbation theory, expressions for the nonlinear coefficients as integrals of the linear modes can be derived from Maxwell’s equations. Such expressions were previously derived for SHG and THG [2], and also recently for DFG [61]. Here, we derive both the abstract TCMT equations and the specific nonlinear coupling coefficients for DFWM in the Maxwell equations with \( \chi^{(3)} \) nonlinearities.

In Sec. II, we begin to apply the coupled-mode formalism to the case of DFWM in a triply resonant cavity to obtain the coupled-mode equations of motion as well as explicit expressions for the nonlinear coupling coefficients. We then briefly discuss general properties of the conversion process in Sec. III and, using the standard Manley-Rowe relations and simple photon-counting arguments, obtain limits on the
nonlinearity. (Right) Diagram illustrating the relationship between the three resonant frequencies.

maximal efficiency of the system. In Secs. IV A and IV B, we analyze the stability and dynamics of the solutions to the coupled-mode equations obtained in Sec. II, neglecting SPM and XPM effects, and demonstrate the existence of the maximal conversion efficiencies obtained in Sec. III. Finally, in Sec. IV C, we briefly consider the effects of SPM and XPM using a simple model to illustrate the qualitative behavior of the system; in particular, we demonstrate the existence of stable, maximal-efficiency solutions, including SPM and XPM effects.

II. TEMPORAL COUPLED-MODE THEORY

We consider the situation depicted schematically in Fig. 1: an input or output channel coupled to a triply resonant nonlinear ($\chi^{(3)}$) cavity. Here, input light at $\omega_0$ and $\omega_m = \omega_0 - \Delta \omega$ is converted to output light at a different frequency $\omega_p = \omega_0 + \Delta \omega$, where $\Delta \omega$ determines the separation between the three frequencies. The frequency-conversion process occurs inside the nonlinear cavity, which supports resonant modes of frequencies $\omega_0$, $\omega_m$, and $\omega_p$, and corresponding modal lifetimes $\tau_k$ (or quality factors $Q_k = \omega_k \tau_k / 2$ [44]) describing the overall decay rate (1/$\tau_k$) of the modes. In particular, the total decay rate consists of decay into the output channel, with rate 1/$\tau_{c,k}$, as well as external losses (e.g., absorption) with rate 1/$\tau_{s,k}$, so that 1/$\tau_k = 1/\tau_{c,k} + 1/\tau_{s,k}$. Note that, to compensate for the effects of SPM and XPM, as described in [1] and in Sec. IV C, we will eventually use slightly different cavity frequencies $\omega_k^{cav}$ that have been preshifted away from $\omega_k$.

It is most convenient to express the TCMT equations in terms of the following degrees of freedom [41,44]: we let $a_k$ denote the time-dependent complex amplitude of the $k$th mode, normalized so that $|a_k|^2$ is the electromagnetic energy stored in this mode, and let $s_{k, \pm}$ denote the time-dependent amplitude of the incoming (+) and outgoing (−) wave, normalized so that $|s_{k, \pm}|^2$ is the power in the $k$th mode. (In what follows, we take $s_{p, +} = 0$, corresponding to the up-conversion of light at $\omega_0$ and $\omega_p$ to light at $\omega_p$, for $\Delta \omega > 0$. In order to study the alternative down-conversion process, one has to set $\Delta \omega < 0$, in which case we effectively have $\omega_p \to \omega_m$, as described in the following.)

The derivation of the linear TCMT equations, corresponding to decoupled modes $a_k$, has been given elsewhere [44], and the generalization to include nonlinearities has been laid out in Ref. [2]. Here we introduce cubic nonlinearities and make the rotating-wave approximation (only terms with frequencies near $\omega_0$ are included in the equation of motion for $a_0$) [2]. This yields the following general coupled-mode equations:

$$\frac{d a_0}{d t} = \left[ i \alpha_0 (1 - \alpha_{00} |a_0|^2 - \alpha_{0m} |a_m|^2 - \alpha_{0p} |a_p|^2) \right] a_0$$

$$- \omega_0 \beta_0 a_0^* a_0 + \frac{2}{\tau_{s,0}} s_{0, +},$$

(1)

$$\frac{d a_m}{d t} = \left[ i \omega_m (1 - \alpha_{m0} |a_0|^2 - \alpha_{mm} |a_m|^2 - \alpha_{mp} |a_p|^2) \right] a_m$$

$$- \omega_m \beta_m a_m^2 a_m^* + \frac{2}{\tau_{s,m}} s_{m, +},$$

(2)

$$\frac{d a_p}{d t} = \left[ i \omega_p (1 - \alpha_{p0} |a_0|^2 - \alpha_{pm} |a_m|^2 - \alpha_{pp} |a_p|^2) \right] a_p$$

$$- \omega_p \beta_p a_p^2 a_p^*,$$

(3)

$$s_{k, -} = \frac{2}{\tau_{s,k}} a_k - s_{k, +}.$$  

(4)

As explained in Ref. [2], the nonlinear coefficients $\alpha_{ij}$ and $\beta_k$ depend on the specific geometry and materials, and express the strength of the nonlinear interactions. The $\alpha_{jk}$ terms describe self- and cross-phase modulation effects, which act to shift the cavity frequencies, while the $\beta_k$ terms characterize the energy transfer (frequency conversion) between the modes. As noted in Ref. [2], these terms are constrained by energy conservation, which amounts to setting $\frac{d}{d t}(|a_0|^2 + |a_m|^2 + |a_p|^2) = 0$ (in the absence of external losses), yielding the following relation:

$$\omega_0 \beta_0^* = \omega_m \beta_m + \omega_p \beta_p.$$  

(5)

In the following sections, for simplicity, we neglect losses such as linear absorption or radiation (we assume $\tau_{c,k} = \tau_k$) and neglect nonlinear two-photon absorption (we assume $\alpha_{ij}$ are strictly real (two-photon absorption effects can be minimized by selecting materials less susceptible to such processes)). As noted in the following, these considerations do not qualitatively change our results, but merely act to slightly decrease the overall conversion efficiency once losses are included [1,2].

The dependence of the coupling coefficients $\alpha_{ij}$ and $\beta_k$ on the geometry of the system can be obtained via a simple perturbative calculation involving the linear eigenmodes of the cavity, as described in Ref. [2]. Carrying out this procedure to first order in $\chi^{(3)}$ yields the following coupling coefficients:

$$\beta_0 = \frac{1}{8} \int d^3 \mathbf{x} \varepsilon_0 \chi^{(3)}[\mathbf{E}_0 \cdot \mathbf{E}_0] \mathbf{E}_m \cdot \mathbf{E}_p + 2 \mathbf{E}_0 \cdot \mathbf{E}_m \mathbf{E}_0 \cdot \mathbf{E}_p]$$

$$\frac{1}{(d^3 x |\mathbf{E}_0|^2)(d^3 x |\mathbf{E}_m|^2)(d^3 x |\mathbf{E}_p|^2)}$$

$$\frac{1}{2} d^3 x [\mathbf{E}^2 + |\mathbf{E}_p|^2]$$

(6)

$$\beta_m = \beta_p = \frac{1}{2} \beta_0^*,$$

(7)

$$\alpha_{jj} = \frac{1}{8} \int d^3 \mathbf{x} \varepsilon_0 \chi^{(3)} [\mathbf{E} \cdot \mathbf{E}]^2 + |\mathbf{E}_j|^2] \frac{1}{(d^3 x |\mathbf{E}^2 + |\mathbf{E}_j|^2)},$$

(8)

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\[ \alpha_{jk} = \frac{1}{8} \int d^3x \varepsilon_{0,k}^{(3)} \left[ |\mathbf{E}_j| \cdot |\mathbf{E}_k| + |\mathbf{E}_j \cdot \mathbf{E}_k|^2 + |\mathbf{E}_j|^2 |\mathbf{E}_k|^2 \right] \left( \frac{d^3x \varepsilon}{|\mathbf{E}_j|^2} \right) \left( \frac{d^3x \varepsilon}{|\mathbf{E}_k|^2} \right) \]

\[ \alpha_{kj} = \alpha_{jk}, \]

where \( \mathbf{E}_k \) is the electric field in the \( k \)th mode and the denominators arise from the normalization of \( |\alpha_k|^2 \). As expected, Eqs. (6) and (7) satisfy Eq. (5), where Eq. (5) was obtained by imposing energy conservation on the TCMT equations without reference to the specific case of Maxwell’s equations.

There are six different \( \alpha_{jk} \) parameters [three SPM (\( \alpha_{jj} \)) and three XPM (\( \alpha_{jk} \)) coefficients] and, in general, they will all differ. However, from Eqs. (8) and (9), we see that they are all determined by similar modal integrals, lead to frequency shifting of the cavity frequencies, and all scale as \( 1/V \), where \( V \) denotes a modal volume of the fields [41]. Therefore, in the following sections, we begin by neglecting the frequency-shifting terms as in Ref. [1], and then, in Sec. IV C, we study the essential effects of frequency shifting in the simplified case where all the coefficients are equal (\( \alpha_{jk} = \alpha \)). Of course, for a specific geometry, one would calculate all coefficients Eqs. (6)–(10); in this paper, we focus on the fundamental physics and phenomena rather than on the precise behavior of a specific geometry.

III. QUANTUM-LIMITED VERSUS COMPLETE CONVERSION

As described in the following, the DFWM process we consider here exhibits drastically different behavior depending on the ratio of \( \Delta \omega \) to \( \omega_0 \). In particular, there exist at least two distinct regimes of operation corresponding to quantum-limited (\( |\Delta \omega| < \omega_0 \)) and complete (\( |\Delta \omega| \geq \omega_0 \)) conversion. It turns out that, although our coupled-mode formalism is entirely classical, the same behaviors can be more easily understood by considering photon interactions in a quantum picture. Although this system is, of course, described by the general Manley-Rowe relations, which can be derived from both classical [44,45,48] and quantum [42,43] arguments similar to those here, it is useful to review a basic picture of such limits and their physical consequences for the specific case of intracavity DFWM.

Our focus in this paper is the up-conversion process (or interaction) corresponding to taking input light at frequencies \( \omega_0 \) and \( \omega_m \) and generating output light at frequency \( \omega_p \). Therefore, an appropriate figure of merit is the ratio of the output power in the \( \omega_p \) mode to the total input power, which we define as the absolute efficiency \( \eta = |s_{-j}|^2 / (|s_{0,+}|^2 + |s_{m,+}|^2) \).

As described in the previous section, the coupled-mode Eqs. (1)–(4) follow from very general and purely classical considerations. The same considerations yield relationships between the frequencies and coupling coefficients of the problem, such as frequency conservation (\( \omega_m + \omega_p = 2\omega_0 \)) and energy conservation (\( \omega_m \beta_m + \omega_p \beta_p = \omega_0 \beta_0^2 \)). Additional conservation rules, which are perhaps best understood from quantum arguments such as photon energy (\( h|\omega| \)) conservation and standard \( \chi^{(3)} \) selection rules [48], also play a substantial role in the physics of nonlinear frequency conversion. In the case of the DFWM up-conversion process considered here, \( \chi^{(3)} \) selection rules imply that nonlinear interactions can only be initiated if there exist at least three input photons: two \( \omega_0 \) photons and one \( \omega_m \) photon.

In the \( |\Delta \omega| < \omega_0 \) regime, there are at least two important features that can be understood from the above relations: First, depletion of the signal input power \( s_{m,+} \) is impossible, leading to a conversion efficiency \( \eta < 1 \). Second, in order to maximize the total conversion efficiency, one desires \( s_{m,+} \) to be as small as possible. These features can be understood by considering a simple picture of the nonlinear photon-photon interaction, as follows. From the DFWM \( \chi^{(3)} \) selection rule [48], it follows that the creation of a \( \omega_p \) photon is accompanied by the destruction of two \( \omega_0 \) photons and one \( \omega_m \) photon. The latter, along with photon energy conservation, leads to the process considered in Fig. 2 (left), in which two \( \omega_0 \) photons and a \( \omega_m \) photon interact to yield two \( \omega_m \) photons and a \( \omega_p \) photon. From the figure, and since \( 2\omega_0 > \omega_P \), one can see that the incident \( \omega_m \) photon (depicted in red) is merely required by the \( \chi^{(3)} \) selection rule to initiate the interaction and emerges unmodified, accompanied by a \( \omega_p \) photon and an additional \( \omega_m \) photon. Thus, it is clear that the input \( \omega_m \) photon does not actively participate in the energy transfer and therefore merely reduces the maximum possible conversion efficiency. This implies that one desires a minimal input signal power to initiate the up-conversion. Effectively, the incident \( \omega_m \) photons are amplified by the conversion process (a similar amplification effect is a crucial component in other nonlinear interactions, such as OPAs in \( \chi^{(2)} \) media [48,108,109]). In addition, it is clear that complete depletion of the signal photons, i.e., \( s_{m,-} = 0 \), is not possible for nonzero \( s_{m,+} \), and therefore the
conversion efficiency must be less than 100% (since the total input power is conserved). No such restriction is placed on $s_{0,-}$ and we therefore expect that maximal efficiency will be obtained for arbitrarily low signal power and complete depletion of the pump power, i.e., $s_{0,-} = 0$.

On the basis of these arguments, we can predict the maximal efficiency of the conversion process by considering the ratio of the energy of the output $\omega_p$ photon ($\hbar \omega_p$) to the energy of the three input photons $[\hbar (2\omega_0 + \omega_m)]$. Since the $\omega_m$ photons can be provided with arbitrarily low amplitude, we therefore expect maximal efficiency to be achieved upon neglecting their contribution, i.e., we predict a maximal efficiency of

$$\eta_{\text{max}}(|\Delta \omega < \omega_0|) = \frac{\hbar \omega_p}{2\hbar \omega_0} = \frac{\omega_p}{2\omega_0}. \quad (11)$$

Note that this efficiency depends only on the ratio of $\Delta \omega$ to $\omega_0$ and $\hbar$ cancels, so it should appear in the classical limit as well. As we shall see in Sec. IV A, this prediction is verified analytically by examining the steady-state solution of our coupled-mode equations.

In the $\Delta \omega \geq \omega_0$ regime, the conversion process is fundamentally different and, in particular, complete depletion of the $\omega_m$ and $\omega_0$ photons is possible, leading to 100% conversion efficiency. Basically, because $\omega_p > 2\omega_0$ in this case, no additional photons are required to satisfy photon energy conservation, yielding the nonlinear interaction process depicted in Fig. 2 (right), where two input $\omega_0$ photons and a $\omega_m$ photon combine to produce a $\omega_p$ photon. Note that now the input $\omega_m$ photon actively participates in the energy transfer, in contrast to the $\Delta \omega < \omega_0$ regime, leading to a maximal conversion efficiency occurring when $s_{0,+}$ and $s_{m,+}$ are both nonzero. Furthermore, since $\omega_p$ is now the only product of the interaction, we expect that complete depletion of both the pump and signal powers $s_{0,-} = s_{m,-} = 0$ should be possible, leading to 100% conversion efficiency. As before, this can also be quantified by comparing the ratio of the output energy ($\hbar \omega_p$) to the input energy $[\hbar (2\omega_0 + \omega_m)]$ (note that now the energy of the $\omega_m$ photon is $\hbar |\omega_m|$, and the result follows from the fact that $2\omega_0 + |\omega_m| = \omega_p$. Again, we shall see in Sec. IV B that this prediction is validated analytically and directly from the coupled-mode equations, yielding also the critical input powers at which 100% conversion is achieved.

In this section, we made a number of predictions based on very general arguments relying on a quantum interpretation of the nonlinear interactions, allowing us to obtain predictions of maximal conversion efficiency. Our final results, of course, contained no factors of $\hbar$ and it is therefore not surprising that we recover the same results (albeit with more detail, e.g., predictions of the values of critical powers) in the ensuing analysis of the purely classical coupled-mode equations. Nevertheless, the heuristic quantum picture of Fig. 2 has the virtue of being simple and revealing, while the classical derivation is more complicated (although more quantitative). Similar quantum arguments have also proven useful in other contexts, such as in many problems involving classical radiation [110], or the recently studied problem of optical bonding and antibonding in waveguide structures [111].

### IV. COUPLED-MODE ANALYSIS

To gain a simple understanding of the system, we shall first consider frequency conversion in the absence of self- and cross-phase modulation, i.e., $\alpha_{jk} = 0$. The nonzero $\alpha$ case will be considered in Sec. IV C. Section IV A focuses on the $|\Delta \omega| < \omega_0$ regime, whereas Sec. IV B focuses on the $\Delta \omega \geq \omega_0$ regime. In both cases, we describe the solutions to the coupled-mode equations (1)–(3) in the steady state, including the stability of these solutions and their dependence on the cavity parameters.

#### A. $|\Delta \omega| < \omega_0$ regime: Limited conversion

Although the analysis in this section is general, for the purposes of plotting results, we choose the specific parameters $\alpha_{jk} = 0$, $t_0 = t_m = t_p = 100/\omega_0$, $\beta = 10^{-4}$, and $\Delta \omega = 0.05\omega_0$. The qualitative results remain unchanged as these parameters are varied, provided that the $Q$ are large enough such that mode overlap is minimal as required by CMT. The influence of varying these parameters is discussed further at the end of this section.

To understand the stability and dynamics of the nonlinear coupled-mode equations in the quantum-limited regime, we apply the standard technique of identifying the fixed points of Eqs. (1)–(3) and analyzing the stability of the linearized equations around each fixed point [112]. A fixed point is given by a steady-state solution where the mode amplitudes vary as $a_k(t) = A_k e^{i\omega_k t}$, with the $A_k$ being unknown constants. Plugging this steady-state ansatz into Eqs. (1)–(3), we obtain three coupled polynomial equations in the parameters $A_0, A_m, A_p, s_{0,+},$ and $s_{m,+}$. These polynomials were solved using Mathematica to obtain the mode energies $|A_j|^2$, which are then used to calculate the efficiency $\eta = |s_{p,-}|^2/(|s_{0,+}|^2 + |s_{m,+}|^2)$. The phases of the $A_k$ can be easily determined from the steady-state equations of motion; $A_0$ and $A_m$ acquire the phases of $s_{0,+}$ and $s_{m,+}$, respectively, while the phase of $A_p$ is that of $\beta_p A_0^2 A_m^* \omega_p$ rotated by $\pi/2$. Without loss of generality, $s_{0,+}$ and $s_{m,+}$ can be chosen to be real.

In general, this system has either one or three solutions, only one of which is ever stable. The stability and efficiency of this solution are shown in Fig. 3 for the specific parameters mentioned here. We observe that maximal conversion efficiency is obtained in the limit as input signal power $s_{m,+}$ is reduced to zero, consistent with the discussion in the previous section. To obtain the maximum efficiency and the corresponding critical input powers, complete depletion of the pump ($\omega_0$) photon is required, i.e., $s_{0,-} = 0$ (note that one can not require depletion of the signal photon, for the reasons discussed in the previous section). We find that the maximum efficiency $\eta_{\text{max}}$ is obtained at $|s_{0,+}|^2 = P_0$ as $|s_{m,+}|^2 \rightarrow 0$, where

$$P_0 = \frac{4}{t_0|\beta_0|\sqrt{t_m t_p |\omega_m| \omega_p}}. \quad (12)$$

$$\eta_{\text{max}} = \frac{\omega_p}{2\omega_0} = \frac{1}{2} \left( 1 + \frac{\Delta \omega}{\omega_0} \right). \quad (13)$$

Note that Eq. (13) is identical to the value predicted in the previous section. In the important case of narrow-band conversion $|\Delta \omega| \ll \omega_0$, the maximum efficiency is approximately
50%. (However, this is relative to the pump power; compared to
the input signal alone, the output signal is amplified to an
arbitrary degree.) If \( Q_0 \sim Q_0 \sim Q_p \), then, as in THG [1],
the critical power scales as \( V/Q_0^2 \), where \( V \) is the modal value
(recall that \( \beta \sim 1/V \)).

As \( \Delta \omega \to \omega_0 \), the maximum efficiency approaches unity,
i.e., 100% conversion can be achieved in the limit. This limit is
reminiscent of second-harmonic generation, since \( \omega_p = 2\omega_0 \).
However, the interaction process is fundamentally different
from the standard (\( \chi^{(2)} \)) SHG in a number of ways. First,
one is converting dc (\( \omega_m \approx 0 \)) light and \( \omega_m \) pump light into
\( 2\omega_0 \). Second, the stability of this solution (described in the
following) is quite different from that of SHG [46,47,83].

Finally, the critical power in this case, \( P_c \), the shaded region indicates that the solution is unstable. The solution with maximal efficiency for a given
input signal power does not correspond to complete depletion
of the pump. Requiring pump depletion (\( s_{0,-} = 0 \)) for a given
signal power \( |s_{m,+}|^2 \) yields two pump powers, which we label
\( P_{\pm}(|s_{m,+}|^2) \). \( P_{\pm}(|s_{m,+}|^2) \) does indeed provide a solution with
maximal efficiency; however, this solution is always unstable.

As seen from Fig. 3, only for small signal power \( s_{m,+} \) does
depletion of the pump lead to maximal efficiency.

In general, to obtain the largest efficiency while retaining
stability, one would aim to operate with low signal power
\( |s_{m,+}|^2 \) and use a pump power near the critical power \( P_0 \)
given in Eq. (12). However, it is interesting to consider the
unstable solutions, because they turn out to be related to limit
cycles. As mentioned above, the system contains either one or
two steady-state solutions for given input powers. Figure 4
plots these stable and unstable solutions as a function of
pump power \( |s_{0,+}|^2 \) at fixed signal power \( |s_{m,+}|^2 = 0.1 P_0 \),
corresponding to the horizontal dashed line in Fig. 3. For
low-input pump power \( |s_{0,+}|^2 \), the system has a single steady-
state solution; as the pump power is increased, the system
experiences a bifurcation yielding two unstable solutions.

As mentioned above, the higher efficiency solution emerging
from the bifurcation achieves a maximum corresponding at
\( |s_{0,+}|^2 = P_{\pm} \), coinciding with complete depletion of the pump
(\( s_{0,-} = 0 \)), but this maximal-efficiency solution is always
unstable; note that there may be a stable solution at
\( |s_{0,+}|^2 = P_+ \), but the stable solution will have a lower efficiency than
the maximal, unstable solution, as shown in Fig. 4. Furthermore,
the original stable solution eventually becomes unstable as the
pump power is increased (this can occur before or after the
bifurcation, depending on the system parameters); this onset
of instability coincides with the onset of limit cycles, which
are stable oscillating-efficiency solutions. An example of these
limit cycles is shown in Fig. 4, where the green dashed lines
indicate the bounds of the oscillations and the solid green line gives the average. The limit cycles are plotted as a function of time in the inset of Fig. 4. The limit cycles shown here were obtained by numerically time evolving the coupled-mode equations. In general, we find that these limit cycles oscillate with a period proportional to \( \tau_p \).

Figures 3 and 4 describe a system corresponding to a particular set of values for the parameters \( \Delta \omega \) and \( \tau_k \). Qualitatively, the most important features of the figures remain largely unchanged as these parameters are varied. Basically, there exist at most three solutions to the coupled-mode equations, one of which has a finite region of stability as a function of \( s_{0,+} \) and \( s_{m,+} \), with the general shape that is shown in Fig. 3, and two others that are always unstable and bifurcate at a finite \( s_{0,+} \). There are, however, some differences to note: First, as \( \Delta \omega \) increases from 0, the maximum steady-state efficiency also increases, asymptoting to \( \eta = 1 \) as \( \Delta \omega \to \omega_0 \). This was obtained analytically and is quantified in Eq. (13).

Unfortunately, we find that as \( \Delta \omega \) increases, the region of instability in Fig. 3 also increases; furthermore, the conversion efficiency at finite \( s_{m,+} \) also drops off more rapidly. (In particular, we observe in the “SHG” limit of \( \Delta \omega \to \omega_0 \) that the system becomes largely unstable except for very low signal powers.) These tendencies are depicted in Fig. 5, which plots \( P_c(\Delta \omega, s_{m,+}^2) \) and the corresponding conversion efficiency for different values of \( \Delta \omega \). The kinks observed in the plots of \( P_c \) are due to the discontinuity in the slope of the \( P_c \) curve as it reaches the region of instability, corresponding to the point \( U \) in Fig. 3.

Varying \( \tau_k \) does not affect the maximum possible efficiency and also leaves Fig. 3 qualitatively unchanged, changing only the scale of the critical input power \( P_0 \). The stability of the system, however, does depend on the relative lifetimes of the cavity modes. In particular, the stability depends largely on the ratio \( \tau_0/\tau_p \), and decreases weakly as \( \tau_0 \) increases with respect to either \( \tau_0 \) or \( \tau_p \). This makes sense since, as argued in Sec. III, the \( \omega_m \) photons do not actively participate in the energy transfer. (A similar dependence on the ratio of the lifetimes was also observed in the case of THG [1].) More quantitatively, we follow the position of the point \( U \) (the point where \( P_c \) reaches the region of instability) as the \( \tau_k \) are varied.

Thus far, we have focused on the up-conversion process: taking input light at frequencies \( \omega_0 \) and \( \omega_m \) and generating output light at frequency \( \omega_p > \omega_0 \). However, it suffices to consider this system when \( \Delta \omega < 0 \) to understand the physics of the alternative, down-conversion process: taking input light at frequencies \( \omega_0 \) and \( \omega_p \) and generating output light at frequency \( \omega_m \). For \( \Delta \omega < 0 \), we effectively have \( \omega_m \leftrightarrow \omega_p \). In this regime, all of the above analysis holds and, in particular, the maximal efficiency, given by Eq. (13), is obtained as \( s_{m,+}^2 \to 0 \) with \( s_{0,+}^2 \approx P_0 \). Similarly, the stability of the solutions follows similar trends to those outlined above.

### B. \( \Delta \omega \gg \omega_0 \) regime: Complete conversion

When \( \Delta \omega \) is larger than \( \omega_0 \), we argued in Sec. III that the system is capable of complete conversion, i.e., \( \eta = 1 \). In this section, we demonstrate the existence of a critical steady-state solution to the classical coupled-mode equations with complete conversion and analyze the stability of this critical solution, as well as relate DFWM to our previous work on THG [1,2].

As in the previous section, we consider the equations of motion (1)–(3) in the steady state. To obtain the critical solution, we again require depletion of the pump power, i.e., \( s_{0,-} = 0 \). However, as argued in Sec. III, complete depletion of the signal \( s_{m,-} = 0 \) must also occur. Recall from Sec. III that complete \( \omega_m \) depletion is possible in the \( \Delta \omega \gg \omega_0 \) regime since the up-conversion process does not produce \( \omega_m \) photons (see Fig. 2). Imposing the depletion constraints on the steady-state equations of motion yields the following critical cavity energies \( \kappa_{k}^{\text{crit}} \):

\[
|a_{0}^{\text{crit}}|^2 = \frac{1}{|\beta_m| \sqrt{\tau_p \omega_m \omega_p}}.
\]

\[
|a_{m}^{\text{crit}}|^2 = \frac{\tau_m |\omega_m|}{2 \tau_0 |\omega_0|} |a_{0}^{\text{crit}}|^2, \tag{15}
\]

\[
|a_{p}^{\text{crit}}|^2 = \frac{\tau_p \omega_p}{2 \tau_0 |\omega_0|} |a_{0}^{\text{crit}}|^2, \tag{16}
\]
which lead to the following critical powers:

\[ |s_{0,+}^{\text{crit}}|^2 = P_0, \]  

(17)

\[ |s_{m,+}^{\text{crit}}|^2 = \frac{|\omega_m|}{2\omega_0} P_0, \]  

(18)

where \( P_0 \) is given by Eq. (12). Solving for the corresponding output signal \( |s_{p,-}|^2 \), the output power is indeed 100% of the input power, as required by energy conservation. (In contrast, the assumption that \( \Delta_1 = \omega_0 = 0 \) in the \( |\Delta_0| < \omega_0 \) case yields no solution.) Note that the critical signal power \( |s_{m,+}^{\text{crit}}|^2 \) is now nonzero due to the fact that the energy from the signal \( \omega_m \) photons is necessary to produce the output \( \omega_p \) photons. This is in contrast with the \( |\Delta_0| < \omega_0 \) regime, where maximal conversion efficiency was only achieved in the limit as input signal power \( |s_{m,+}|^2 \) decreased to zero. The critical pump and signal powers, with the corresponding maximum efficiency \( \eta \), are plotted versus \( \Delta_0 \) in Fig. 6 for both \( \Delta_0 \) regimes.

As may be noted from Fig. 6, there are two particular values of \( \Delta_0 \) that warrant special attention when \( \Delta_0 \geq \omega_0 \). The first case, when \( \Delta_0 = \omega_0 \) (the “SHG” case), was discussed in the previous section. The second case is when \( \Delta_0 = 2\omega_0 \). In this case, \( \omega_m = -\omega_0 \) and \( \omega_p = 3\omega_0 \), which is reminiscent of third-harmonic generation (THG). In fact, this case of DFWM corresponds exactly to \( \chi^{(3)} \) THG and, thus, \( \Delta_0 > \omega_0 \) strictly generalizes our previous THG analysis [1]. To see this, some care must be taken to adjust the coupling coefficients \( \beta_k \) given in Eqs. (6) and (7) to properly implement the rotating wave approximation; since \( \omega_m = -\omega_0 \), we have \( \alpha_m = \alpha_0 \), and thus \( \beta_0 \rightarrow \beta_0 + \beta_0^* \) and \( \beta_m \rightarrow \beta_m + \beta_0^* \). This results in \( \beta_0 = \beta_0^* = 3\beta_0^* \) exactly as shown in [1]. Furthermore, we have \( |s_{0,+}^{\text{crit}}|^2 = |s_{m,+}^{\text{crit}}|^2 = P_0 \) [note that this differs by a factor of 2 from Eq. (18), due to the adjusted \( \beta_k \) values]; upon requiring that \( \tau_0 = \tau_m \), this recovers the critical power previously obtained for THG [1]. Note that the correspondence between \( \Delta_0 = 2\omega_0 \) and \( \chi^{(3)} \) THG is exact, whereas the \( \Delta_0 = \omega_0 \) limit has little in common with \( \chi^{(3)} \) SHG as discussed above.

With the existence of a \( s_{0,-} = s_{m,-} = 0 \) solution having demonstrated the existence of critical powers where 100% conversion can be achieved, we are now interested in characterizing the system at this critical power by studying all of the fixed points. These fixed points were obtained using Mathematica as in the previous section, and their stability was determined via linear stability analysis as before. For the critical input power, the steady-state equations of motion yield three solutions; however, in contrast to the \( |\Delta_0| < \omega_0 \) regime, there exists multistability when \( \Delta_0 \geq \omega_0 \). Similar to the case of THG (\( \Delta_0 = \omega_0 \)), the system is either singly stable, doubly stable, or unstable, depending on the values of the mode lifetimes \( \tau_k \) (see Fig. 7). In this \( \Delta_0 > \omega_0 \) regime, the stability of the solutions does not depend on \( \Delta_0 \) again in contrast with the quantum-limited regime. Unlike the \( |\Delta_0| < \omega_0 \) regime, the value of \( \tau_m \) now plays a significant role in the stability of the solutions.

C. Self- and Cross-Phase Modulation (\( \alpha \neq 0 \))

Finally, we briefly consider the effects of SPM and XPM. This corresponds to taking the coefficients \( \alpha_{jk} \) to be nonzero; as mentioned above, for simplicity, we take all the coefficients to be equal, i.e., \( \alpha_{jk} = \alpha \) for all \( j,k \). The main effect of SPM and XPM in Eqs. (1) and (2) is to shift the resonant frequencies of the cavity in proportion to the energy of the modes in the cavity. Generally, this drives the frequency input light off resonance and therefore degrades the overall conversion efficiency obtained in Secs. IV A and IV B, as shown in Ref. [1]. However, in Ref. [1], we showed that one simple way to overcome this difficulty is to preshift the cavity resonant
can be accounted for by a preshifting technique described in this case as well.

find that 100% photon-conversion efficiency can be obtained explained above, their stability may change. Using the results obtained in Secs. IV A and IV B and, in particular, we find that 100% photon-conversion efficiency can be obtained in this case as well.

The change in cavity frequency due to SPM and XPM can be accounted for by a preshifting technique described in Ref. [1]. In particular, the $\alpha$ terms in Eqs. (1)–(3) act to shift the cavity resonant frequencies from $\omega^c_0 \rightarrow \omega^c_k$, spoiling the frequency-conservation relations necessary for efficient nonlinear frequency conversion as well as detuning the resonances from the input light. However, one can simply design the cavity frequencies to be resonant at the shifted frequencies, i.e., $\omega^c_0 = \omega^c_{N_0}$ for a given steady-state solution. For the critical solutions corresponding to 100% photon-conversion efficiency, this implies that the new cavity frequencies will be given by [1]

$$\omega^c_0 = \frac{\omega_0}{1 - \alpha (|a_0^{\text{crit}}|^2 + |a_p^{\text{crit}}|^2 + |a_m^{\text{crit}}|^2)},$$

$$\omega^c_m = \frac{\omega_m}{1 - \alpha (|a_0^{\text{crit}}|^2 + |a_p^{\text{crit}}|^2 + |a_m^{\text{crit}}|^2)},$$

$$\omega^c_p = \frac{\omega_p}{1 - \alpha (|a_0^{\text{crit}}|^2 + |a_p^{\text{crit}}|^2 + |a_m^{\text{crit}}|^2)},$$

where $|a_k^{\text{crit}}|^2$ are the energies of the modes at critical power. For cavity resonances $\omega^c_0$, the new equations of motion are given by

$$\frac{d\alpha_0}{dt} = \left[ i\omega^c_0 (1 - \alpha_0 |a_0|^2 - \alpha_m |a_m|^2 - \alpha_p |a_p|^2) - \frac{1}{\tau_0} \right] a_0 - i\alpha_0 \beta_0 a_0 a_m a_p + \sqrt{\frac{2}{\tau_{r,0}}} s_{0,\pm},$$

$$\frac{d\alpha_m}{dt} = \left[ i\omega^c_m (1 - \alpha_m |a_0|^2 - \alpha_m |a_m|^2 - \alpha_m |a_p|^2) - \frac{1}{\tau_m} \right] a_m - i\alpha_0 \beta_0 a_0 a_m a_p + \sqrt{\frac{2}{\tau_{s,m,\pm}}} s_{m,\pm},$$

$$\frac{d\alpha_p}{dt} = \left[ i\omega^c_p (1 - \alpha_p |a_0|^2 - \alpha_p |a_m|^2 - \alpha_p |a_p|^2) - \frac{1}{\tau_p} \right] a_p - i\alpha_0 \beta_0 a_0 a_m a_p.$$

Note that the frequencies $\omega^c_0$ multiplying the $\beta_k$ terms do not need to be shifted, since the terms introduced by such a shifting will be higher order in $\chi^3$. By inspection, we observe that the solutions obtained in Secs. IV A and IV B at critical input power $a_0^{\text{crit}}$ are also solutions of Eqs. (22) and (23), but, as explained above, their stability may change. Using the results from Secs. IV A and IV B, we now study the stability properties of these solutions in the two $\Delta \omega$ regimes.

We first consider the $\Delta \omega \leq \omega_0$ regime. As in Sec. IV A, we restrict our analysis to a specific parameter regime ($\tau_0 = \tau_m = \tau_p = 100/\omega_0, \beta = 10^{-4}$, and $\Delta \omega = 0.05\omega_0$) for simplicity, although our qualitative conclusions apply to other parameter ranges. As discussed in Sec. IV A, the maximal efficiency is obtained for input light with $|s_{0,\pm}|^2 = P_0$ as $|s_{m,\pm}|^2 \rightarrow 0$. Since one must always pump with finite $|s_{m,\pm}|^2$, and there are no analytic solutions in this case, we solve for the field energies $|a_k^{\text{crit}}|^2$ numerically at a small $|s_{m,\pm}|^2$ and for $|s_{k,\pm}|^2 = P_0$ in the case of $\alpha = 0$ in order to compute the shifted frequencies (19)–(21). This allows us to solve the coupled-mode Eqs. (22) and (23) and therefore obtain the steady-state field amplitudes and phases. As in Ref. [1], the inclusion of self- and cross-phase modulation introduces new steady-state solutions absent in the $\alpha = 0$ case, and the stability of the old and new solutions are then examined again via a linear stability analysis, as in Sec. IV A. In particular, we find that the inclusion of SPM and XPM does not destroy the stability of the maximal-efficiency solution in the $\alpha = 0$ case studied in Sec. IV A and, in fact, creates additional stable solutions, as shown in Fig. 8.

A similar analysis can be performed in the $\Delta \omega > \omega_0$ regime, where it is possible to obtain the analytic form of the maximal-efficiency solutions [Eqs. (14)–(16) in Sec. IV B]. We find that, as in the previous regime, the presence of $\alpha$ introduces additional stable solutions, while retaining the original 100% efficiency $\alpha = 0$ solution over finite regions of the parameter space.

The presence of SPM and XPM in our system provides an opportunity to observe rich and interesting dynamical behaviors, including limit cycles and hysteresis effects, that we do not explore in this paper. As noted in this section, the inclusion of these effects is not prohibitive for 100% nonlinear frequency conversion, although predicting which parameter regimes allow for such conversion will depend on the system under question.

In the future, we plan to examine SPM and XPM effects in more detail for realistic parameters.
geometries with realistic values of $\alpha_{ij}$ and $\beta_i$. As in Ref. [1], the presence of multiple stable solutions means that the manner in which the source is initiated will determine which solution is excited, but a simple initialization procedure similar to that in Ref. [1] should be possible to excite the maximal-efficiency solution.

V. CONCLUSION

By exploiting a simple but rigorous coupled-mode theory framework, we have demonstrated the possibility of achieving highly efficient (low-power) DFWM in triply resonant cavities, similar to our previous work in SHG and THG [1,2]. We conclude that there are two main regimes of operation, determined by the ratio of $\Delta \omega$ to $\omega_0$. In particular, whereas the maximal efficiency obtainable in the $\Delta \omega \leq \omega_0$ regime, corresponding to conversion between closely spaced resonances, is bounded above by a quantum-limited process, there is no such bound when $\Delta \omega > \omega_0$. In both regimes, a suitable choice of system parameters leads to stable, maximal-efficiency nonlinear frequency conversion, even in the presence of SPM and XPM effects. We remark that all of the results obtained in this paper correspond to the idealized case of lossless interactions, since the main focus of the paper is in examining the basic considerations involved in operating with these systems rather than predicting results for specific experimentally relevant systems. Nevertheless, based on our previous experience with SHG and THG [1,2], we expect that linear and nonlinear losses, e.g., coming from radiation or material absorption, will only act to slightly decrease the overall conversion efficiency and will not affect the qualitative predictions here. In a future manuscript, we plan to explore DFWM in a realistic geometry such as a ring resonator coupled to an index-guided waveguide and study some of the dynamical effects arising from SPM and XPM.

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