Probabilistic Safety Constraints for Learned High Relative Degree System Dynamics

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Abstract

This paper focuses on learning a model of system dynamics online while satisfying safety constraints. Our motivation is to avoid offline system identification or hand-specified dynamics models and allow a system to safely and autonomously estimate and adapt its own model during online operation. Given streaming observations of the system state, we use Bayesian learning to obtain a distribution over the system dynamics. In turn, the distribution is used to optimize the system behavior and ensure safety with high probability, by specifying a chance constraint over a control barrier function. **Keywords:** Gaussian Process regression, online system dynamics learning, high relative-degree safety, exponential control barrier function

1. Introduction

Unmanned vehicles promise to transform many aspects of our lives, including transportation, agriculture, mining, and construction. Successful use of robot autonomy in these areas depends critically on the ability of robots to adapt safely to changing operational conditions. Existing systems, however, rely on brittle hand-designed dynamics models and safety rules that often fail to account for the complexity and uncertainty of real-world operation. Recent work (Deisenroth and Rasmussen, 2011; Dean et al., 2019; Sarkar et al., 2019; Rantzer, 2018; Tu and Recht, 2018; Coulson et al., 2019; Chen et al., 2018; Rosolia et al., 2018; Taylor et al., 2019; Liu et al., 2019; Umlauft and Hirche, 2019) has demonstrated that learning-based system identification and control techniques may be successful at complex tasks and control objectives. However, two critical considerations for applying these techniques onboard autonomous systems remain: learning *online*, relying on streaming data, and guaranteeing *safe* operation, despite the uncertainty inherent to learning algorithms.

Motivated by the utility of Lyapunov functions for certifying stability properties, Ames et al. (2016); Xu et al. (2017); Xu et al. (2015); Prajna et al. (2007); Ames et al. (2019) proposed *control* barrier functions (CBFs) as a tool for characterizing long-term safety of dynamical systems. A CBF certifies whether a control policy achieves forward invariance of a *safe set* C by evaluating if the system trajectory remains away from the boundary of C. Most of the literature on CBFs

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considers systems with known dynamics, low relative degree, no disturbances, and time-triggered control, in which the control inputs are recalculated at a fixed and sufficiently small period. This is limiting because, low control frequency in a time-triggered setting may lead to safety constraint violation in-between sampling times. On the other hand, high control frequency leads to inefficient use of computational resources and actuators. Yang et al. (2019) extend the CBF framework to a self-triggered setup in which the longest time until a control input needs to be recomputed to guarantee safety is provided. CBF techniques handle nonlinear control-affine systems but many existing results apply only to relative-degree-one systems, in which the first time derivative of the CBF depends on the control input. This requirement is violated by many underactuated robot systems and motivated extensions to relative-degree-two systems, such as bipedal and car-like robots. (Hsu et al., 2015; Nguyen and Sreenath, 2016b). Nguyen and Sreenath (2016a) generalized these ideas by designing an exponential control barrier function (ECBF) capable of handling control-affine systems with arbitrary relative degree.

Providing safety guarantees for learning-based control techniques has received a great deal of attention (Koller et al., 2018; Berkenkamp et al., 2017, 2016; Fisac et al., 2018; Lew et al., 2019). In particular, the utility of the CBF framework may be expanded by considering noisy or a priori unknown system dynamics. Techniques for handling additive disturbances have been proposed in (Clark, 2019; Santoyo et al., 2019), while CBF conditions for systems with uncertain dynamics have been proposed in (Fan et al., 2019; Wang et al., 2018; Taylor and Ames, 2019; Cheng et al., 2019; Salehi et al., 2019). Fan et al. (2019) study time-triggered CBF-based controllers for controlaffine systems with relative degree one, where the input gain part of the dynamics is known and invertible. Bayesian learning is used in (Fan et al., 2019) to determine a distribution over the drift term of the dynamics. In particular, (Fan et al., 2019) compared the performances of Gaussian Process regression (Williams and Rasmussen, 2006), Dropout neural networks (Gal and Ghahramani, 2016), and ALPaCA (Harrison et al., 2018) in simulations. Wang et al. (2018), (Cheng et al., 2019), and (Taylor and Ames, 2019) study time-triggered CBF-based control relative-degree-one systems in presence of additive uncertainty in the drift part of the dynamics. In (Wang et al., 2018), GP regression is used to approximate the unknown part of the 3D nonlinear dynamics of a quadrotor. Cheng et al. (2019) proposed a two-layers control design architecture that integrates CBF-based controllers with model-free reinforcement learning. Taylor and Ames (2019) proposed adaptive CBFs to deal with parameter uncertainty. Salehi et al. (2019) studies nonlinear systems only with drift terms and uses Extreme Learning Machines to approximate the dynamics.

Our work proposes a learning approach for estimating posterior distribution of robot dynamics from online data to design a control policy that guarantees safe operation. We make the following **contributions**. First, we develop a matrix variate Gaussian Process (GP) regression approach with efficient covariance factorization to learn the *drift term* and *input gain* terms of a nonlinear control-affine system. Second, we use the GP posterior to specify a probabilistic safety constraint and determine the longest time until a control input needs to be recomputed to guarantee safety with high probability. Finally, we extend our formulation to dynamical systems with arbitrary relative degree and show that a safety constraint can be specified only in terms of the mean and variance of the Lie derivatives of the CBF. **Notation, proofs, and additional remarks are available in the appendix at arXiv (Khojasteh et al., 2019)**.

2. Background

Consider a control-affine nonlinear system:

$$\dot{\mathbf{x}} = f(\mathbf{x}) + g(\mathbf{x})\mathbf{u} = \begin{bmatrix} f(\mathbf{x}) & g(\mathbf{x}) \end{bmatrix} \begin{bmatrix} 1\\ \mathbf{u} \end{bmatrix} =: F(\mathbf{x})\underline{\mathbf{u}}$$
(1)

where $\mathbf{x}(t) \in \mathbb{R}^n$ and $\mathbf{u}(t) \in \mathbb{R}^m$ are the system state and control input, respectively, at time *t*. Assume that the *drift term* $f : \mathbb{R}^n \to \mathbb{R}^n$ and the *input gain* $g : \mathbb{R}^n \to \mathbb{R}^{n \times m}$ are locally Lipschitz. We study the problem of enforcing probabilistic safety properties via CBF when *f* and *g* are unknown. We first review key results on CBF-based safety for *known dynamics* (Ames et al., 2019).

2.1. Known Dynamics: Control Barrier Functions for Safety

Let $C \subset D \subset \mathbb{R}^n$ be a *safe set* of system states. Assume $C = \{\mathbf{x} \in D \mid h(\mathbf{x}) \ge 0\}$ is specified as the superlevel set of $h \in C^1(D, \mathbb{R})$, a continuously differentiable function $D \to \mathbb{R}$, such that $\nabla_{\mathbf{x}}h(\mathbf{x}) \ne 0$ for all \mathbf{x} when $h(\mathbf{x}) = 0$. For any initial condition $\mathbf{x}(0)$, there exists a maximum time interval $I(\mathbf{x}(0)) = [0, \bar{t})$ with $\bar{t} \in \mathbb{R} \cup \{\infty\}$ such that $\mathbf{x}(t)$ is a unique solution to (1) (Khalil, 2002). System (1) is *safe* with respect to set C if C is *forward invariant*, i.e., for any $\mathbf{x}(0) \in C$, $\mathbf{x}(t)$ remains in C for all t in $I(\mathbf{x}(0))$. System safety may be asserted as follows.

Definition 1 A function $h \in C^1(D, \mathbb{R})$ is a control barrier function (CBF) for the system in (1) if the following control barrier condition (CBC) is satisfied:

$$\sup_{\mathbf{u}} CBC(\mathbf{x}, \mathbf{u}) \ge 0, \qquad \forall \mathbf{x} \in \mathcal{D}$$
(2)

for $CBC(\mathbf{x}, \mathbf{u}) := \mathcal{L}_f h(\mathbf{x}) + \mathcal{L}_g h(\mathbf{x}) \mathbf{u} + \alpha(h(\mathbf{x}))$, where α is any extended class K_{∞} function and $\mathcal{L}_f h(\mathbf{x})$ and $\mathcal{L}_g h(\mathbf{x})$ are the Lie derivatives of h along f and g, respectively.

Theorem 1 (Sufficient Condition for Safety (Ames et al., 2019)) Consider a safe set C with associated function $h \in C^1(\mathcal{D}, \mathbb{R})$. If $\nabla_{\mathbf{x}} h(\mathbf{x}) \neq 0$ for all $\mathbf{x} \in \partial C$, then any Lipschitz continuous control policy $\pi(\mathbf{x}) \in {\mathbf{u} \in \mathcal{U} | CBC(\mathbf{x}, \mathbf{u}) \ge 0}$ renders the system in (1) safe.

Ames et al. (2019) also provide a necessary condition for safety allowing a concise charaterization:

(1) is safe with respect to $\mathcal{C} \iff \exists \mathbf{u} = \pi(\mathbf{x}) \text{ s.t. } \operatorname{CBC}(\mathbf{x}, \mathbf{u}) \ge 0 \quad \forall \mathbf{x} \in \mathcal{D}.$ (3)

2.2. Known Dynamics: Optimization-based Safe Control

The results in Sec. 2.1 allow designing a control policy $\pi(\mathbf{x})$ that guarantees system safety as long as $\text{CBC}(\mathbf{x}, \pi(\mathbf{x}))$ remains positive along the system trajectories. In practice, this is achieved by solving a quadratic program (QP) repeatedly at triggering times $t_k = k\tau$ for $k \in \mathbb{N}$ and $\tau > 0$:

$$\min_{\mathbf{u}_k} \mathbf{u}_k^\top Q \mathbf{u}_k \qquad \text{s.t. } \mathbf{CBC}(\mathbf{x}_k, \mathbf{u}_k) \ge 0, \tag{4}$$

where $Q \succ 0$, $\mathbf{x}_k := \mathbf{x}(t_k)$, $\mathbf{u}_k := \mathbf{u}(t_k)$. While the QP above cannot be solved infinitely fast, Theorem 3 of Ames et al. (2016) shows that if f, g, and $\alpha \circ h$ are locally Lipschitz, then $\mathbf{u}_k(\mathbf{x})$ and $\text{CBC}(\mathbf{x}, \mathbf{u}_k(\mathbf{x}))$ are locally Lipschitz. Thus, for sufficiently small τ , solving (4) at $\{t_k\}_{k \in \mathbb{N}}$ ensures safety during the inter-triggering times as well.

3. Problem Statement

Consider a control-affine nonlinear system (1), where $F : \mathbb{R}^n \to \mathbb{R}^{n \times (m+1)}$ is *unknown*. Our objective is to estimate $F(\mathbf{x})$ from online observations of the system state and control trajectory and ensure that (1) remains safe with respect to a set C.

Problem 1 Given a prior Gaussian Process distribution $vec(F(\mathbf{x}))^1 \sim \mathcal{GP}(vec(\mathbf{M}_0(\mathbf{x})), \mathbf{K}_0(\mathbf{x}, \mathbf{x}'))$ on the unknown system dynamics and a training set $\mathbf{X}_{1:k} := [\mathbf{x}(t_1), \dots, \mathbf{x}(t_k)], \mathbf{U}_{1:k} := [\mathbf{u}(t_1), \dots, \mathbf{u}(t_k)], \dot{\mathbf{X}}_{1:k} = [\dot{\mathbf{x}}(t_1), \dots, \dot{\mathbf{x}}(t_k)]^2$, compute the posterior Gaussian Process distribution $\mathcal{GP}(vec(\mathbf{M}_k(\mathbf{x})), \mathbf{K}_k(\mathbf{x}, \mathbf{x}'))$ of $vec(F(\mathbf{x}))$ conditioned on $(\mathbf{X}_{1:k}, \mathbf{U}_{1:k}, \dot{\mathbf{X}}_{1:k})$.

Problem 2 Given a safe set C, the system state $\mathbf{x}_k := \mathbf{x}(t_k)$, and the distribution $\mathcal{GP}(vec(\mathbf{M}_k(\mathbf{x})))$, $\mathbf{K}_k(\mathbf{x}, \mathbf{x}')$ of $vec(F(\mathbf{x}))$ at time t_k , choose a control input \mathbf{u}_k and triggering period τ_k such that:

$$\mathbb{P}(CBC(\mathbf{x}(t), \mathbf{u}_k) \ge 0) \ge p_k \quad for \quad \mathbf{u}(t) \equiv \mathbf{u}_k \quad and \quad t \in [t_k, t_k + \tau_k) \tag{5}$$

where $\mathbf{x}(t)$ follows the dynamics in (1), and $p_k \in (0, 1)$ is a user-specified risk tolerance.

4. Matrix Variate Gaussian Process Regression of System Dynamics

We propose an efficient Gaussian Process (GP) regression approach to compute a posterior distribution over the dynamics $F(\mathbf{x})$ of the nonlinear control-affine systems (1). The posterior will be used to determine the distribution of $\text{CBC}(\mathbf{x}, \mathbf{u})$ in Sec. 5. Since $F(\mathbf{x})$ is matrix-valued, we define a GP over its vectorization, $vec(F(\mathbf{x})) \sim \mathcal{GP}(vec(\mathbf{M}_0(\mathbf{x})), \mathbf{K}_0(\mathbf{x}, \mathbf{x}'))$. As in Coregionalization models (Alvarez et al., 2012), we can simplify the covariance structure by assuming that $\mathbf{K}_0(\mathbf{x}, \mathbf{x}') = \Sigma \kappa_0(\mathbf{x}, \mathbf{x}')$ decomposes into a scalar state-dependent kernel $\kappa_0(\mathbf{x}, \mathbf{x}')$ and an outputdimension-dependent covariance matrix $\Sigma \in \mathbb{R}^{n(1+m)\times(1+m)n}$. For systems with large state or control dimensions, learning the $(1+m)^2n^2$ parameters of Σ may require large amounts of training data. Moreover, the nice matrix-times-scalar-kernel structure is not preserved in the posterior. We develop a different factorization of $\mathbf{K}_0(\mathbf{x}, \mathbf{x}')$ based on the Matrix Variate Gaussian distribution (Sun et al., 2017).

Definition 2 The Matrix Variate Gaussian (MVG) distribution is a three-parameter distribution $\mathcal{MN}(\mathbf{M}, \mathbf{A}, \mathbf{B})$ describing a random matrix $\mathbf{X} \in \mathbb{R}^{n \times m}$ with probability density function:

$$p(\mathbf{X}; \mathbf{M}, \mathbf{A}, \mathbf{B}) := \frac{\exp\left(-\frac{1}{2}\operatorname{tr}\left[\mathbf{B}^{-1}(\mathbf{X} - \mathbf{M})^{\top}\mathbf{A}^{-1}(\mathbf{X} - \mathbf{M})\right]\right)}{(2\pi)^{nm/2}\operatorname{det}(\mathbf{A})^{m/2}\operatorname{det}(\mathbf{B})^{n/2}}$$
(6)

where $\mathbf{M} \in \mathbb{R}^{n \times m}$ is the mean, and $\mathbf{A} \in \mathbb{R}^{n \times n}$, $\mathbf{B} \in \mathbb{R}^{m \times m}$ encode the covariance matrix of the rows and columns of \mathbf{X} , respectively.

We provide additional properties of the MVG distribution in Appendix B.1. Note that if $\mathbf{X} \sim \mathcal{MN}(\mathbf{M}, \mathbf{A}, \mathbf{B})$, then $vec(\mathbf{X}) \sim \mathcal{N}(vec(\mathbf{M}), \mathbf{B} \otimes \mathbf{A})$. Based on this observation, we propose the following GP parameterization for the vector-valued functions $vec(F(\mathbf{x}))$:

$$vec(F(\mathbf{x})) \sim \mathcal{GP}(vec(\mathbf{M}_0(\mathbf{x})), \mathbf{B}_0(\mathbf{x}, \mathbf{x}') \otimes \mathbf{A})$$
 (7)

^{1.} $vec(F(\mathbf{x})) \in \mathbb{R}^{n(m+1)}$ is a vector obtained by stacking the columns of $F(\mathbf{x})$

^{2.} If not available, the derivatives may be approximated via $\dot{\mathbf{X}}_{1:k-1} := \begin{bmatrix} \mathbf{x}(t_2) - \mathbf{x}(t_1) \\ t_2 - t_1 \end{bmatrix}^\top, \dots, \frac{\mathbf{x}(t_k) - \mathbf{x}(t_{k-1})}{t_k - t_{k-1}}^\top \end{bmatrix}^\top$ provided that the inter-triggering times $\{\tau_k\}$ are sufficiently small.

The above parameterization is efficient because $\mathbf{B}_0(\mathbf{x}, \mathbf{x}') \in \mathbb{R}^{(m+1) \times (m+1)}$ and $\mathbf{A} \in \mathbb{R}^{n \times n}$ and its structure is preserved in the posterior distribution as we show next.

Consider the training set $(\mathbf{X}_{1:k}, \mathbf{U}_{1:k}, \mathbf{X}_{1:k})$ and a query test point \mathbf{x}_* . The train and test data are jointly Gaussian:

$$\begin{bmatrix} \dot{\mathbf{x}}_1 \\ \vdots \\ \dot{\mathbf{x}}_k \\ vec(F(\mathbf{x}_*)) \end{bmatrix} \sim \mathcal{N} \left(\begin{bmatrix} \mathbf{M}_0(\mathbf{x}_1)\underline{\mathbf{u}}_1 \\ \vdots \\ \mathbf{M}_0(\mathbf{x}_k)\underline{\mathbf{u}}_k \\ vec(\mathbf{M}_0(\mathbf{x}_k)) \end{bmatrix}, \begin{bmatrix} \underline{\mathbf{u}}_1^\top \mathbf{B}_0(\mathbf{x}_1, \mathbf{x}_1)\underline{\mathbf{u}}_1 & \cdots & \underline{\mathbf{u}}_1^\top \mathbf{B}_0(\mathbf{x}_1, \mathbf{x}_k)\underline{\mathbf{u}}_k & \underline{\mathbf{u}}_1^\top \mathbf{B}_0(\mathbf{x}_1, \mathbf{x}_*) \\ \vdots & \ddots & \vdots & \vdots \\ \underline{\mathbf{u}}_k^\top \mathbf{B}_0(\mathbf{x}_k, \mathbf{x}_1)\underline{\mathbf{u}}_1 & \cdots & \underline{\mathbf{u}}_k^\top \mathbf{B}_0(\mathbf{x}_k, \mathbf{x}_k)\underline{\mathbf{u}}_k & \underline{\mathbf{u}}_k^\top \mathbf{B}_0(\mathbf{x}_k, \mathbf{x}_*) \\ \mathbf{B}_0(\mathbf{x}_*, \mathbf{x}_1)\underline{\mathbf{u}}_1 & \cdots & \mathbf{B}_0(\mathbf{x}_*, \mathbf{x}_k)\underline{\mathbf{u}}_k & \mathbf{B}_0(\mathbf{x}_*, \mathbf{x}_*) \end{bmatrix} \otimes \mathbf{A} \right)$$

To simplify notation, let $\mathbf{B}_0(\mathbf{X}_{1:k}, \mathbf{X}_{1:k}) \in \mathbb{R}^{k(m+1) \times k(m+1)}$ be a matrix with elements $[\mathbf{B}_0(\mathbf{X}_{1:k}, \mathbf{X}_{1:k})]_{ij} := \mathbf{B}_0(\mathbf{x}_i, \mathbf{x}_j)$ and define $\mathcal{M}_{1:k} := [\mathbf{M}_0(\mathbf{x}_1) \cdots \mathbf{M}_0(\mathbf{x}_k)] \in \mathbb{R}^{n \times k(m+1)}$ and $\underline{\mathcal{U}}_{1:k} := \operatorname{diag}(\underline{\mathbf{u}}_1, \dots, \underline{\mathbf{u}}_k) \in \mathbb{R}^{k(m+1) \times k}$. Applying a Schur complement, we can derive the posterior distribution of $vec(F(\mathbf{x}_*))$ conditioned on $(\mathbf{X}_{1:k}, \mathbf{U}_{1:k}, \dot{\mathbf{X}}_{1:k})$ as a Gaussian Process $\mathcal{GP}(vec(\mathbf{M}_k(\mathbf{x}_*)), \mathbf{B}_k(\mathbf{x}_*, \mathbf{x}'_*) \otimes \mathbf{A})$ with parameters:

$$\mathbf{M}_{k}(\mathbf{x}_{*}) := \mathbf{M}_{0}(\mathbf{x}_{*}) + \left(\dot{\mathbf{X}}_{1:k} - \mathcal{M}_{1:k}\underline{\mathcal{U}}_{1:k}\right) \left(\underline{\mathcal{U}}_{1:k}^{\top}\mathbf{B}_{0}(\mathbf{X}_{1:k}, \mathbf{X}_{1:k})\underline{\mathcal{U}}_{1:k}\right)^{-1} \underline{\mathcal{U}}_{1:k}^{\top}\mathbf{B}_{0}(\mathbf{X}_{1:k}, \mathbf{x}_{*})$$
$$\mathbf{B}_{k}(\mathbf{x}_{*}, \mathbf{x}_{*}') := \mathbf{B}_{0}(\mathbf{x}_{*}, \mathbf{x}_{*}') + \mathbf{B}_{0}(\mathbf{x}_{*}, \mathbf{X}_{1:k})\underline{\mathcal{U}}_{1:k} \left(\underline{\mathcal{U}}_{1:k}^{\top}\mathbf{B}_{0}(\mathbf{X}_{1:k}, \mathbf{X}_{1:k})\underline{\mathcal{U}}_{1:k}\right)^{-1} \underline{\mathcal{U}}_{1:k}^{\top}\mathbf{B}_{0}(\mathbf{X}_{1:k}, \mathbf{x}_{*}')$$

Details are provided in Appendix C.1.2.

$$F(\mathbf{x}_*)\underline{\mathbf{u}}_* = f(\mathbf{x}_*) + g(\mathbf{x}_*)\mathbf{u}_* \sim \mathcal{GP}(\mathbf{M}_k(\mathbf{x}_*)\underline{\mathbf{u}}_*, \underline{\mathbf{u}}_*^\top \mathbf{B}_k(\mathbf{x}_*, \mathbf{x}'_*)\underline{\mathbf{u}}'_* \otimes \mathbf{A}).$$
(8)

5. Self-triggered Control with Probabilistic Safety Constraints

Sec. 4 addressed Problem 1 by proposing a Gaussian Process inference algorithm for nonlinear control-affine systems. Now, we consider Problem (2). As discussed in Sec. 2.1 if f and g are locally Lipschitz, then system (1) has a unique solution for any $\mathbf{x}(0)$ for all time t in $I(\mathbf{x}(0))$. We assume the sample paths of the GP used to model the dynamics (1) are locally Lipschitz with high probability. Similar smoothness assumption has been made previously in Srinivas et al. (2009). In detail, we assume that for any $L_k > 0$, and triggering time t_k , there exists a constant $b_k > 0$, such that the event

$$\sup_{s \in [0,\tau_k)} \|f(\mathbf{x}(t_k+s)) + g(\mathbf{x}(t_k+s))\mathbf{u}_k - f(\mathbf{x}_k) - g(\mathbf{x}_k)\mathbf{u}_k\| \le L_k \|\mathbf{x}(t_k+s) - \mathbf{x}_k\|,$$
(9)

occurs at least with probability:

$$q_k := 1 - e^{-b_k L_k}.$$
 (10)

This assumption is valid for a large class of GPs, e.g., those with stationary kernels that are four times differentiable, such as squared exponential and some Matérn kernels (Ghosal et al., 2006; Shekhar et al., 2018). However, it may not hold for GPs with highly erratic sample paths.

The posterior of $F(\mathbf{x})\mathbf{u}$ in (8) induces a distribution over $\text{CBC}(\mathbf{x}, \mathbf{u})$. To ensure that safety in the sense of (5) is preserved over a period of time $[t_k, t_k + \tau_k)$, we enforce a tighter constraint at time t_k and determine the time τ_k for which it remains valid. In detail, we solve a chance-constrained version of (4) at time t_k ,

$$\min_{\mathbf{u}_k} \mathbf{u}_k^\top Q \mathbf{u}_k \qquad \text{s.t. } \mathbb{P}(\text{CBC}(\mathbf{x}_k, \mathbf{u}_k) \ge \zeta | \mathbf{x}_k, \mathbf{u}_k) \ge \tilde{p}_k, \tag{11}$$

where $\tilde{p}_k = p_k/q_k$. As mentioned in Problem (2), we use a zero-order hold (ZOH) control mechanism in inter-triggering time, i.e., $\mathbf{u}(t) \equiv \mathbf{u}_k$ for $t \in [t_k, t_k + \tau_k)$. The choice of ζ and its effect on τ_k is discussed next.

Lemma 2 Consider the dynamics in (1) with posterior distribution in (8). Given \mathbf{x}_k and \mathbf{u}_k , $CBC_k := CBC(\mathbf{x}_k, \mathbf{u}_k)$ is a Gaussian random variable with the following parameters:

$$\mathbb{E}[CBC_k] = \nabla_{\mathbf{x}} h(\mathbf{x}_k)^{\top} \mathbf{M}_k(\mathbf{x}_k) \underline{\mathbf{u}}_k + \alpha(h(\mathbf{x}_k)),$$
(12)

$$Var[CBC_k] = \underline{\mathbf{u}}_k^{\top} \mathbf{B}_k(\mathbf{x}_k, \mathbf{x}_k) \underline{\mathbf{u}}_k \nabla_{\mathbf{x}} h(\mathbf{x}_k)^{\top} \mathbf{A} \nabla_{\mathbf{x}} h(\mathbf{x}_k)$$
(13)

Using Lemma 12, we can rewrite the safety constraint as

$$\mathbb{P}(\operatorname{CBC}_{k} \geq \zeta | \mathbf{x}_{k}, \mathbf{u}_{k}) = 1 - \Phi\left(\frac{\zeta - \mathbb{E}[\operatorname{CBC}_{k}]}{\sqrt{\operatorname{Var}[\operatorname{CBC}_{k}]}}\right) \geq \tilde{p}_{k},\tag{14}$$

where $\Phi(\cdot)$ is the cumulative distribution function of the standard Gaussian. Note that if the control input is chosen so that $\zeta - \mathbb{E}[\text{CBC}_k] < 0$, as the posterior variance of CBC_k tends to zero, the probability $\mathbb{P}(\text{CBC}_k \ge \zeta | \mathbf{x}_k, \mathbf{u}_k)$ tends to one. Namely, as the uncertainty about the system dynamics tends to zero, our results reduce to the setting of Sec. 2.1, and safety can be ensured with probability one. Noting that $\Phi^{-1}(1 - \tilde{p}_k) = \sqrt{2} \text{erf}^{-1}(1 - 2\tilde{p}_k)$, ζ needs to satisfy:

$$0 < \zeta \le \mathbb{E}[\operatorname{CBC}_k] + \sqrt{2 \operatorname{Var}[\operatorname{CBC}_k]} \operatorname{erf}^{-1}(1 - 2\tilde{p}_k).$$
(15)

The program (11) provides a probabilistic safety constraints at the triggering times $\{t_k\}_{k\in\mathbb{N}}$. Next, we will extend our analysis to inter-triggering times $\{\tau_k\}$. We continue by re-writing the Proposition 1 of (Yang et al., 2019) for our setup.

Proposition 1 Consider the system in (1) with zero-order hold control in inter-triggering times. If the event (9) occurs at the kth triggering time, then for all $s \in [0, \tau_k)$ we have

$$\|\mathbf{x}(t_k+s) - \mathbf{x}_k\| \le \overline{r}_k(s) := \frac{1}{L_k} \|\dot{\mathbf{x}}_k\| \left(e^{L_k s} - 1\right).$$
(16)

Recall from Sec. 2.1 that h is a continuously differentiable function. Thus using Proposition 1, we notice for any inter-triggering time τ_k , there exist a constant $\chi_k > 0$ such that

$$\sup_{\in [0,\tau_k)} \|\nabla h(\mathbf{x}(t_k+s))\| \le \chi_k.$$
(17)

This is used in the next theorem which concerns Problem 2.

s

Theorem 3 Consider the system in (1) with safe set C. Assume the program (11) has a solution at triggering time t_k , event (9) occurs at least with probability q_k in (10), $\|\dot{\mathbf{x}}_k\| \neq 0$, and for all $s \in [0, \tau_k)$, $\alpha \circ h$ satisfies the following Lipschitz property

$$|\alpha \circ h(\mathbf{x}(t_k+s)) - \alpha \circ h(\mathbf{x}_k)| \le L_{\alpha \circ h} \|\mathbf{x}(t_k+s) - \mathbf{x}_k\|.$$
(18)

Then (5) is valid for $p_k = \tilde{p}_k q_k$, and $\tau_k \leq \frac{1}{L_k} \ln \left(1 + \frac{L_k \zeta}{(\chi_k L_k + L_{\alpha \circ h}) \|\dot{\mathbf{x}}_k\|} \right)$, where χ_k is given in (17).

Remark 4 Assuming $||\dot{x}(t_k)|| \neq 0$ in Theorem (3) is not restricting our results. Since, if the state of the system is safe and it does not change it remains safe.

6. Extension to Higher Relative-degree Systems

Next, we extend the probabilistic safety constraint formulation for systems with arbitrary relative degree, using an exponential control barrier function (ECBF) (Nguyen and Sreenath, 2016a; Ames et al., 2019). Let $r \ge 1$ be the relative degree of $h(\mathbf{x})$, that is, $\mathcal{L}_g \mathcal{L}_f^{(r-1)} h(\mathbf{x}) \ne 0$ and $\mathcal{L}_g \mathcal{L}_f^{(k-1)} h(\mathbf{x}) = 0$, $\forall k \in \{1, \dots, r-2\}$. Define traverse dynamics with traverse vector $\eta(\mathbf{x})$,

$$\dot{\eta}(\mathbf{x}) = \mathcal{F}\eta(\mathbf{x}) + \mathcal{G}\mathbf{u}, \qquad h(\mathbf{x}) = C\eta(\mathbf{x})$$
(19)

where $C = [1, 0, ..., 0]^{\top} \in \mathbb{R}^r$. Also, $\eta(\mathbf{x})$, \mathcal{F} , and \mathcal{G} are defined in Appendix A.

Definition 3 A function $h \in C^r(\mathcal{D}, \mathbb{R})$ is an exponential control barrier function (ECBF) for the system in (1) if there exists a row vector $K_\alpha \in \mathbb{R}^r$ such that the rth order condition $CBC^{(r)}(\mathbf{x}, \mathbf{u}) := \mathcal{L}_f^{(r)}h(\mathbf{x}) + \mathcal{L}_g\mathcal{L}_f^{(r-1)}h(\mathbf{x})\mathbf{u} + K_\alpha\eta(\mathbf{x})$ satisfies:

$$\sup_{\mathbf{u}} CBC^{(r)}(\mathbf{x}, \mathbf{u}) \ge 0, \qquad \forall \mathbf{x} \in \mathcal{D},$$
(20)

which results in $h(\mathbf{x}(t)) \ge C\eta(\mathbf{x}_0)e^{(\mathcal{F}-\mathcal{G}K_\alpha)t} \ge 0$, whenever $h(\mathbf{x}_0) \ge 0$.

If K_{α} is chosen appropriately (see Appendix B.2), a control policy $\mathbf{u} = \pi(\mathbf{x})$ that ensures $\text{CBC}^{(r)} \ge 0$, renders the dynamics (1) safe with respect to set C. Thus, as in (11), we are interested in solving

$$\min_{\mathbf{u}_k} \ \mathbf{u}_k^\top Q \mathbf{u}_k \qquad \text{s.t.} \ \mathbb{P}(\operatorname{CBC}_k^{(r)} \ge \zeta | \mathbf{x}_k, \mathbf{u}_k) \ge \tilde{p}_k.$$
(21)

While we explicitly characterised the distribution of CBC_k for relarive degree one in Lemma 2, finding the distribution of $CBC_k^{(r)}$ for arbitrary r may be a cumbersome task. Instead, a concentration bound can be used to rewrite the chance constraint in terms of moments of $CBC_k^{(r)}$. In particular, using Cantelli's inequality, for any scalar $\lambda < 0$, we have

$$\mathbb{P}\left(\operatorname{CBC}_{k}^{(r)} \geq \mathbb{E}[\operatorname{CBC}_{k}^{(r)}] + \lambda | \mathbf{x}_{k}, \mathbf{u}_{k}\right) \geq 1 - \frac{\operatorname{Var}[\operatorname{CBC}_{k}^{(r)}]}{\operatorname{Var}[\operatorname{CBC}_{k}^{(r)}] + \lambda^{2}}.$$
(22)

If $\mathbb{E}[\operatorname{CBC}_{k}^{(r)}] \geq -\lambda$ we can let $\zeta = \mathbb{E}[\operatorname{CBC}_{k}^{(r)}] + \lambda$. Thus, using (22), the solution of the program,

$$\min_{\mathbf{u}_{k}^{\top}} \mathbf{u}_{k}^{\top} Q \mathbf{u}_{k} \qquad \text{s.t.} \quad \mathbb{E}[\operatorname{CBC}_{k}^{(r)}] \geq -\lambda \quad \text{and} \quad \frac{\operatorname{Var}[\operatorname{CBC}_{k}^{(r)}]}{\operatorname{Var}[\operatorname{CBC}_{k}^{(r)}] + \lambda^{2}} \leq 1 - \tilde{p}_{k}, \quad (23)$$

is also a solution to (21). Solving the program (23) requires the knowledge of the mean and variance of $\text{CBC}_k^{(r)}$. In general, Monte Carlo sampling could be used to estimate this quantities. If $\zeta = 0$, the chance constraint in (23) can be simplified to

$$\mathbb{E}[\operatorname{CBC}_{k}^{(r)}] \ge \sqrt{\frac{\tilde{p}_{k}}{1 - \tilde{p}_{k}} \operatorname{Var}[\operatorname{CBC}_{k}^{(r)}]},$$
(24)

which means the standard deviation of $CBC_k^{(r)}$ should be smaller than the mean by a factor of $\sqrt{\tilde{p}_k/(1-\tilde{p}_k)}$. Thm. 10 in the appendix provides the expressions for mean and variance of $CBC_k^{(2)}$.



Figure 1: **Top left**: Pendulum simulation (left) with an unsafe (red) region. **Top right**: The pendulum trajectory (middle) resulting from the application of safe control inputs (right) is shown. **Bottom row:**Learned vs true pendulum dynamics using matrix variate Gaussian Process regression

7. Simulations

We evaluate the proposed approach on a pendulum with mass m and length l with state $\mathbf{x} = [\theta, \omega]$ and control-affine dynamics $f(\mathbf{x}) = [\omega, -\frac{g}{l}\sin(\theta)]$ and $g(\mathbf{x}) = [0, \frac{1}{ml}]$ as depicted in Fig 1. A safe set is chosen as the complement of a radial region $[\theta_c - \Delta_{col}, \theta_c + \Delta_{col}]$ that needs to be avoided. The controller knows a priori that the system is control-affine with relative degree two, but it is not aware of f and g. The control barrier function is thus $h(\mathbf{x}) = \cos(\Delta_{col}) - \cos(\theta - \theta_c)$. We formulate a quadratically constrained quadratic program as in (23) for r = 2. We specify a task requiring the pendulum to track a reference control signal \mathbf{u}_0 and specify the optimization objective as $(\mathbf{u}_k - \mathbf{u}_0)^{\top}Q(\mathbf{u}_k - \mathbf{u}_0)$. We initialize the system with parameters $\theta_0 = 75^\circ$, $\omega_0 = -0.01$, $\tau = 0.01$, $m = 1, g = 10, l = 1, \theta_c = 45, \Delta_{col} = 22.5$. The system dynamics are approximated accurately (see Fig. 1) while the system remains in the safe region (see Fig. 1). An ϵ -greedy exploration strategy is used to sample $\mathbf{u}_0 \in [-20, 20]$. We use an exponentially decreasing ϵ -greedy scheme going from 1 to 0.01 in 100 steps. Negative control inputs get rejected by the CBF-based constraint, while positive inputs allow the pendulum to bounce back from the unsafe region.

8. Conclusion

Allowing artificial systems to safely adapt their own models during online operation will have significant implications for their successful use in unstructured, changing real-world environments. This paper developed a Bayesian inference approach to approximate system dynamics and their uncertainty from online observations. The posterior distribution over the dynamics may be used to enforce probabilistic constraints that guarantee safe online operation with high probability. Our results offer a promising approach for controlling complex systems in challenging environments. Future work will focus on extending the self-triggering time analysis to systems with higher relative degree and on applications of the proposed approach to real robot systems.

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