

2018

Chapter VI Molecular motors

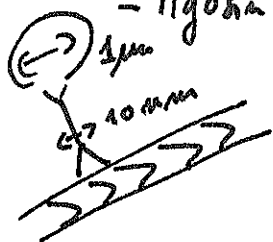
6.1

I) Introduction

Molecular motors are proteins capable of exerting a non-zero average work.

E.g. - kinesin & dynein transport vesicles along microtubules

- Myosin exerts forces on actin filaments.

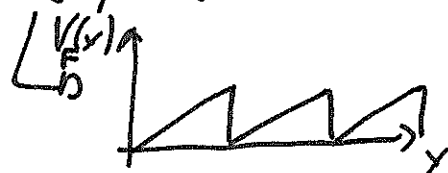


How is it possible? At this scale, temperature equilibrates in $\mu s \Rightarrow$ isothermal motor.

① Spatial symmetry broken because filaments are polar.

If equilibrium $P \propto e^{-\beta V(x)}$

$$J(x) = T \partial_x P + V' \cdot P = 0 \rightarrow \text{no motion}$$



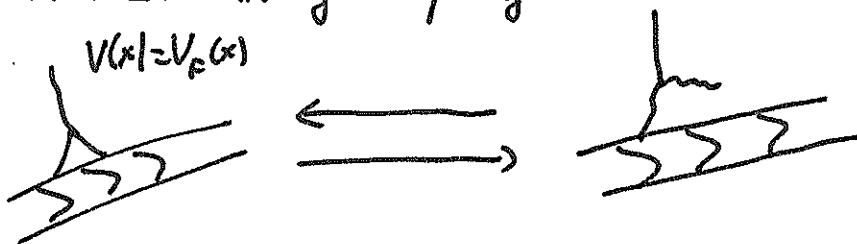
② Two-state model breaks detailed-balance

State 1: strong coupling

State 2: weak coupling

$$V(x) = V_F(x)$$

$$V(x) \approx 0$$



In each state, the dynamics would relax to $e^{-\beta V(x)}$ and hence leads to vanishing current, but the transitions between the states prevent that. Q: how?

II Model and dynamics

Brownian dynamics in each state. Rates ω_1 and ω_2 at which the motor goes from $1 \rightarrow 2$ and from $2 \rightarrow 1$.

$P_i(x, t)$: the proba to find the system in i at time t .

$$P_i(x, t+dt) = \int dy P_i(y, t) \underbrace{P(1, x, t+dt | 1, y, t)}_{\text{states}} + \int dy P_i(y, t) \underbrace{P(1, x, t+dt | 2, y, t)}_{\text{states}}$$

At linear order in dt , only 1 state change is possible, with proba $\omega_i dt$ (a state-change occur with proba $\sim dt^n$)

$$\begin{aligned} \textcircled{1} P(1, x, t+dt | 1, y, t) &= (\text{proba to stay in 1}) \times (\text{proba to go from } y \text{ to } x \text{ in } dt) \\ &= (1 - \omega_1(y)dt + O(dt^2)) \underbrace{P_1(x, t+dt | y, t)}_{\text{because } x-y \sim dt^n} \\ &\quad P_1(x, t | y, t) + dt \partial_x P_1(x, t | y, t) \\ &\simeq (1 - dt H_{FP}^1) \delta(x-y) \\ &\quad \hookrightarrow \text{Fokker-Planck operator in state 1.} \end{aligned}$$

$$P(1, x, t+dt | 1, y, t) \simeq (1 - \omega_1(y)dt - dt H_{FP}^1) \delta(x-y)$$

$$\int dy P_1(y, t) dy \simeq (1 - \omega_1(x)dt - H_{FP}^1 dt) P_1(x, t)$$

$$\begin{aligned} \textcircled{2} P(1, x, t+dt | 2, y, t) &= (\text{proba } 2 \rightarrow 1) \times (\text{proba } y \rightarrow x) \\ &\simeq \omega_2(y)dt (1 - dt H_{FP}^2) \delta(x-y) \simeq \omega_2(y)dt \delta(x-y) \end{aligned}$$

All in all

$$P_i(x, t+dt) = P_i(x, t) - dt (H_{FP}^i + \omega_i(x)) P_i + \omega_i(x) P_j(x, t)$$

$$\Rightarrow \partial_t P_1(x, t) = -H_{FP}^1 P_1(x, t) - \omega_1(x) P_1(x, t) + \omega_2(x) P_2(x, t)$$

$$\partial_t P_2(x, t) = -H_{FP}^2 P_2(x, t) + \omega_1(x) P_1(x, t) - \omega_2(x) P_2(x, t)$$

rate of change of the proba to be in (i, x) at t

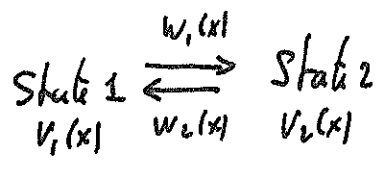
$\hookrightarrow -\nabla \cdot J_i$
dynamics in state i

$\downarrow$
loss/gain due to hop from 1 to 2

$\swarrow$
gain/loss due to hops from 2 to 1.

Switching rates $\omega_i(x)$

Forget space and focus on



Dynamics $\partial_t P_1 = -\omega_1 P_1 + \omega_2 P_2$; $\partial_t P_2 = -\omega_2 P_2 + \omega_1 P_1$

Steady-state $\omega_1 P_1 = \omega_2 P_2$

① Thermally activated switch $\left. \begin{aligned} \omega_1^{th}(x) &= \omega(x) e^{\beta V_1(x)} \\ \omega_2^{th}(x) &= \omega(x) e^{\beta V_2(x)} \end{aligned} \right\} \xrightarrow{\text{steady state}} P_i(x) = \frac{1}{Z_i} e^{-\beta V_i(x)}$

② Chemically activated switch (1), ATP $\leftrightarrow$ (2), ADP + P

~~$\omega_i^{th} = \omega_i(x) e^{\beta V_i(x)}$~~
 $\omega_i^{ch} = \sigma(x) \omega_i^{th}(x) e^{\beta \Delta \mu_{ATP}}$; $\omega_2^{ch} = \sigma(x) \omega_1^{th}(x) e^{\beta \Delta \mu_{ADP} + \beta \Delta \mu_P}$; $\Delta \mu_i = \mu_i - \mu_i^{eq}$
 $\mu_i = \mu_i^{sd} + k_B \ln [i]$

Excess of ATP favors 1 $\rightarrow$ 2
ADP or P $\rightarrow$ 2 $\rightarrow$ 1

If $\Delta \mu_{ATP} \neq \Delta \mu_{ADP} + \Delta \mu_P$ then $\frac{\omega_1^{ch}}{\omega_2^{ch}} \neq \frac{\omega_1^{th}}{\omega_2^{th}} \Rightarrow$ competing steady-states $\rightarrow$ out of equilibrium

③ In practice: both processes $\omega_i(x) = \omega_i^{th}(x) + \omega_i^{ch}(x)$

The Brownian dynamics in state (i) makes $P_i(x,t)$ relax to $e^{-\beta V_i(x)}$ with $J_i = 0$
 $\rightarrow$ compatible with ω_i^{th} but not with ω_i^{ch} if one species is in excess

Comment: as time goes on, $[ATP] \rightarrow [ATP]^{eq}$ and the system relaxes to equilibrium
 $\Rightarrow$ need to maintain $\Delta \mu_i \neq 0$ (food, breath, mitochondria, etc.)

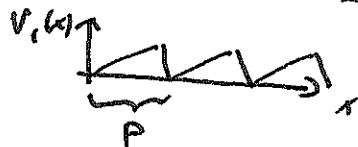
Conclusion: $\Delta \mu_i \neq 0$ drives the system out of equilibrium $\Rightarrow$ is there a current?

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III A simple example [Jülicher, Ajdari, Prost; RMP 69, 1269 (1997)]

$V_2 = 0$, ω , $d\omega_2$ constant, $V_1(x)$ periodic with period p



Dynamics: $\partial_t P_i(x,t) = \frac{\partial}{\partial x} \left[T \frac{\partial}{\partial x} + V_1'(x) \right] P_i - \omega_i P_i(x) + \omega_2 P_2(x)$

$$\partial_t P_2(x,t) = \frac{\partial}{\partial x} \left[T \frac{\partial}{\partial x} + V_2'(x) \right] P_2 + \omega_1 P_1(x) - \omega_2 P_2(x)$$

$$P_{\text{tot}}(x) = P_1(x) + P_2(x)$$

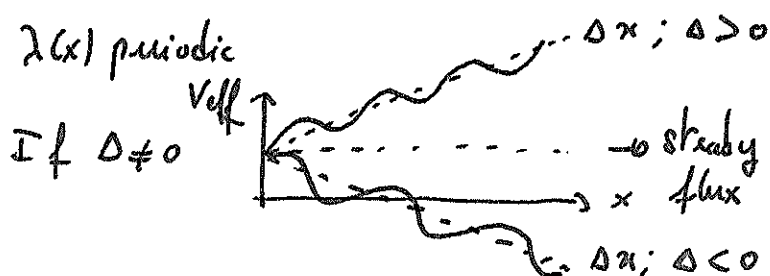
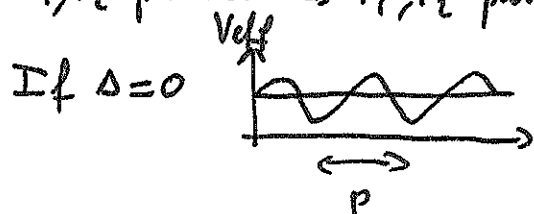
$$\partial_t P_{\text{tot}}(x) = T \partial_{xx} P_{\text{tot}} + \partial_x [V_1'(x) P_1(x)] = T \partial_{xx} P_{\text{tot}} + \partial_x [V_{\text{eff}}'(x) P_{\text{tot}}(x)]$$

where $V_{\text{eff}}'(x) = \lambda(x) V_1'(x)$, with $\lambda(x) = \frac{P_1(x)}{P_{\text{tot}}(x)}$

Brownian dynamics in an effective potential $V_{\text{eff}}(x) = V_{\text{eff}}(0) + \int_0^x du \lambda(u) V_1'(u)$

let $\Delta = \int_0^p dx \lambda(x) V_1'(x)$

V_1, V_2 periodic $\Rightarrow P_1, P_2$ periodic $\Rightarrow \lambda(x)$ periodic



What is the condition for $\Delta = 0$?

$$\rightarrow \text{If } V_1(x) = V_1(-x) \Rightarrow P_1, P_2 \text{ even} \Rightarrow \lambda(x) = \lambda(-x) \left. \vphantom{\begin{matrix} \Rightarrow \lambda(x) = \lambda(-x) \\ \Rightarrow V_1'(x) \text{ odd} \end{matrix}} \right\} \lambda(x) V_1'(x) \text{ odd} \Rightarrow \Delta = 0$$

$\Rightarrow$ Otherwise, $\Delta \neq 0$ generically $\Rightarrow$ current.

Comment: $\partial_t P_i = T \partial_{xx} P_i + \partial_x (V_1' P_i)$ satisfies DB with respect to $P_i \propto e^{-\beta V_1}$

$$\partial_t P_2 = T \partial_{xx} P_2$$

$$\partial_t P_i = -\omega_i P_i + \omega_j P_j$$

$P_i \propto \text{Constant}$

$$\frac{P_i}{P_j} = \frac{\omega_j}{\omega_i}$$

All together $\Rightarrow$ the competition between the $\neq$ steady-state drives the system out of equilibrium.

2018] IV Collective behaviours of molecular motors

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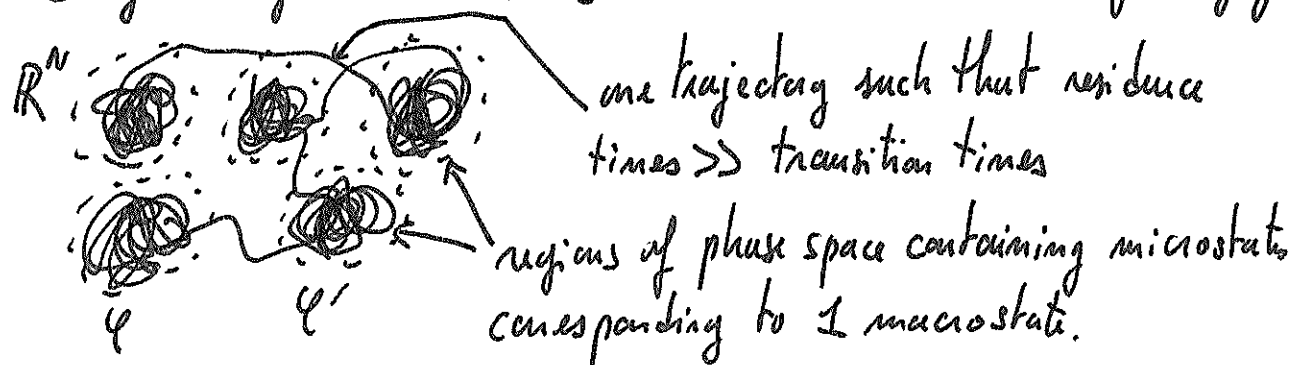
1 motor = 1 ratchet

N motors = N coupled ratchets $\Rightarrow$ horribly complicated...

Idea: coarse-graining the many microstates describing one motor bound to a given site into one macrostate

All the trajectories leading to the next site then yield one transition rate.

Langevin dynamics in $\mathbb{R}^N \Rightarrow$ Markov chain on a set of configurations.



$$\int_{\mathcal{Q}} dx_i \int_{\mathcal{Q}'} dx_j P(x_i, t + dt | x_j, t) \equiv \underbrace{W(q' \rightarrow q)}_{\text{transition rate}} dt$$

Current: in practice the projection from $\mathbb{R}^N$ to $\{q\}$ is very difficult.

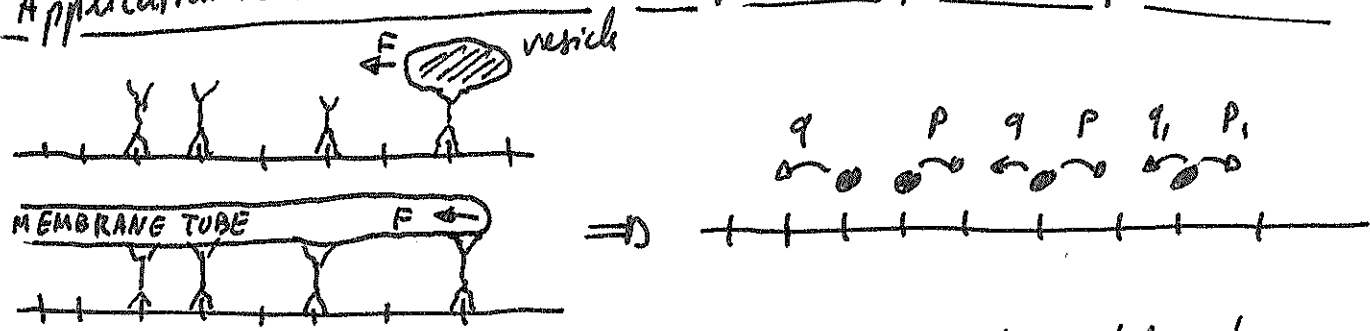
Model: Set of configurations $\{q\}$ and transition rates between them.

$$\begin{aligned} P(q, t + dt) &= P(q, t) \times (\text{prob to stay in } q \text{ in } [t, t + dt]) + \sum_{q' \neq q} P(q', t) \times (\text{prob to go from } q' \text{ to } q) \\ &= P(q, t) \times (1 - \sum_{q' \neq q} W(q \rightarrow q') dt) + \sum_{q' \neq q} P(q', t) W(q' \rightarrow q) dt + \mathcal{O}(dt^2) \end{aligned}$$

Master equation:

$$\frac{\partial P(q)}{\partial t} = \sum_{q' \neq q} W(q' \rightarrow q) P(q', t) - \sum_{q' \neq q} W(q \rightarrow q') P(q)$$

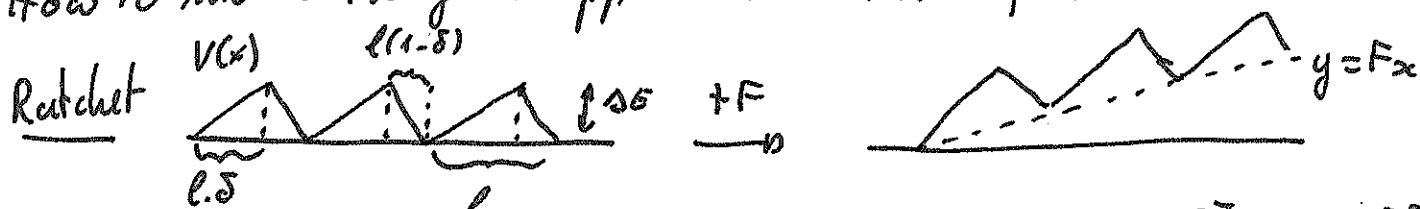
Application to molecular motors: The asymmetric simple exclusion process (ASEP) [6.6]



[MacDonald, Gibbs, Diphin, Biopolymers 6, 1-25, 1965] to model ribosomes along DNA.

Particles hop at constant rates onto free sites.

How to model the force applied to the ~~first~~ first motor?



Energy barrier ΔE : forward $p \propto e^{-\beta \Delta E} \Rightarrow p_1 \propto e^{-\beta [\Delta E + F \cdot \delta l]} = p e^{-\beta F \delta l}$
 backward $q \propto e^{-\beta \Delta E} \Rightarrow q_1 \propto e^{-\beta [\Delta E - F(1-\delta)l]} = q e^{+(1-\delta)\beta F l}$

Too many letters $\Rightarrow$ units such that $\beta F l = f$.

IV.1 Isolated motor and stall force

On average, p_1 jumps to the right per unit of time
 q_1 ——— left ——— } average speed $v^{(1)} = p_1 - q_1$

Simple proof: $i(t)$ position of the motor at time t .

$$\langle i(t) \rangle = \sum_j j P(i(t)=j) \Rightarrow \partial_t \langle i(t) \rangle = \sum_j j \partial_t P(i(t)=j)$$

very cumbersome, we simply write $P(j)$

Master eq^o $\partial_t P(q) = \sum_{q'} W(q' \rightarrow q) P(q') - W(q \rightarrow q') P(q)$

Here $q \leftrightarrow j$

Identify all pairs q, q' such that $W(q \rightarrow q') \neq 0$ or $W(q' \rightarrow q) \neq 0$

$$q \leftrightarrow j, q' \leftrightarrow j \pm 1.$$

$$\begin{aligned} \partial_t P(j, t) &= W(j-1 \rightarrow j) P(j-1) + W(j+1 \rightarrow j) P(j+1) - [W(j \rightarrow j-1) + W(j \rightarrow j+1)] P(j) \\ &= p_1 P(j-1) + q_1 P(j+1) - (p_1 + q_1) P(j) \end{aligned}$$

$$\begin{aligned}
 \partial_\epsilon \langle j \rangle &= \sum_j j p_j P(j-1) + j q_j P(j+1) - j(p_1 + q_1) P(j) \\
 &= \sum_h (h+1) p_1 P(h) + \sum_h (h-1) q_1 P(h) - \sum_h h (p_1 + q_1) P(h) \\
 &= (p_1 - q_1) \sum_h P(h) = (p_1 - q_1) \Rightarrow \langle j(\epsilon) \rangle - \langle j(0) \rangle = (p_1 - q_1) \epsilon \\
 \Rightarrow v_1^n &= p_1 - q_1
 \end{aligned}$$

Stall force F such that $v_1^n(F) = 0 \Leftrightarrow p_1 = q_1 \Leftrightarrow p e^{-\delta f} = q e^{(1-\delta)f}$

$$\Leftrightarrow \boxed{f = \ln \frac{p}{q}}$$

Comment: f does not depend on δ since only the work along a full period matters.

IV.2) Two motors

We allow for short-range interactions between motors

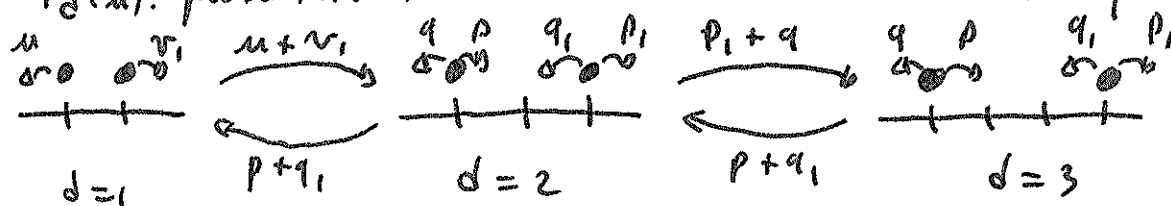


$v_1 > p_1$ & $u > q \Rightarrow$ repulsive interactions

$v_1 < p_1$ & $u < q \Rightarrow$ attractive

IV.2.1) Average distance between two motors

$P_d(k)$: proba that the distance between the motors is equal to k .



$$\partial_\epsilon P_d(1) = (p + q_1) P_d(2) - (u + v_1) P_d(1) \quad (1)$$

$$\begin{aligned}
 \partial_\epsilon P_d(2) &= (u + v_1) P_d(1) - (p + q_1) P_d(2) \\
 &\quad - (p_1 + q) P_d(2) + (p + q_1) P_d(3)
 \end{aligned} \quad (2)$$

...

$$\begin{aligned}
 \partial_\epsilon P_d(m) &= (p_1 + q) P_d(m-1) - (p + q_1) P_d(m) \\
 &\quad - (p_1 + q) P_d(m) + (q_1 + p) P_d(m+1)
 \end{aligned} \quad (m)$$

2018 Steady-state $\partial_t P_d(i) = 0; \forall i$

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$$(1) \Rightarrow P_d(2) = \frac{\mu + v_1}{p + q_1} P_d(1) \equiv r, P_d(1); \quad r = \frac{\mu + v_1}{p + q_1}$$

$$(1+2) \Rightarrow P_d(3) = \frac{p_1 + q}{p + q_1} P_d(2) \equiv r P_d(2) = r^2 P_d(1); \quad r = \frac{p_1 + q}{p + q_1}$$

$$(1+\dots+n) \Rightarrow P_d(n+1) = r P_d(n) = \dots = r^{n-1} r_1 P_d(1) \Rightarrow P_d(n \geq 2) = r^{n-2} r_1 P_d(1)$$

Normalisation: $\sum_{k=1}^{\infty} P_d(k) = 1 = P_d(1) + r P_d(1) + \dots = P_d(1) \left[1 + r + \sum_{k=2}^{\infty} r^{k-1} \right] = P_d(1) \left(1 + \frac{r}{1-r} \right)$

$$\Rightarrow \boxed{P_d(1) = \frac{1-r}{1-r+r_1}; \quad P_d(k \geq 2) = \frac{r_1(1-r)}{1-r+r_1} r^{k-2}}$$

Comment: $p_1 < p$ & $q_1 > q \Rightarrow r = \frac{p_1 + q}{p + q_1} < 1$; otherwise, no stationary state.

Comment: $P_d(k)$ decreases as $r^k \propto e^{k \ln r} \xrightarrow{\ln r < 0} \Rightarrow \langle k \rangle$ finite, of order $\frac{1}{|\ln r|}$

The mean distance between the motors is finite $\Rightarrow$ they go at the same speed.

IV.2.2) Mean speed of the first motor

$$\begin{aligned} \langle v \rangle &= v_{\text{isolated}} \cdot p(\text{isolated}) + v_1 P_d(1) = (p_1 - q_1) [1 - P_d(1)] + v_1 P_d(1) \\ &= \frac{(p_1 - q_1)(\mu + v_1)}{p + q_1 - p_1 - q + \mu + v_1} + \frac{v_1(p + q_1 - p_1 - q)}{p + q_1 - p_1 - q + \mu + v_1} \\ &= \frac{\mu(p_1 - q_1) + v_1(p - q)}{p + q_1 - p_1 - q + \mu + v_1} \equiv V^{2M} \end{aligned}$$

Stall force: $V^{2M} = 0 = \mu e^{-\delta f} (p - q e^f) + v e^{-\delta f} (p - q)$

$$\Rightarrow \mu q e^f = \mu p + v p - v q$$

$$f_s^{2M} = \ln \left[\frac{vp}{\mu q} + \frac{p}{q} - \frac{v}{\mu} \right] = \ln \left[\frac{p}{q} + \frac{v}{\mu} \left(\frac{p}{q} - 1 \right) \right] \stackrel{>0}{>} f_s^{1M}$$

The force to stop two motors is always larger because the 2nd motor prevents the first one from stepping backward.

Comment: $f_s^{2M} = 2 f_s^{1M} \Leftrightarrow \ln \left(\frac{p}{q} + \frac{v}{\mu} \frac{p}{q} - \frac{v}{\mu} \right) = \ln \frac{p}{q^2}$

$\Leftrightarrow \frac{v}{\mu} \left(1 - \frac{p}{q} \right) = \frac{p}{q} \left(1 - \frac{p}{q} \right) \Leftrightarrow \frac{p}{q} = \frac{v}{\mu}$

If interactions derive from (free) energy $\left. \begin{array}{l} v = p e^{-\beta \phi} \\ \mu = q e^{-\beta \phi} \end{array} \right\} \frac{p}{q} = \frac{v}{\mu}$

Then one needs twice the force to stop two motors.

Comment: The second motor always increase the stall force, but not always the speed $\Rightarrow$ possible to have $V^{2M} < V^{1M}$.

$$V^{2M} - V^{1M} = \frac{\mu(p_1 - q_1) + v_1(p - q)}{p - q + \mu + v_1 - (p_1 - q_1)} - \frac{(p_1 - q_1)(p - q + \mu + v_1 - (p_1 - q_1))}{p - q + \mu + v_1 - (p_1 - q_1)} \equiv \frac{Num}{Den}$$

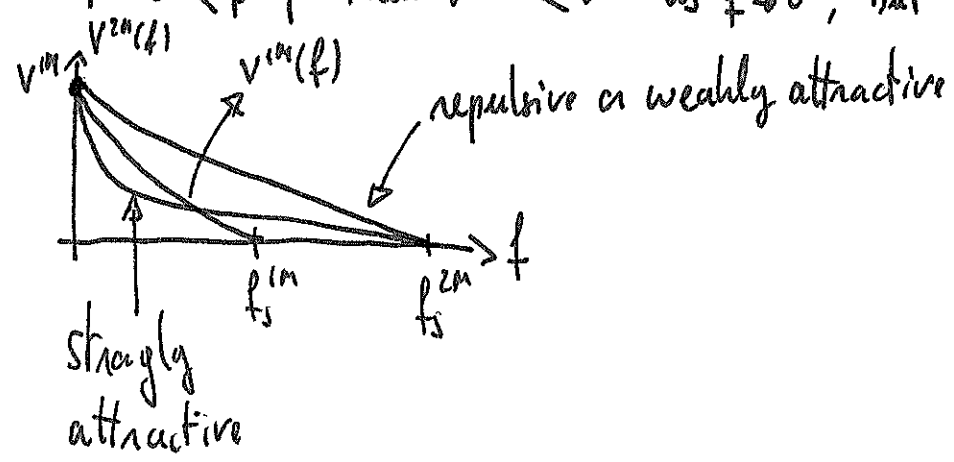
$Den = p(1 - e^{-\delta f}) + q[e^{(1-\delta)f} - 1] + \mu + v_1 > 0$

$Num = v_1[p - q - p_1 + q_1] - (p_1 - q_1)[p - p_1 + q_1 - q] = (v_1 - p_1 + q_1) \underbrace{(p - p_1 + q_1 - q)}_{> 0 \text{ if } f > 0}$

Comment: $f \rightarrow 0$, $V^{2M} = V^{1M}$, motors are unbound.

$f > 0$ if $v_1 > (p_1 - q_1)$ then $V^{2M} > V^{1M}$
 $\Leftrightarrow v > p - q e^f$

If $v < p - q$ then $V^{2M} < V^{1M}$ as $f \rightarrow 0$; but $V^{2M} > V^{1M}$ if $f = f_s^{1M} = \ln \frac{p}{q}$



V Detailed balance for Markov chains

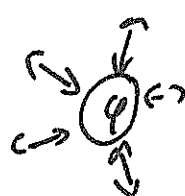
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① At the rates level

$$\partial_t P(q) = \sum_{q' \neq q} W(q' \rightarrow q) P(q') - W(q \rightarrow q') P(q)$$

Steady-state: $\sum_{q' \neq q} W(q' \rightarrow q) P_s(q') = \sum_{q' \neq q} W(q \rightarrow q') P_s(q)$

Global balance in and out of q



The sum of outward proba flux (r.h.s) is balanced by the sum of inward proba flux (l.h.s.)

Detailed-balance: $\boxed{\forall q, q' \quad W(q \rightarrow q') P(q) = W(q' \rightarrow q) P(q')}$

The fluxes are balanced along each link.

② At the trajectory level

Escape rate: $\lambda(q) = \sum_{q' \neq q} W(q' \rightarrow q)$ is the total rate at which the system hops out of configuration q .

Escape time: τ , the time at which the system first escape from q .

$\tau = N \Delta t$, in the limit $\Delta t \rightarrow 0$, $N \rightarrow \infty$, τ constant

Proba ($q \rightarrow q'$ during Δt) = $W(q \rightarrow q') \Delta t$

Proba (out of q —) = $\sum_{q'} W(q \rightarrow q') \Delta t$

Proba (stay in q —) = $1 - \sum_{q'} W(q \rightarrow q') \Delta t$

$$P(\tau) d\tau = \underbrace{\left(1 - \sum_{q'} W(q \rightarrow q') \Delta t\right)^{N-1}}_{\text{stays in } q \text{ for } [0, (N-1)\Delta t]} \times \underbrace{\sum_{q'} W(q \rightarrow q') \Delta t}_{\text{exits in } [(N-1)\Delta t, N\Delta t]} \approx (1 - \lambda(q) \Delta t)^{N-1} \lambda(q) \Delta t$$

$$\approx e^{-(N-1)\Delta t \lambda(q)} \lambda(q) \Delta t \sim \lambda(q) \Delta t e^{-\tau \lambda(q)}$$

$$\boxed{P(\tau) = \lambda(q) e^{-\tau \lambda(q)}}$$

Comment: $P(\tau > t) = \int_t^\infty d\tau P(\tau) = e^{-t \lambda(q)}$

When the jumps occurs, the probability to go from q to q' is

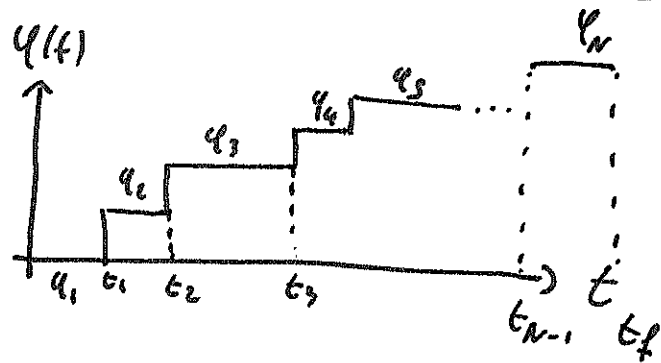
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$$\frac{w(q \rightarrow q')}{\sum_{q''} w(q \rightarrow q'')} = \frac{w(q \rightarrow q')}{r(q)}$$

probability of a trajectory:

Start from q_1 in steady-state

$\rightarrow q_N$ at t_f .



$$P(\{q\}) = P_{ss}(q_1) r(q_1) e^{-\lambda(q_1)t_1} \frac{w(q_1 \rightarrow q_2)}{r(q_1)} \cdot r(q_2) e^{-\lambda(q_2)(t_2-t_1)} \frac{w(q_2 \rightarrow q_3)}{r(q_2)} \dots \frac{w(q_{N-1} \rightarrow q_N)}{r(q_{N-1})} \times e^{-(t_f-t_N)\lambda(q_N)}$$

If there is detailed balance, $P_{ss}(q_i) W(q_i \rightarrow q_{i+1}) = P_{ss}(q_{i+1}) W(q_{i+1} \rightarrow q_i)$

$$P(\{q\}) = e^{-\lambda(q_1)t_1} \left(\frac{w(q_1 \rightarrow q_2)}{r(q_1)} r(q_2) e^{-(t_2-t_1)\lambda(q_2)} \right) \times \left(\frac{w(q_2 \rightarrow q_3)}{r(q_2)} r(q_3) e^{-(t_3-t_2)\lambda(q_3)} \right) \times \dots \frac{w(q_N \rightarrow q_{N-1})}{r(q_N)} \cdot r(q_N) e^{-\lambda(q_N)(t_f-t_N)} P_{ss}(q_N) = P(\{q | t_f-t\})$$

Forward & backward trajectories have the same probability.

Summing over all intermediate steps $P_{ss}(q_1) \cdot P(q_N, t_f | q_1, 0) = P_{ss}(q_N) P(q_1, t_f | q_N, 0)$

③ At the transition matrix level

Vector $|P\rangle$ of dimension $\# \{q\}$; the i^{th} component $P_i = P(q_i, t) = P_q(t)$

$$\partial_t P(q, t) = \sum_{q' \neq q} W(q' \rightarrow q) P(q', t) - \left(\sum_{q' \neq q} W(q \rightarrow q') \right) P(q, t) \Leftrightarrow \partial_t P_q = \sum_{q'} M_{qq'} P_{q'}$$

$$M_{q, q' \neq q} = W(q' \rightarrow q) ; M_{qq} = - \sum_{q' \neq q} W(q \rightarrow q')$$

$$\Leftrightarrow \partial_t |P\rangle = M |P\rangle$$

like a Fokker-Planck equation!
in finite dimension

Detailed balance

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$$\forall q \neq q' \quad P(q)W(q \rightarrow q') = P(q')W(q' \rightarrow q)$$

$$\Leftrightarrow M_{q'q} P_q = M_{qq'} P_{q'}$$

$$\Leftrightarrow M_{qq'}^+ = P_q^{-1} M_{qq'} P_{q'}$$

$$\Leftrightarrow \boxed{M^+ = P^{-1} M P} ; \text{ where } P = \text{diag}(P_q)$$

$$\text{But also } P_q^{-1/2} M_{qq'} P_{q'}^{1/2} = P_{q'}^{-1/2} M_{q'q} P_q^{1/2} =$$

$$\text{If } D = \text{diag}(P_q^{1/2}) \quad \tilde{M} = D^{-1} M D \text{ is such that } (\tilde{M})_{qq'}^+ = \tilde{M}_{qq'}$$

$\tilde{M}$ is hermitian $\Rightarrow$ orthogonal eigenbasis (unlike M)

$\Rightarrow$ real spectrum (like M)