

# Occam's Razor and Alphabet Soup:

What anisotropic elastic parameters can we reasonably measure in borehole seismic experiments?

Douglas E. Miller

Schlumberger-Doll Research

*MIT-ERL Friday Informal Seminar Hour*

*October 21, 2005*

# Occam's Razor and Alphabet Soup:

What anisotropic elastic parameters can we reasonably measure in borehole seismic experiments?

*Entities are not to be multiplied beyond necessity*

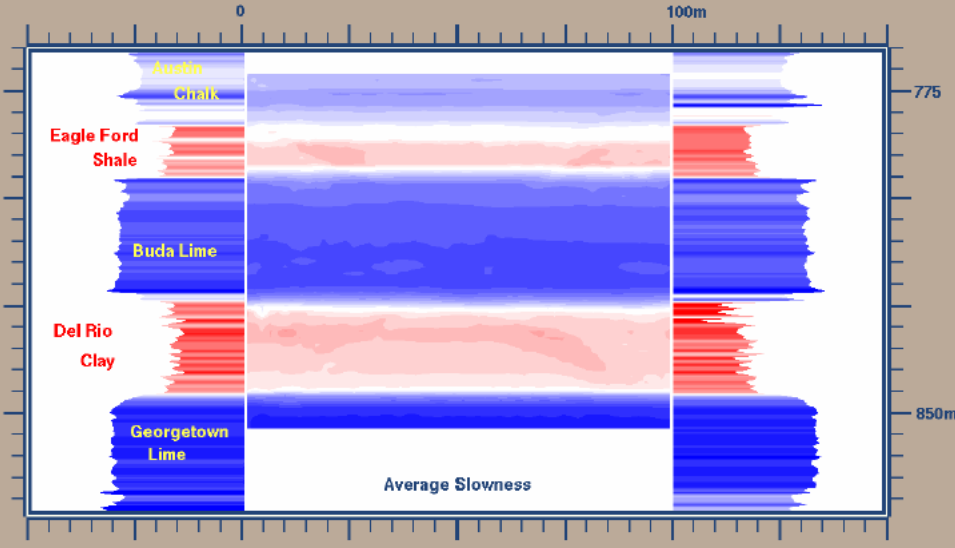
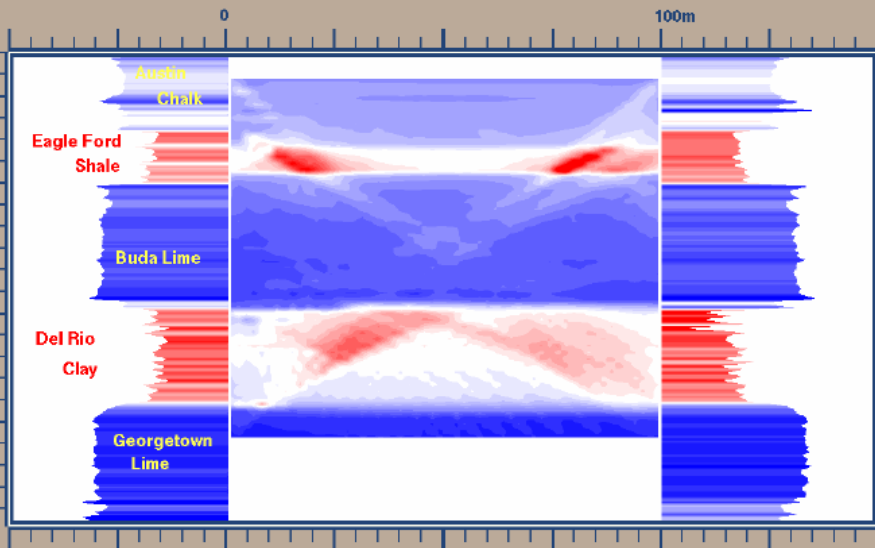
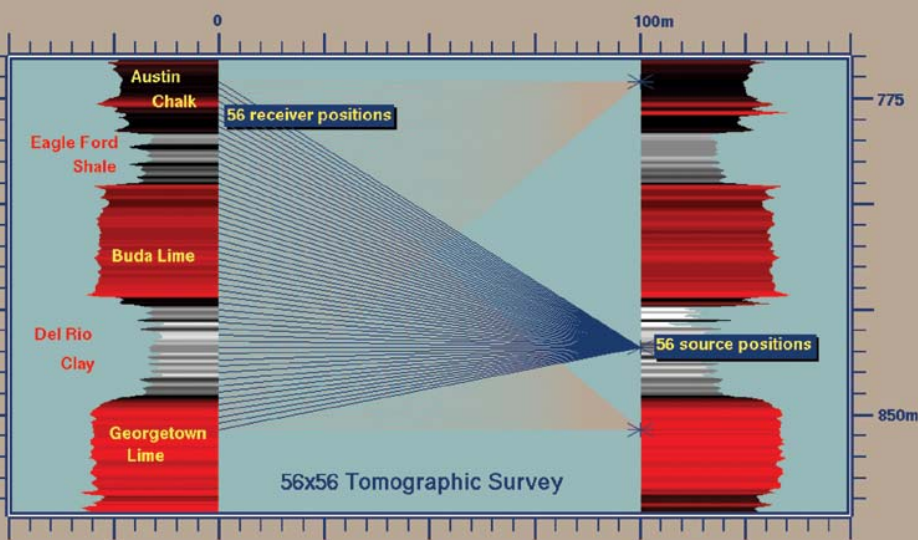
- William of Ockham as paraphrased by John Ponce of Cork.

*Entities must not be reduced to the point of inadequacy*

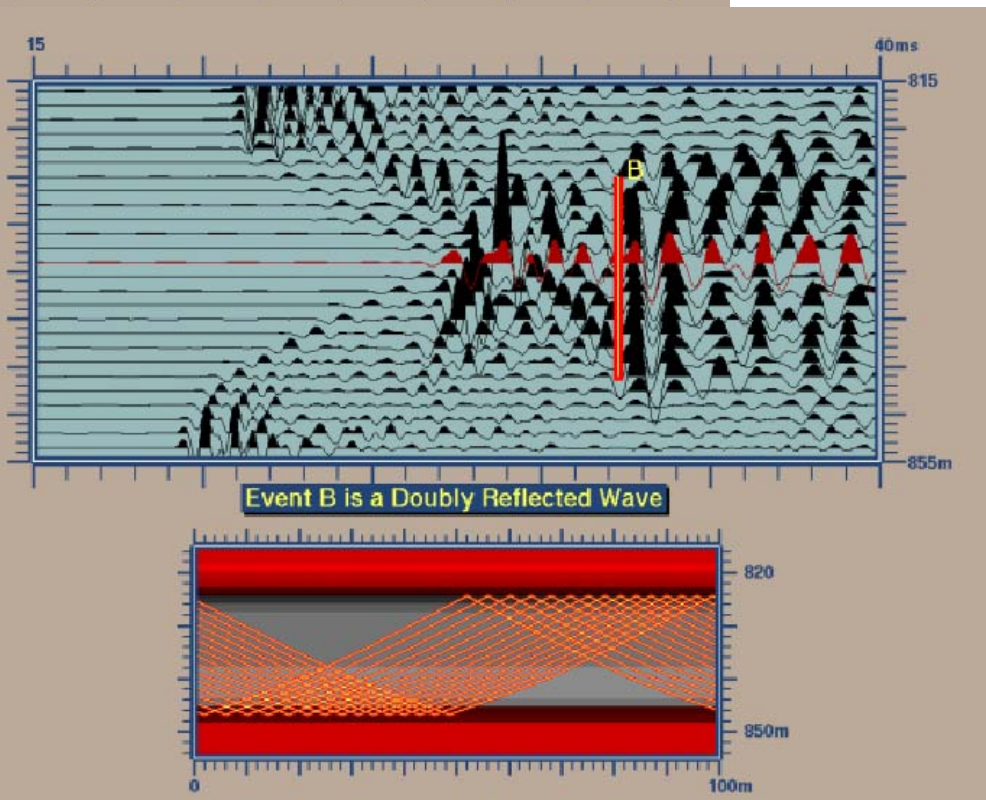
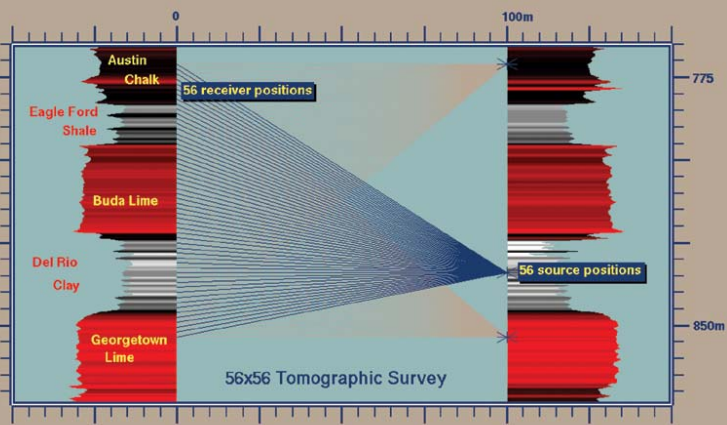
- Walter of Chatton as paraphrased by Karl Menger.

# Crosswell Seismic Example

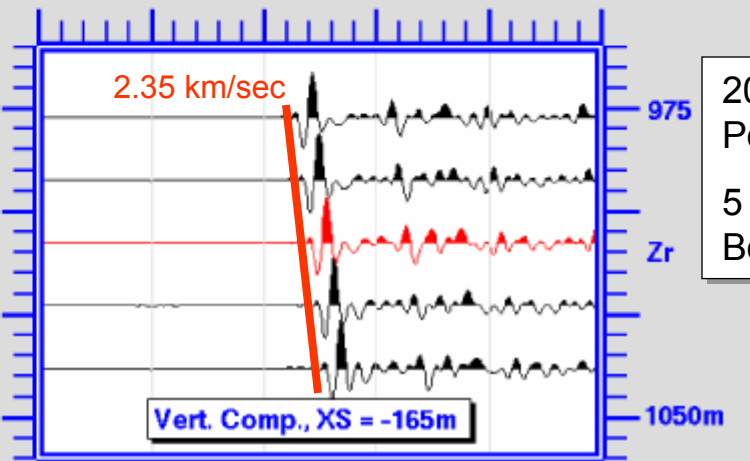
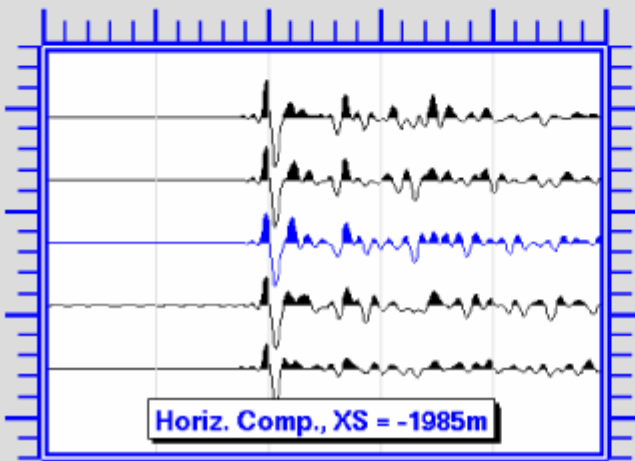
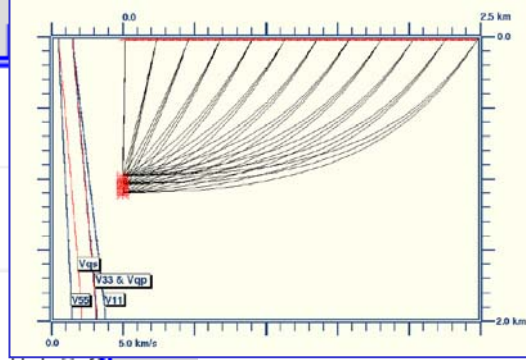
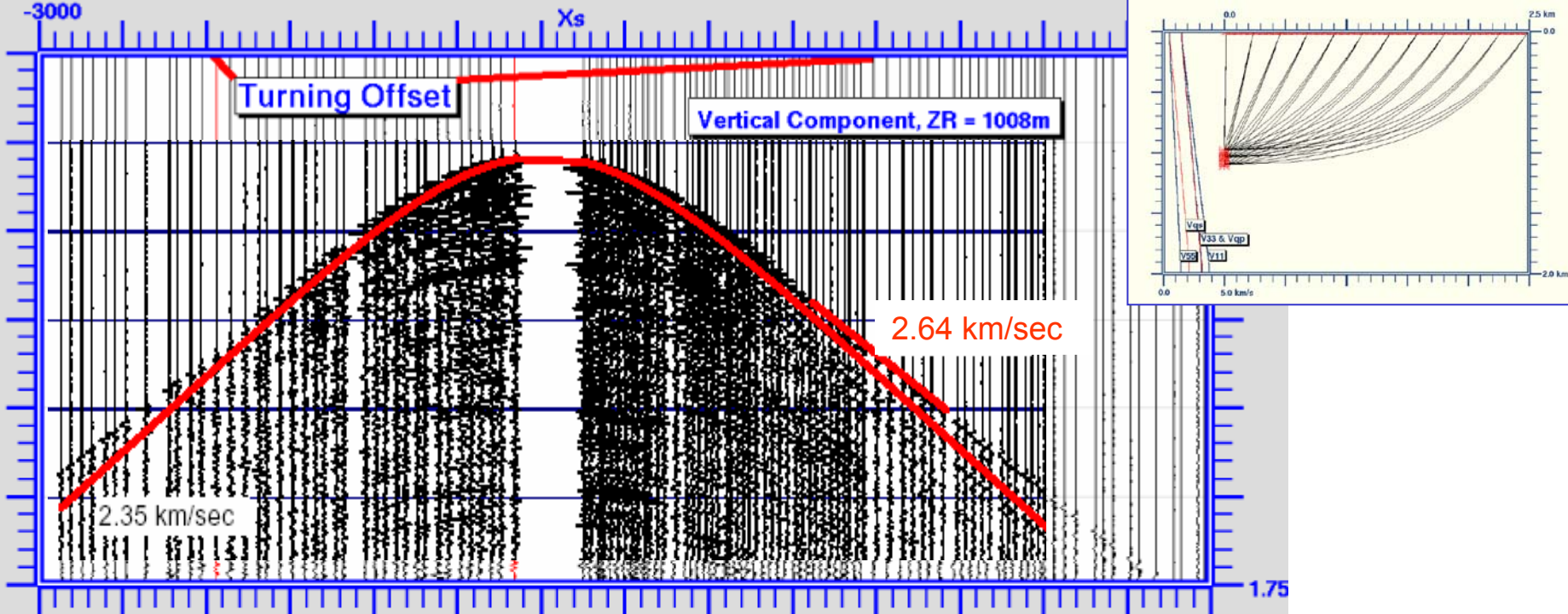
- Anisotropic Solution with 53x3 parameters
- Isotropic Solution with 56x56 parameters
- Similar (good) fit to data



# Crosswell Seismic Example



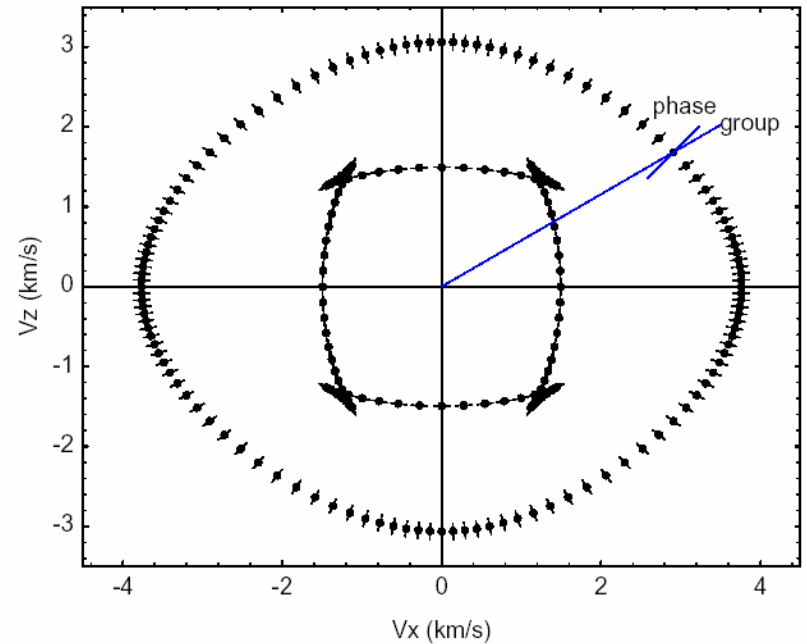
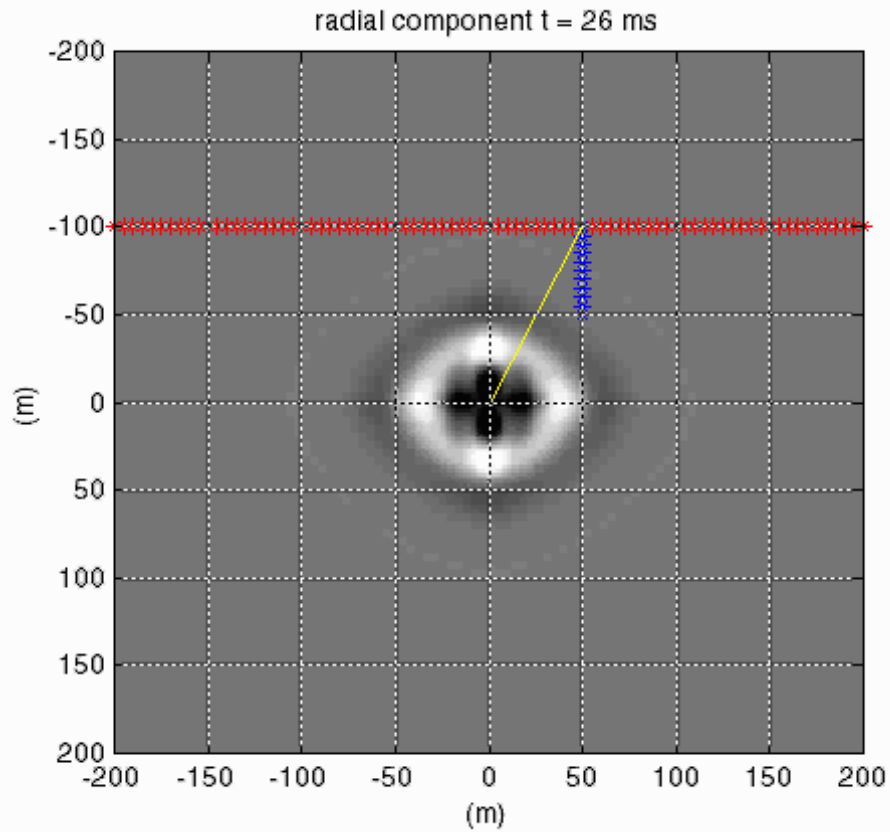
- The anisotropic solution is a good predictor of other coherent arrivals. The isotropic solution is not.
- Conclusion: The shales are anisotropic.

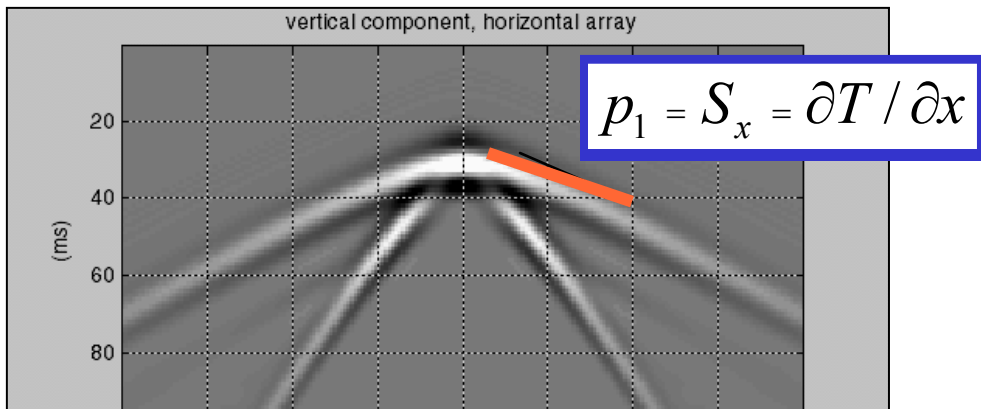


201 Source Positions  
5 3-Component Borehole receivers

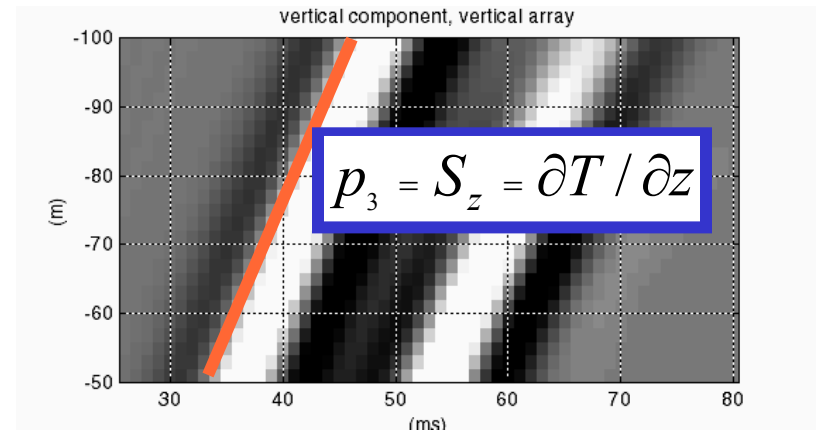
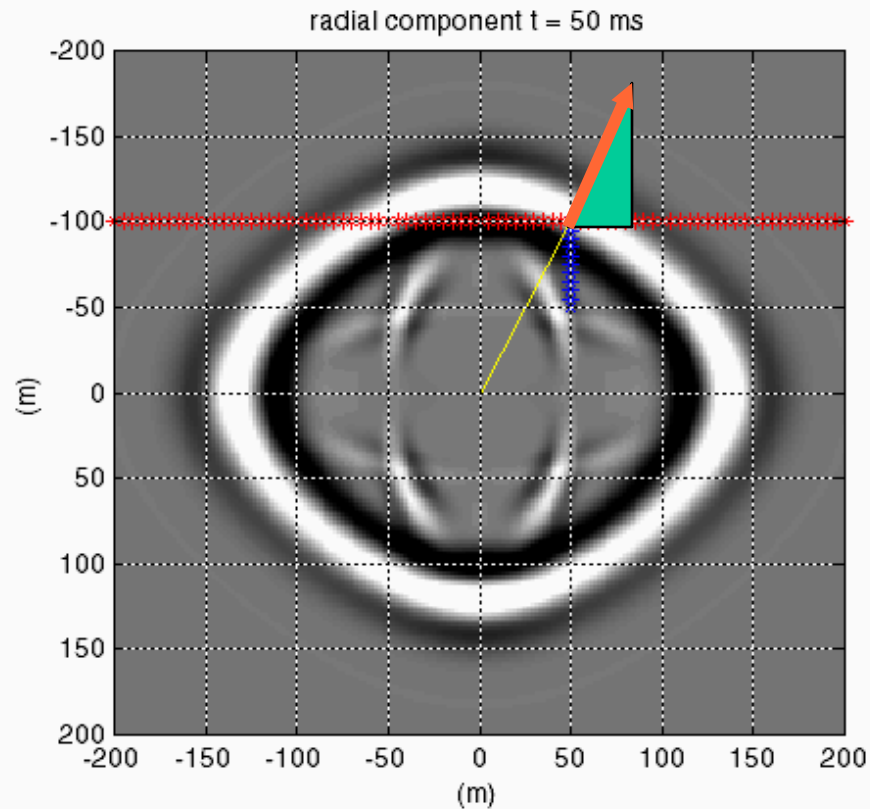
# 5 Walkaway VSP Example

# Anisotropy 101





The spatial gradient of the traveltime function is the Phase Slowness Vector

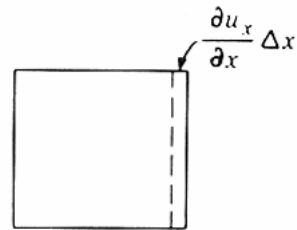




# Hooke's Law

- isotropic

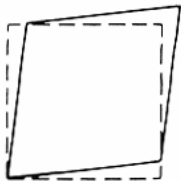
$$\begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{33} \\ \sigma_{12} \\ \sigma_{13} \\ \sigma_{23} \end{bmatrix} = \begin{bmatrix} \lambda + 2\mu & \lambda & \lambda & & & \\ \lambda & \lambda + 2\mu & \lambda & & & \\ \lambda & \lambda & \lambda + 2\mu & & & \\ & & & \mu & & \\ & & & & \mu & \\ & & & & & \mu \end{bmatrix} \begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{33} \\ \epsilon_{12} \\ \epsilon_{13} \\ \epsilon_{23} \end{bmatrix}$$



(b) Simple extension

To achieve a unit of pure longitudinal strain along the 1-axis:

- Pull *left-right* with traction  $\lambda + 2\mu$
- Pull *up-down, in-out* with traction  $\lambda$



(e) Pure shear

To achieve a unit of pure shear strain:

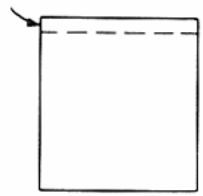
- Squeeze opposite corners with differential traction  $\mu$



# Hooke's Law

- TIV - rotational symmetry around 3-axis

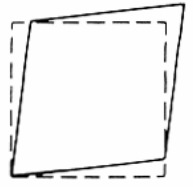
$$\begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{33} \\ \sigma_{12} \\ \sigma_{13} \\ \sigma_{23} \end{bmatrix} = \begin{bmatrix} c_{1111} & c_{1111} - 2c_{1212} & c_{1133} & & & \\ c_{1111} - 2c_{1212} & c_{1111} & c_{1133} & & & \\ c_{1133} & c_{1133} & c_{3333} & & & \\ & & & c_{1313} & & \\ & & & c_{1313} & & \\ & & & & & c_{1212} \end{bmatrix} \begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{33} \\ \epsilon_{12} \\ \epsilon_{13} \\ \epsilon_{23} \end{bmatrix}$$



(b) Simple extension

To achieve a unit of pure longitudinal strain along the 3-axis:

- Pull *up-down* with traction  $c_{3333}$
- Pull *left-right, in-out* with traction  $c_{1133}$



(e) Pure shear

To achieve a unit of pure 13 shear strain:

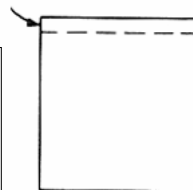
- Apply 13 traction  $c_{1313}$

# Hooke's Law: Reduced (Voigt) Notation

- TIV - rotational symmetry around 3-axis

$$\begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \\ \sigma_4 \\ \sigma_5 \\ \sigma_6 \end{bmatrix} = \begin{bmatrix} c_{11} & c_{11} - 2c_{66} & c_{13} & & & \\ c_{11} - 2c_{66} & c_{11} & c_{13} & & & \\ c_{13} & c_{13} & c_{33} & & & \\ & & & c_{44} & & \\ & & & & c_{44} & \\ & & & & & c_{66} \end{bmatrix} \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \epsilon_3 \\ \epsilon_4 \\ \epsilon_5 \\ \epsilon_6 \end{bmatrix}$$

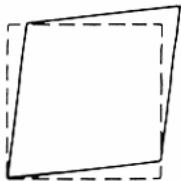
11	22	33	32 = 23	31 = 13	12 = 21
↓	↓	↓	↓	↓	↓
1	2	3	4	5	6



(b) Simple extension

To achieve a unit of pure longitudinal strain along the 3-axis:

- Pull *up-down* with traction  $c_{33}$
- Pull *left-right, in-out* with traction  $c_{13}$



(e) Pure shear

To achieve a unit of pure 13 shear strain:

- Apply 13 traction  $c_{55}$

# Christoffel (Dispersion) Relation

HL +  $F = ma + \mathbf{u} = \hat{\mathbf{g}} e^{i\omega(\mathbf{p}\cdot\mathbf{x}-t)}$  gives the Christoffel (Eigenvalue) Equation:

$$[p_i p_l c_{ijkl} - \rho \delta_{jk}] \hat{g}_k = 0$$

- A solution exists when  $Det(matrix) = 0$ . This is the **Christoffel Relation** that implicitly defines the phase slowness surface:

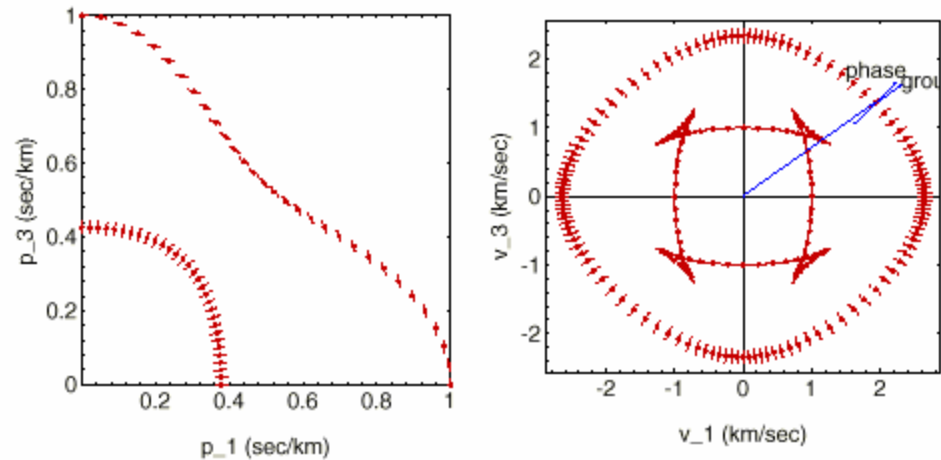
$$\mathcal{S} = \{\mathbf{p} : |[p_i p_l c_{ijkl} - \rho \delta_{jk}]| = 0\}$$

- 

$$a_{ijkl} = c_{ijkl} / \rho$$

$$A_{11} = a_{xxxx}, A_{13} = a_{xxzz}, A_{55} = a_{zzzz}, \dots$$

N.B.:  $A_{ij}$  have units of velocity<sup>2</sup>



## Dispersion Relation:

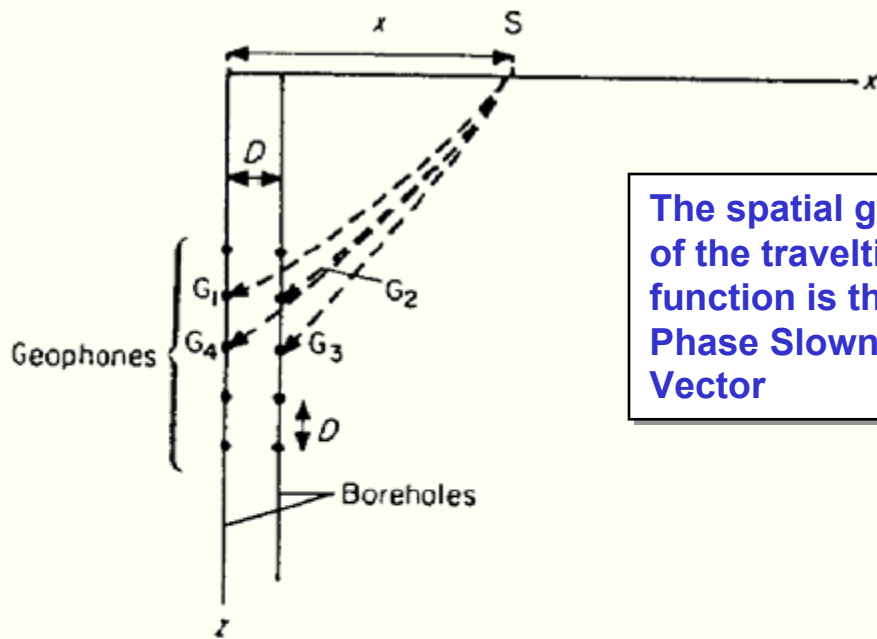
$$A_{11}A_{55}p_1^4 + A_{33}A_{55}p_3^4 + Ap_1^2p_3^2 - (A_{11} + A_{55})p_1^2 - (A_{33} + A_{55})p_3^2 + 1 = 0$$

$$A = A_{11}A_{33} + A_{55}^2 - (A_{13} + A_{55})^2$$

$$\mathbf{p} \cdot \mathbf{v} = 1$$

N.B.: Given  $A_{ij}$ 's and  $p_1$ , this yields a quadratic equation for  $(p_3)^2$

# White, et al., 1983



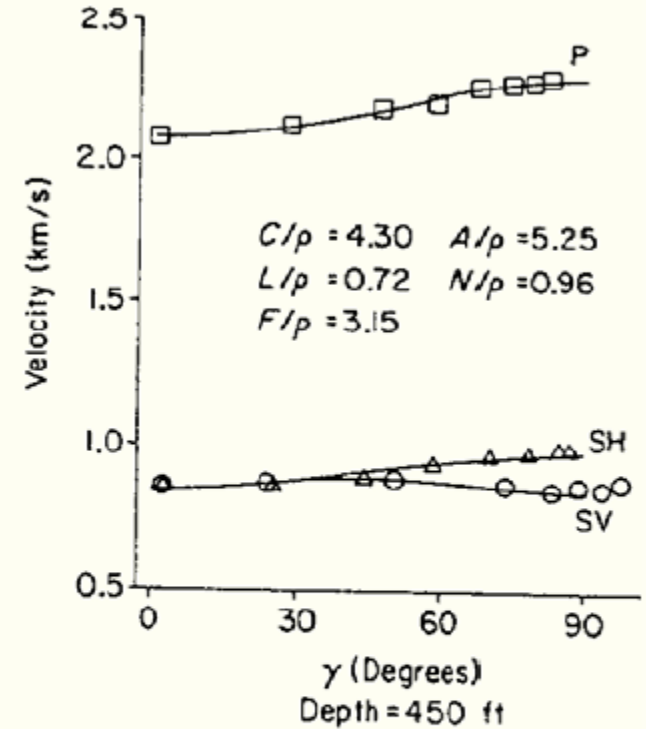
The spatial gradient of the travelttime function is the Phase Slowness Vector

$$\Delta t_h = (t_1 - t_2 + t_4 - t_3)/2,$$

$$\Delta t_v = (t_3 - t_2 + t_4 - t_1)/2.$$

$$V_h = \frac{D}{\Delta t_h}$$

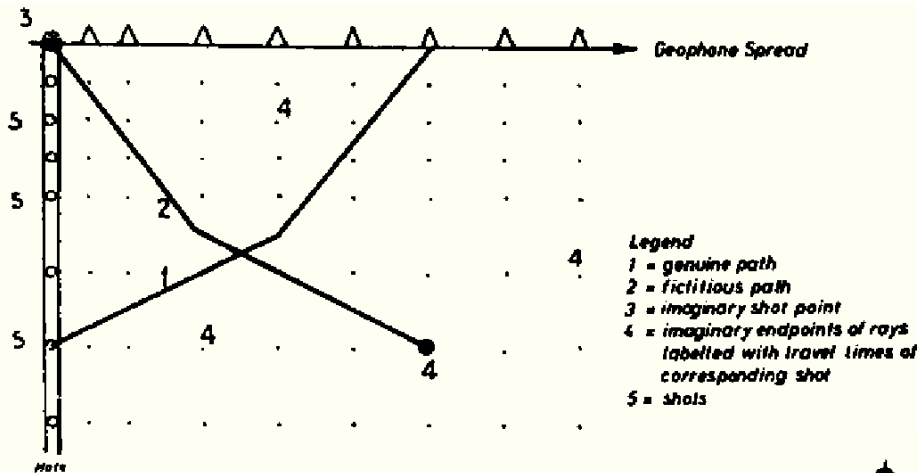
$$V_v = \frac{D}{\Delta t_v}$$



$$V_{PH} = [(1/V_h)^2 + (1/V_v)^2]^{-1/2},$$

$$\gamma = \tan^{-1} [V_v/V_h].$$

# Meisner, 1961



J. Gaiser (1992) used this method to estimate phase slownesses which he inverted for TIV parameters.

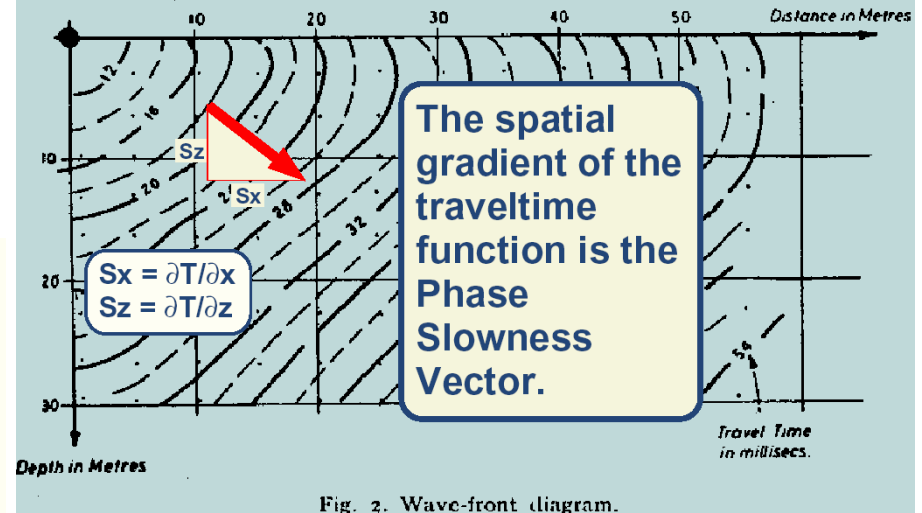


Fig. 2. Wave-front diagram.

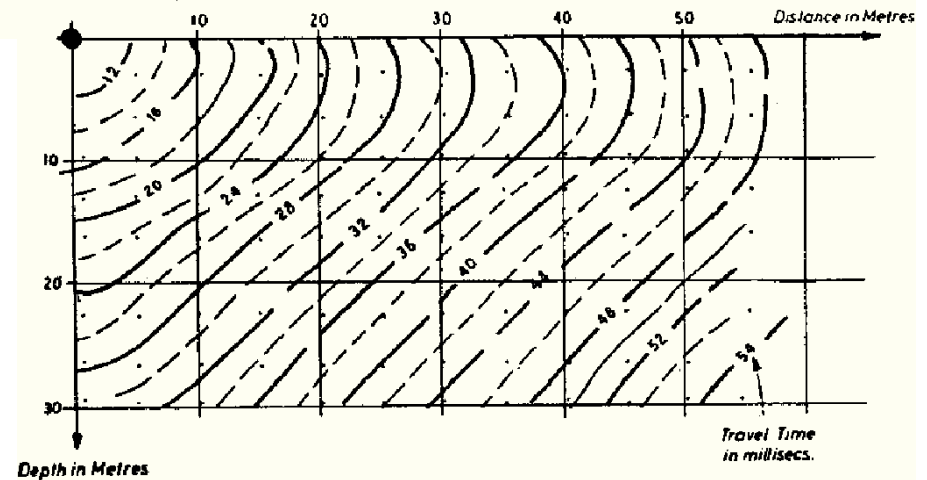
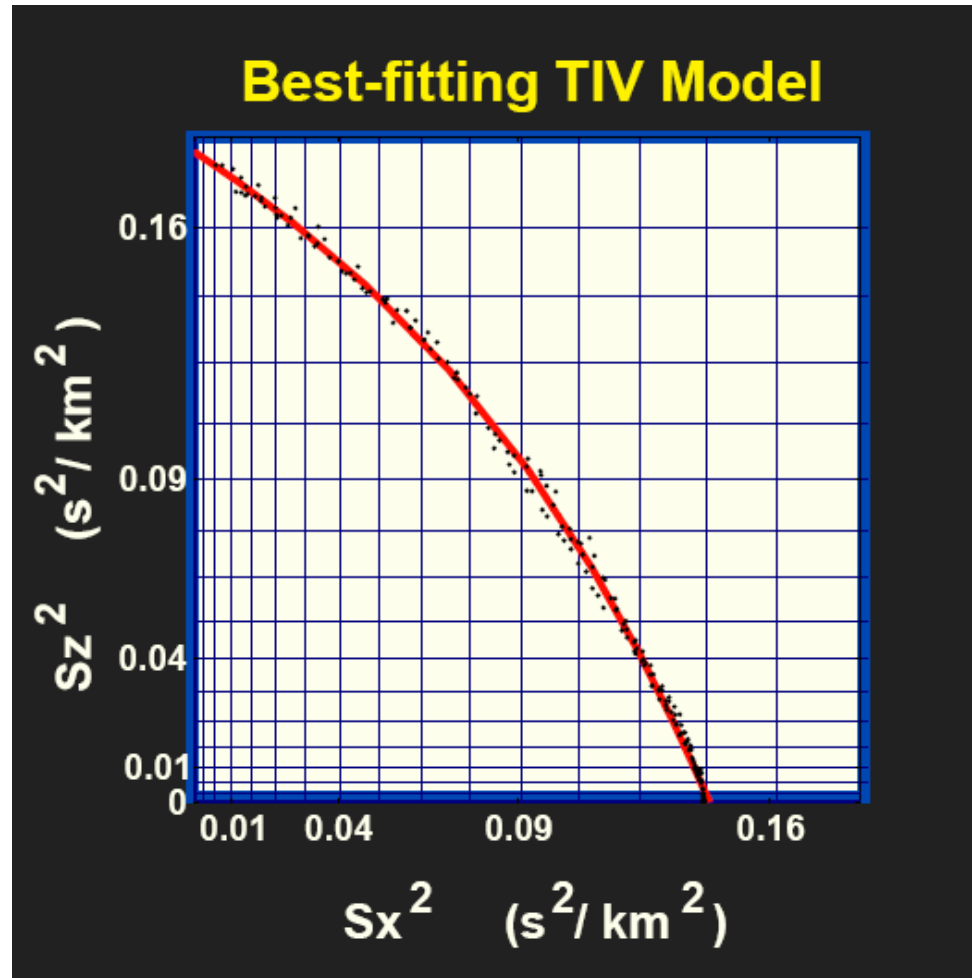
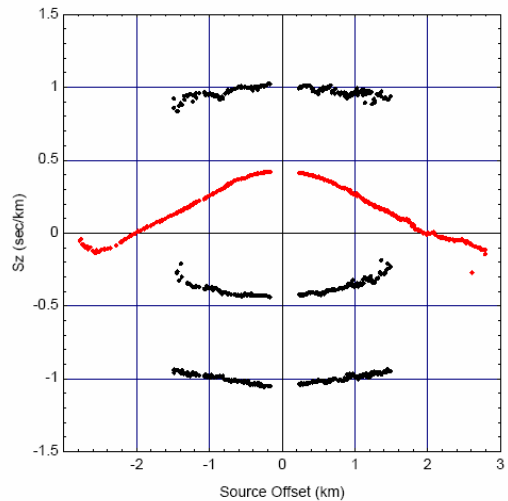
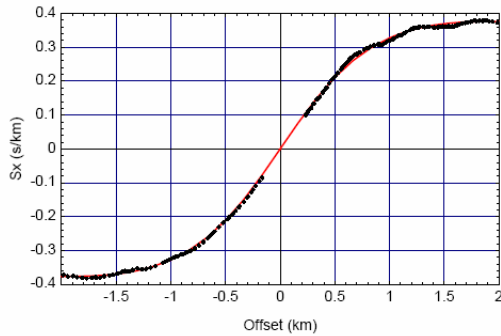


Fig. 2. Wave-front diagram.

# Squared Phase Slowness



N.B.: Isotropy would require a line at  $45^\circ$



# TI Parameters from Phase Slowness:

Let  $X = S_x^2$ ,  $Z = S_z^2$ , and

$$A = A_{11}A_{33} + A_{55}^2 - (A_{13} + A_{55})^2.$$

Assuming a TI medium, the Christoffel relation can be written:

$$A_{11}(A_{55}X^2 - X) + A_{33}(A_{55}Z^2 - Z) + AXZ = A_{55}(X + Z) - 1$$

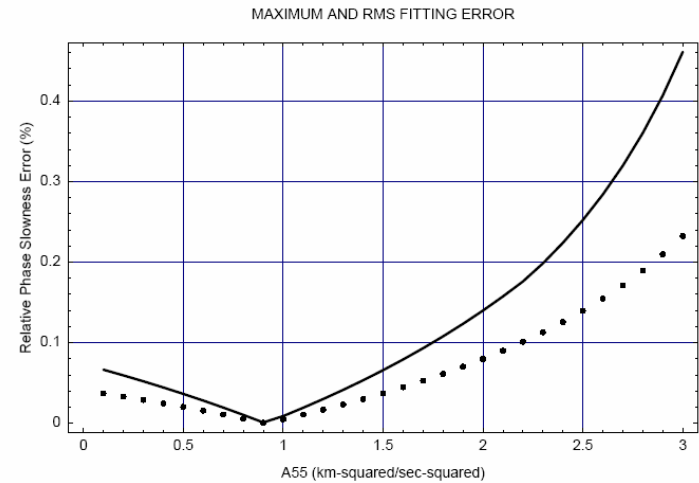
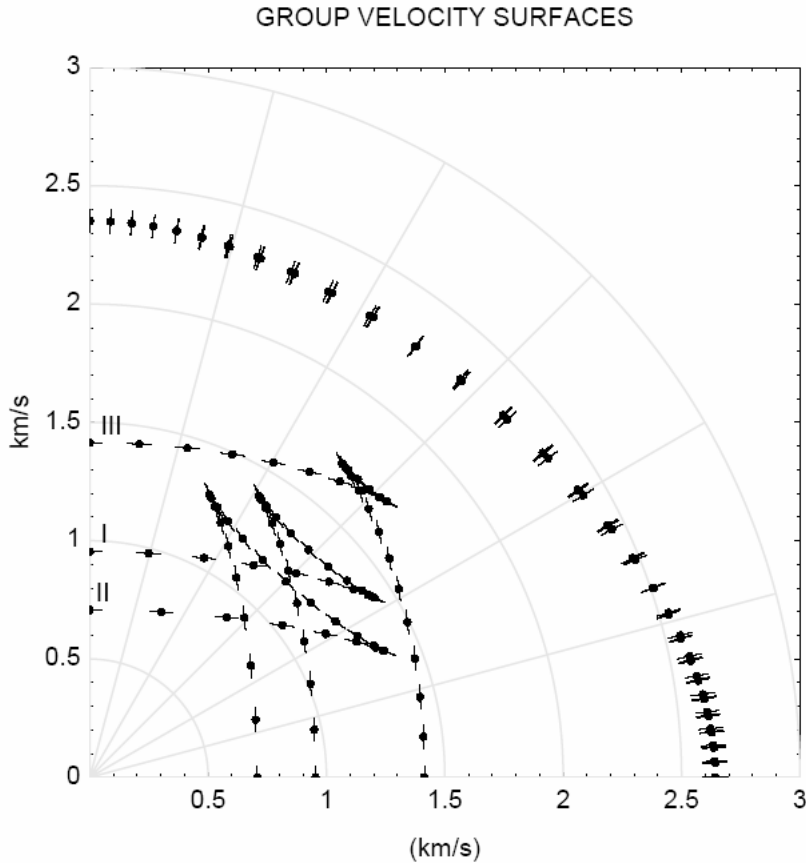
Given data points  $\{X_i, Z_i\}$  and a choice of  $A_{55}$ , the above equation becomes a linear system to be solved for  $A_{11}$ ,  $A_{33}$ , and  $A$ .

$A$  is then solved for  $A_{13}$  assuming  $A_{13} + A_{55} > 0$ :

$$A_{13} = (A_{11}A_{33} + A_{55}^2 - A)^{.5} - A_{55}$$

Question: Can we optimize the fit as a function of  $A_{55}$  to determine all four “sagittal” parameters from qP data only?

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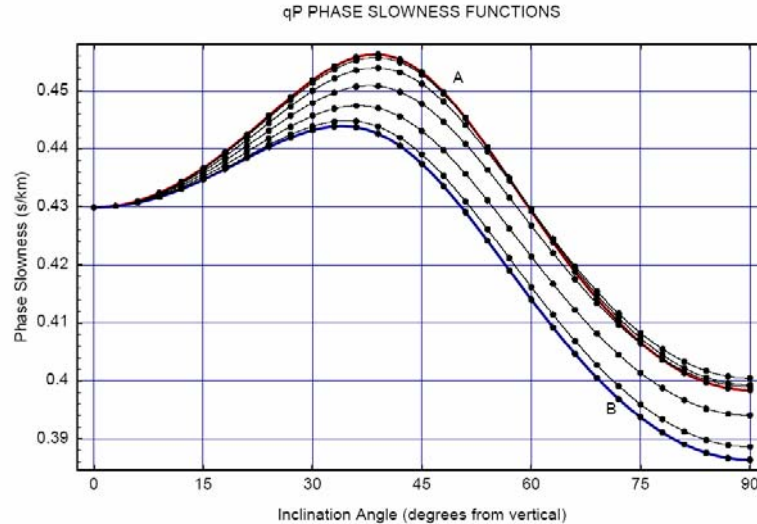
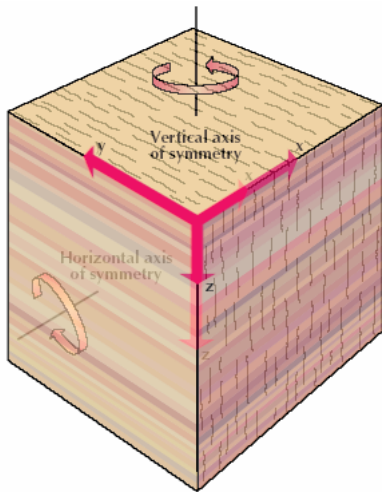


Answer: No

Question: Does a good TI fit to data from a single vertical plane imply that the medium has negligible azimuthal anisotropy?

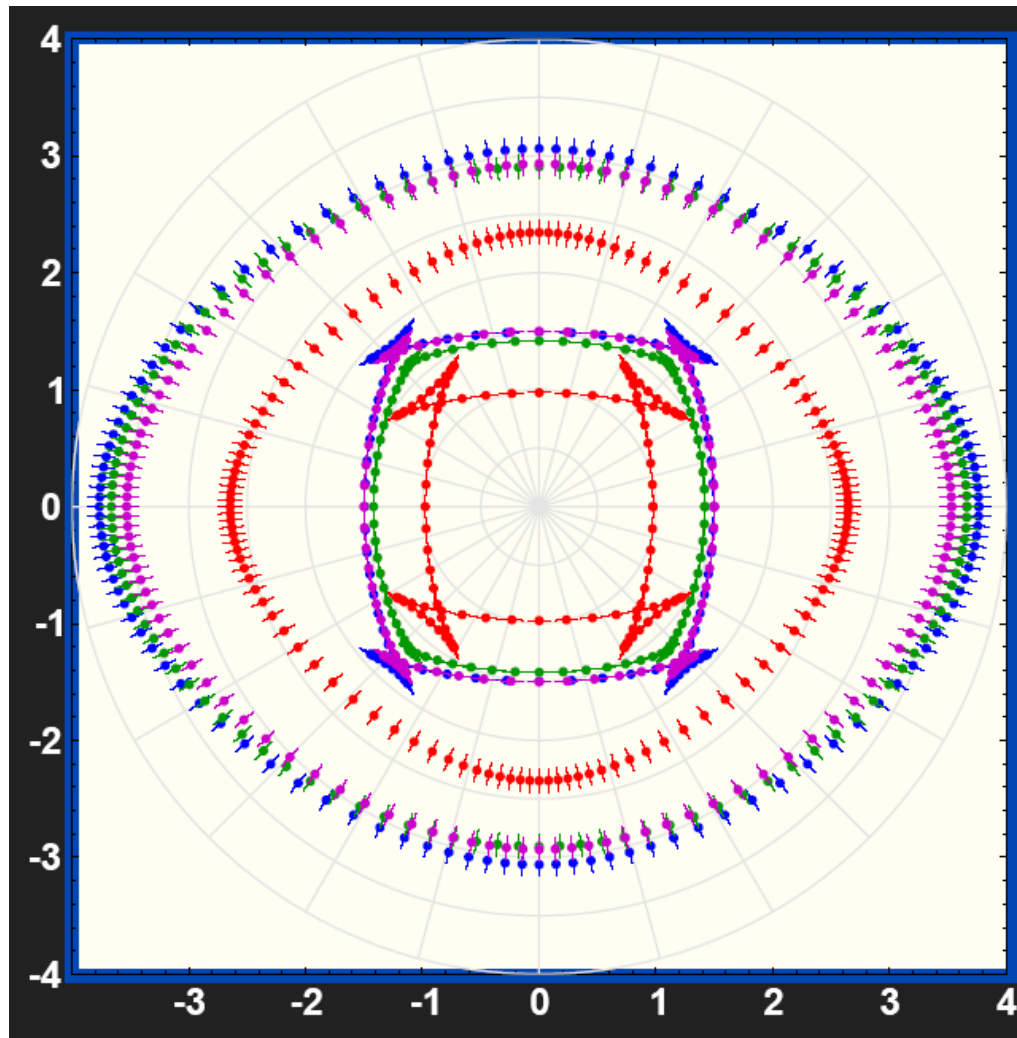
• Fractured TIV

$$\begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \\ \sigma_4 \\ \sigma_5 \\ \sigma_6 \end{bmatrix} = \begin{bmatrix} c_{11} & \frac{c_{13}c_{22}-c_{23}c_{11}}{c_{23}-c_{13}} & c_{13} & & & \\ \frac{c_{13}c_{22}-c_{23}c_{11}}{c_{23}-c_{13}} & c_{22} & c_{23} & & & \\ c_{13} & c_{23} & c_{33} & & & \\ & & & c_{44} & & \\ & & & & c_{55} & \\ & & & & & c_{66} \end{bmatrix} \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \epsilon_3 \\ \epsilon_4 \\ \epsilon_5 \\ \epsilon_6 \end{bmatrix}$$



Answer: No

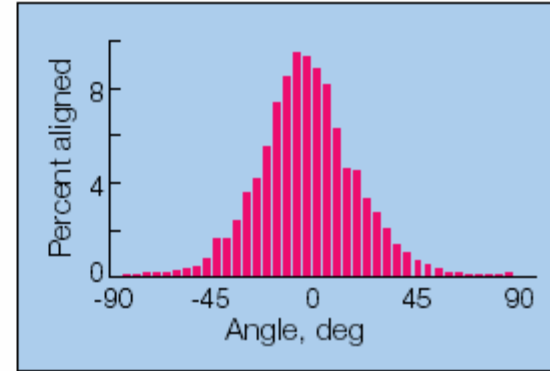
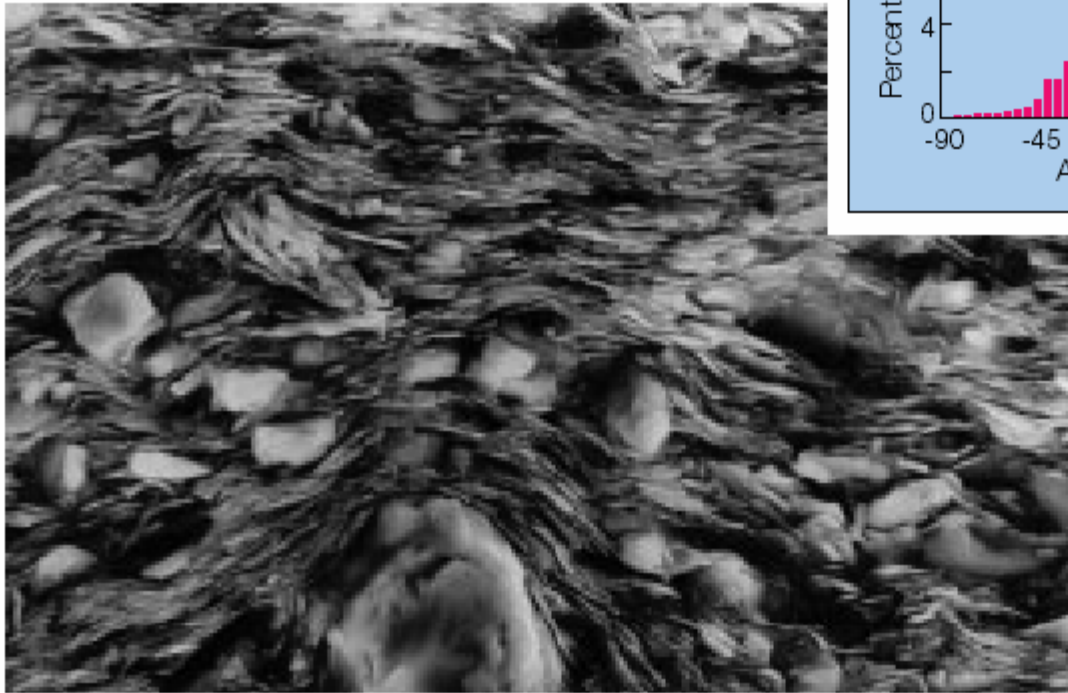
Question: Is this case typical?



- **Petronas (WVSP)**
- **Another WVSP**
- **Del Rio (crosswell)**
- **Greenhorn (core)**

Answer: It is not rare

# Shale Morphology

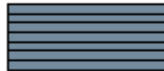


10  $\mu\text{m}$

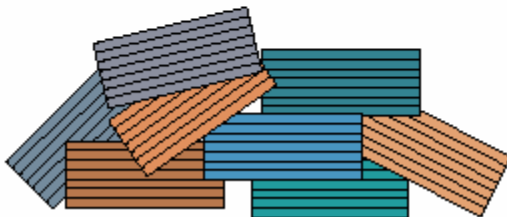
□ *Photomicrograph of shale showing clay platelets distributed around the horizontal. Inset graph shows the distribution of the normal to the platelet, distributed around vertical.*

# Shale Model

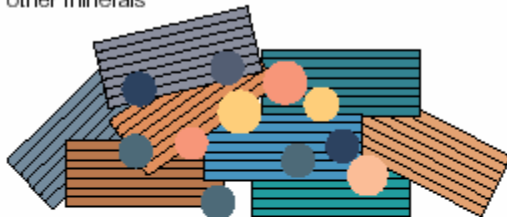
Solve for aligned inclusions of a fluid-clay composite



Average over distribution function

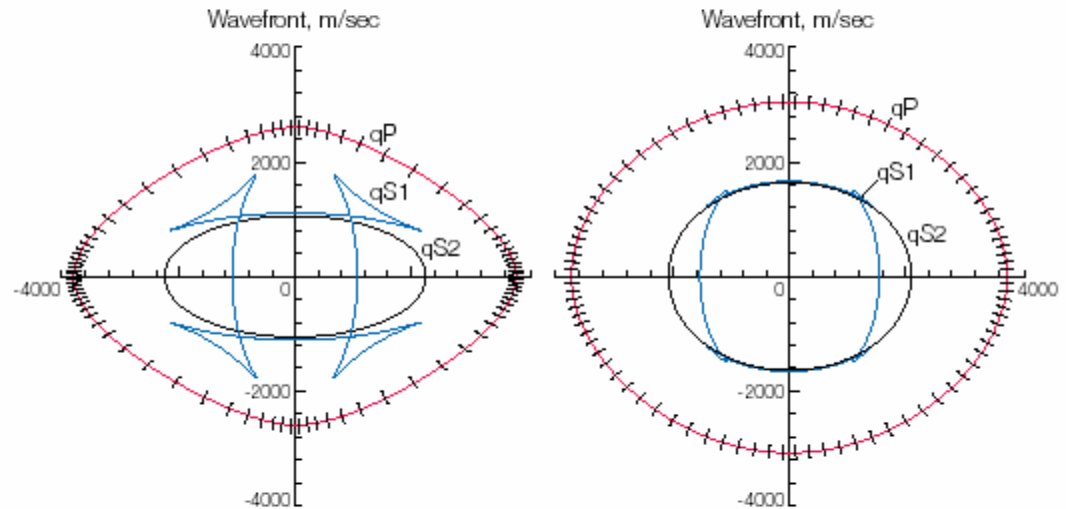


Add silt and other minerals



□ Components of a shale model. Individual model clay platelets (top) are oriented according to the distribution measured in the shale photograph on previous page (middle). Silt particles are added (bottom) to resemble real shales.

N.B.: Think about excess horizontal shear compliance



□ Wavefront velocities for synthetic shales.  $qP$ - and  $qS$ -wave velocities are computed for a shale with all clay platelets oriented horizontally (left). The shale synthesized with a realistic clay platelet distribution shows computed velocities (right) similar to those of the real shale depicted on the previous page.

# Hooke's Law Revisited

To get a unit of pure strain (assuming  $\rho = 1$ ):

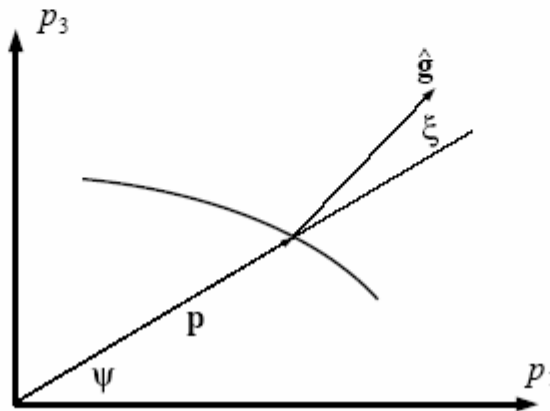
Mode	Direction	Stress
P	$0^\circ$	$A_{11}$
P	$90^\circ$	$A_{33}$
S	$0^\circ$	$A_{55}$
S	$90^\circ$	$A_{55}$
P	$45^\circ$	$.25(A_{11} + A_{33} + 2(A_{13} + 2A_{55}))$
S	$45^\circ$	$.25(A_{11} + A_{33} - 2A_{13})$



# Perturbation Result (Chapman & Pratt, 1992)

$$\begin{aligned} \delta p &\simeq -\frac{1}{2}p^3 \delta a_{ijkl} \hat{p}_i \hat{p}_l \hat{g}_j \hat{g}_k \\ &= -\frac{1}{2}p^3 \{ \hat{p}_1^2 \hat{g}_1^2 \delta A_{11} + 2\hat{p}_1 \hat{p}_3 \hat{g}_1 \hat{g}_3 \delta(A_{13} + 2A_{55}) + \hat{p}_3^2 \hat{g}_3^2 \delta A_{33} \\ &\quad + (\hat{p}_1 \hat{g}_3 - \hat{p}_3 \hat{g}_1)^2 \delta A_{55} \}. \end{aligned}$$

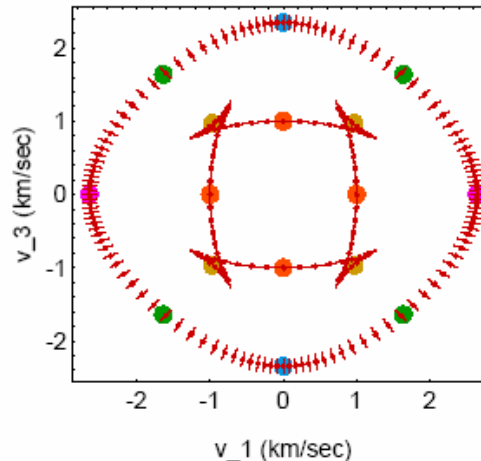
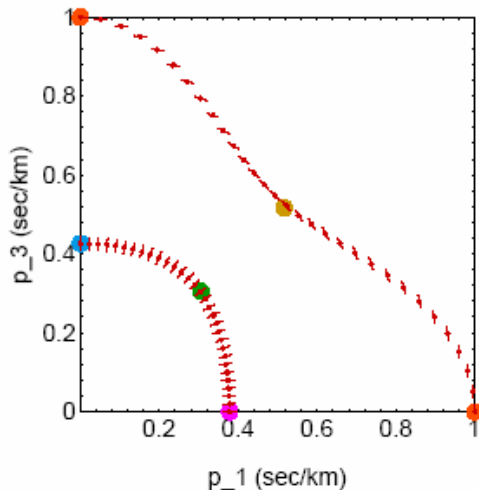
Analyze consequences of setting  $\delta p = 0$  under the approximation that phase and polarization vectors are parallel or orthogonal.



# PushPin Parameters

$P_{0^\circ}$	$A_{11}$
$P_{90^\circ}$	$A_{33}$
$S_{0^\circ}$	$A_{55}$
$S_{90^\circ}$	$A_{55}$
$P_{45^\circ}$	$.25(A_{11} + A_{33} + 2(A_{13} + 2A_{55}))$
$S_{45^\circ}$	$.25(A_{11} + A_{33} - 2A_{13})$

If an arbitrary TI medium is perturbed in a way that preserves a given push-pin, then slowness points in the associated direction and mode will be approximately preserved in the new medium.



# PushPin Parameters

$P_{0^\circ}$	$A_{11}$
$P_{90^\circ}$	$A_{33}$
$S_{0^\circ}$	$A_{55}$
$S_{90^\circ}$	$A_{55}$
$P_{45^\circ}$	$.25(A_{11} + A_{33} + 2(A_{13} + 2A_{55}))$
$S_{45^\circ}$	$.25(A_{11} + A_{33} - 2A_{13})$

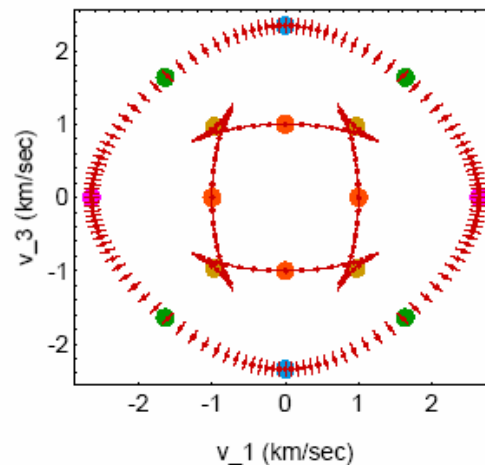
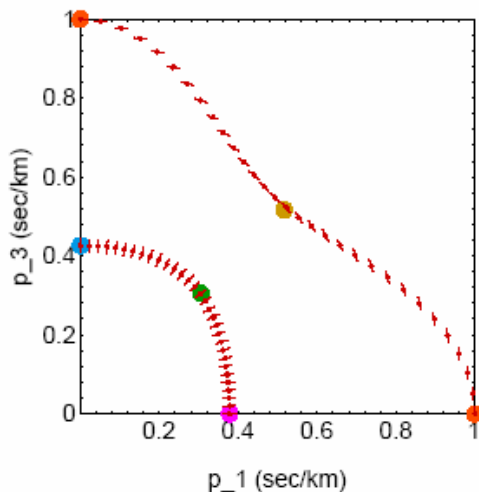
## Thomsen Parameters

$$\varepsilon \equiv \frac{C_{11} - C_{33}}{2C_{33}};$$

$$\gamma \equiv \frac{C_{66} - C_{44}}{2C_{44}};$$

$$\delta \equiv \frac{1}{2} \left[ \varepsilon + \frac{\delta^*}{(1 - \beta_0^2/\alpha_0^2)} \right]$$

$$= \frac{(C_{13} + C_{44})^2 - (C_{33} - C_{44})^2}{2C_{33}(C_{33} - C_{44})}.$$



# TIV-Stressed Isotropic Medium (Bag of Marbles)

$$c_{11} := \lambda + 2\mu + e(2\nu(2\lambda + 3\mu + A + 4B + 2C) - (\lambda + 2B + 2C))$$

$$c_{33} := \lambda + 2\mu + e(2\nu(\lambda + 2B + 2C) - (3\lambda + 6\mu + 2A + 6B + 2C))$$

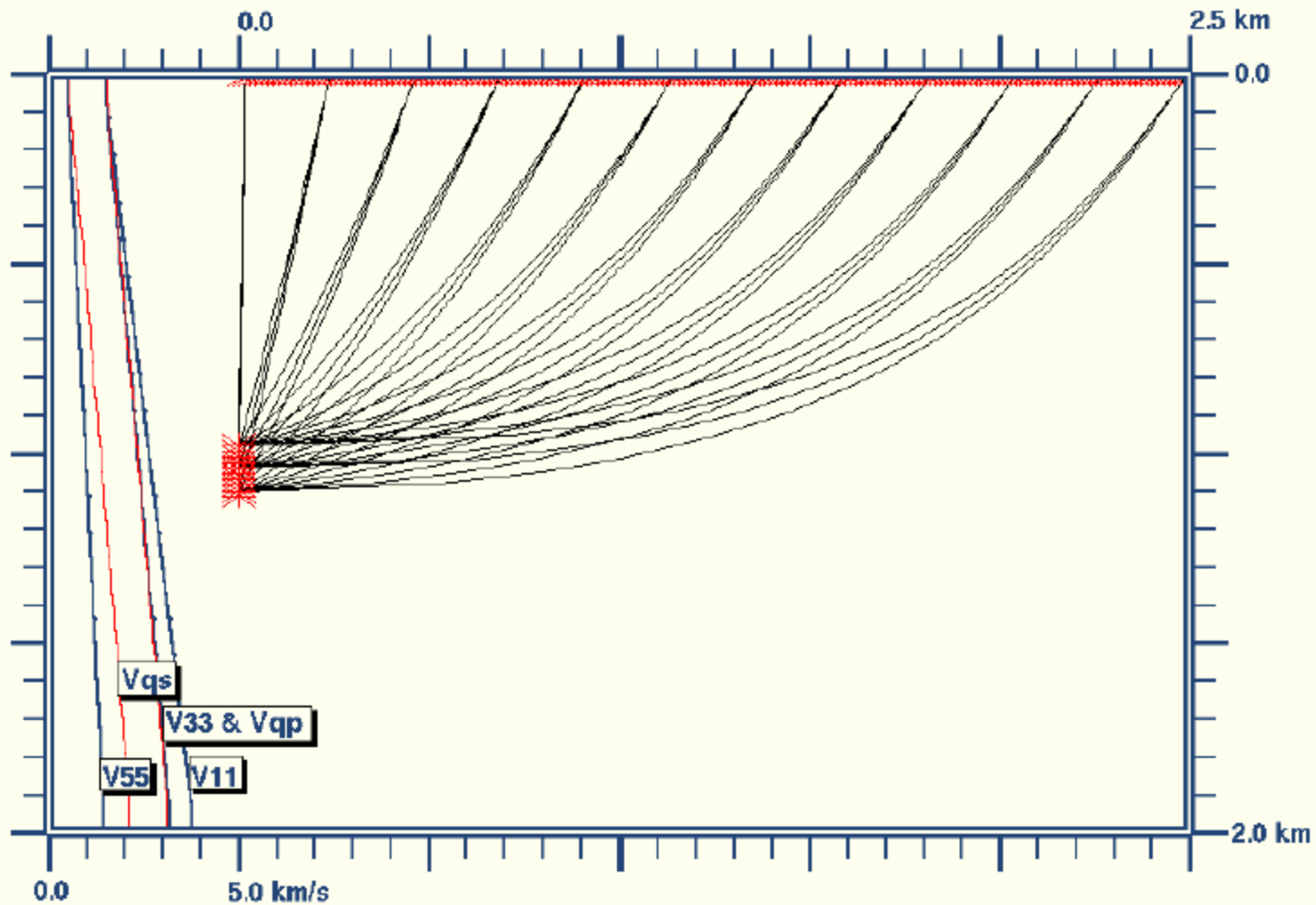
$$c_{55} := \mu + e(2\nu(\lambda + \mu + A/4 + B) - (\lambda + 2\mu + A/2 + B))$$

$$c_{13} := \lambda + \mu + e(\nu(\lambda + \mu + A/2 + 4B + 4C) - (\lambda + \mu + A/2 + 3B + 2C)) - c_{55}$$

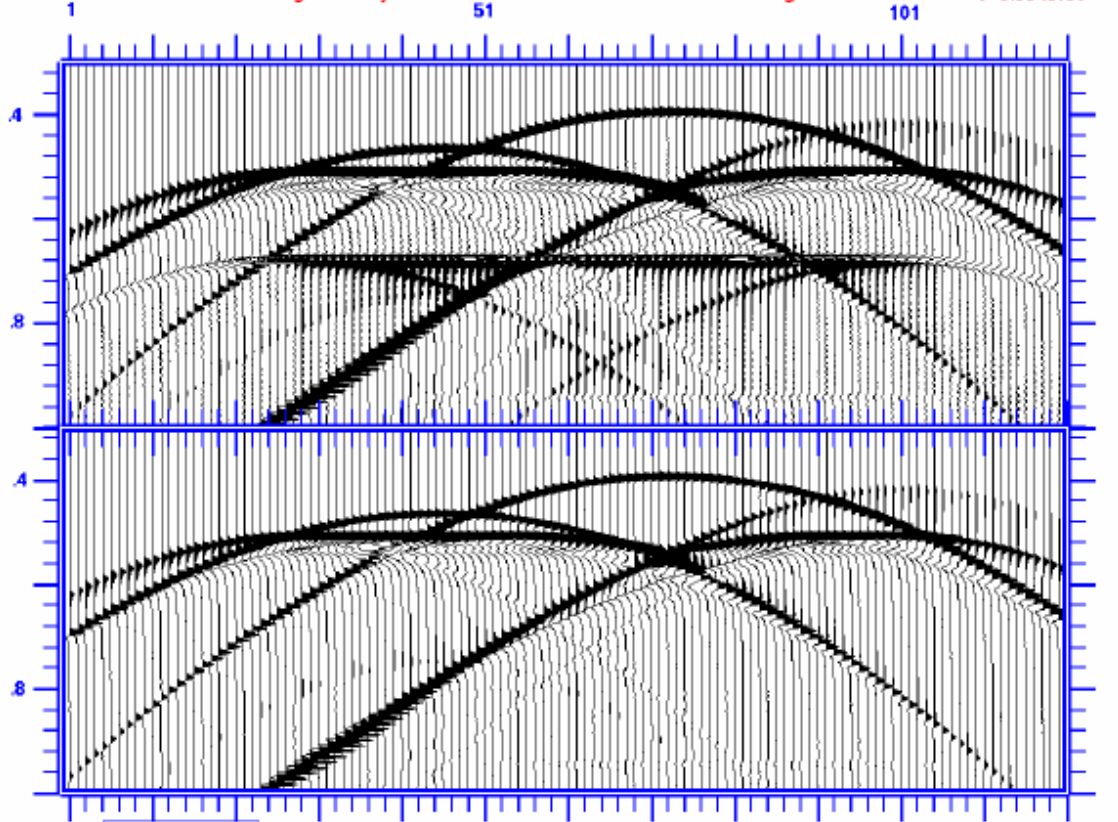
$$c_{66} := \mu + e(2\nu(\lambda + 2\mu + A/2 + B) - (\lambda + B))$$

$$\text{Simplify}[c_{11} + c_{33} - 2(c_{13} + 2c_{55})]$$

0



Coincident source and receiver gather at  $y=1.44$  k/ft  $x=-2.89:10.319:111$  k/ft Triangle Size 60 ft  $V=9.86$  k/ft/s



Born and Kirchhoff seismograms

Schlumberger Cambridge Research

k\_versus\_born.ps

Figure 22: A coincident source and receiver profile over the French model calculated by Born volume integration (top) and Kirchhoff surface integration (bottom).

## 9 TI Zero-offset GRT Migration/Inversion

### 9.1 GRT inversion formula:

$$\langle f(\mathbf{x}_o) \rangle = \frac{1}{\pi^2} \int d^2\xi(\mathbf{s}, \mathbf{x}_o) \frac{|\beta(\mathbf{s}, \mathbf{x}_o)|^3}{A(\mathbf{s}, \mathbf{x}_o)^2} u_{sc}(\mathbf{s}, t = \tau_o).$$

### 9.2 Simplification

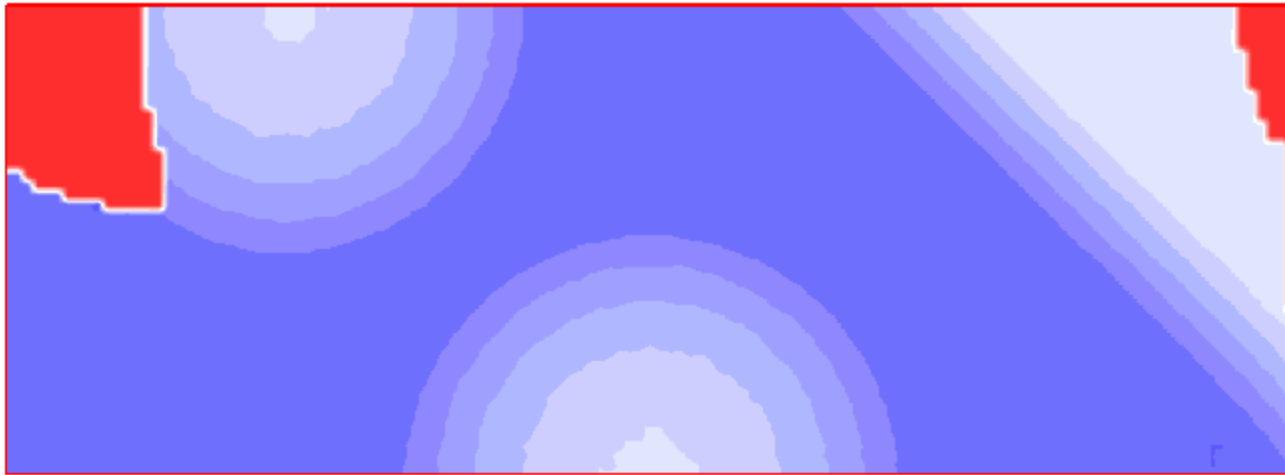
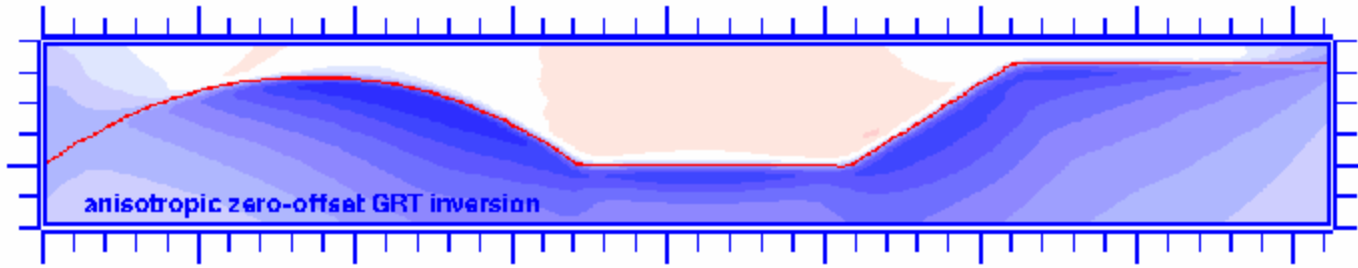
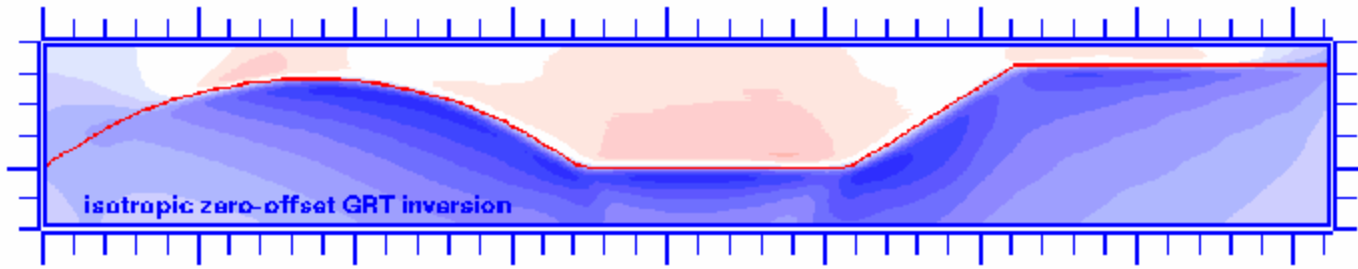
$$d^2\xi \frac{\beta^2}{A^2(\mathbf{s}, \mathbf{x}_o)} = ds_1 ds_2 \cos(\alpha)$$

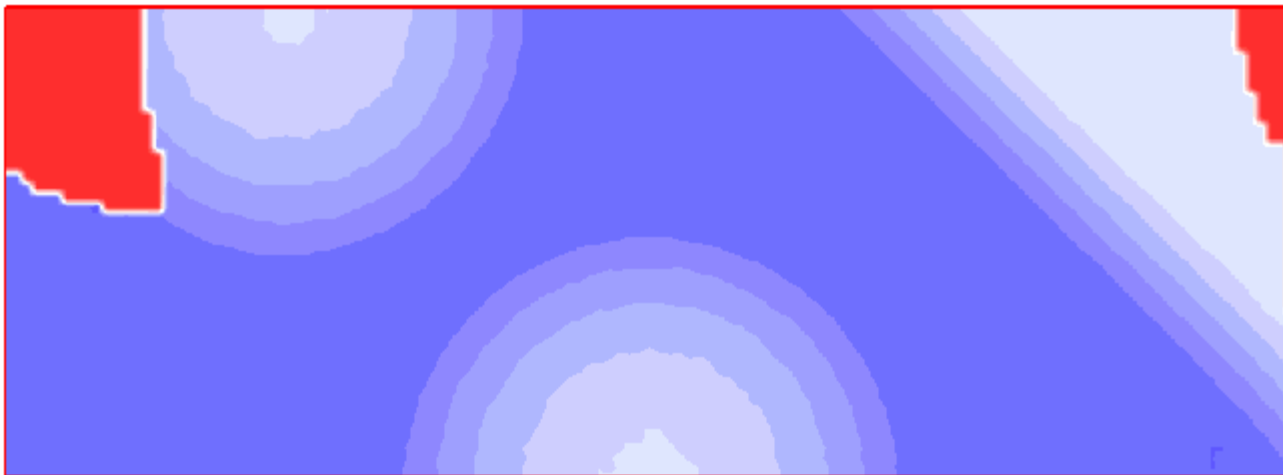
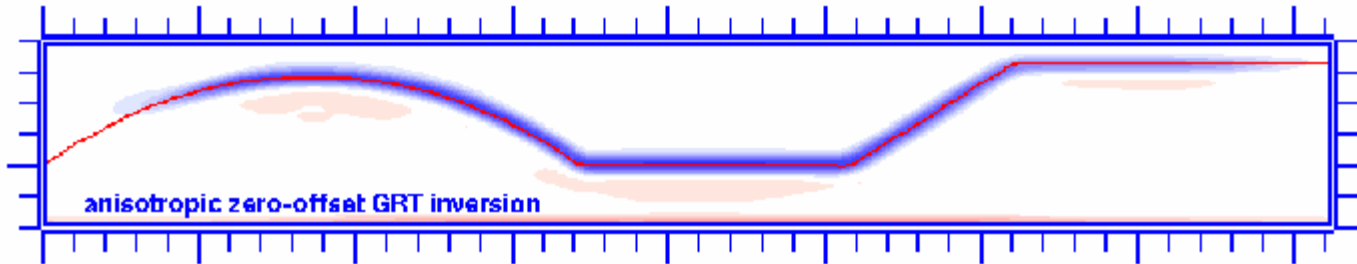
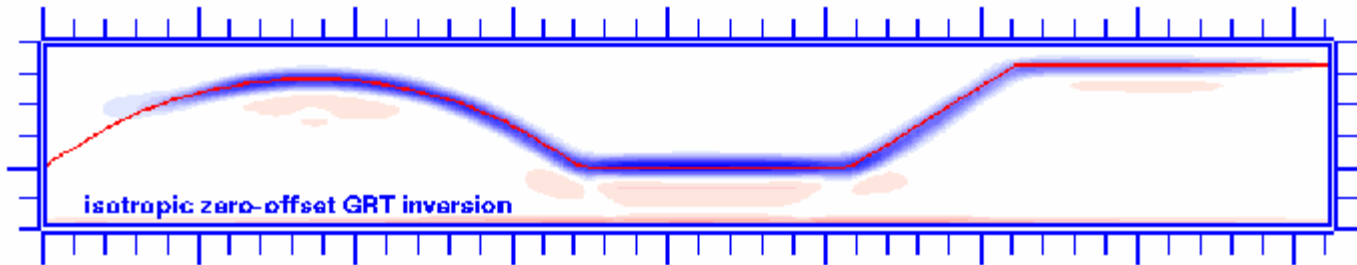
where  $\alpha$  is the vertical phase angle at the surface.

### 9.3 What I Calculated:

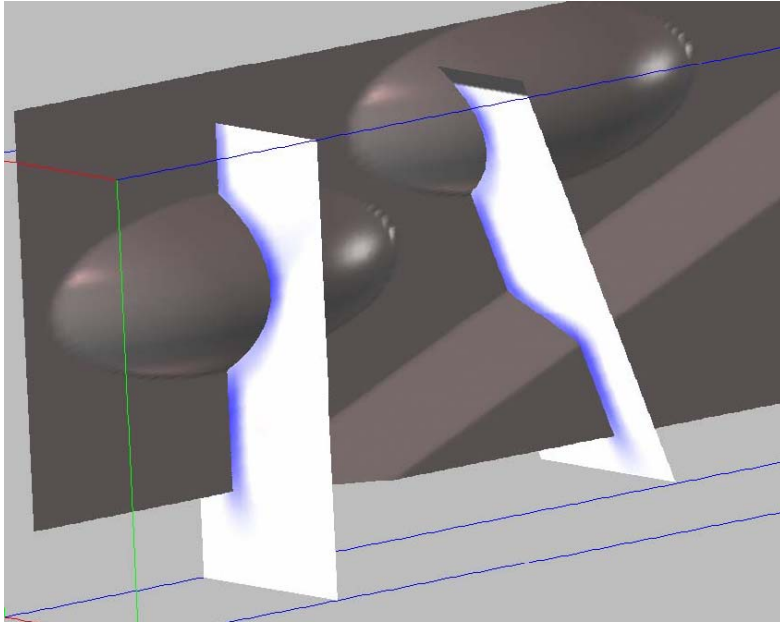
$$\int ds_1 ds_2 \cos(\alpha) |\beta(\mathbf{s}, \mathbf{x}_o)| u_{sc}(\mathbf{s}, t = \tau_o)$$



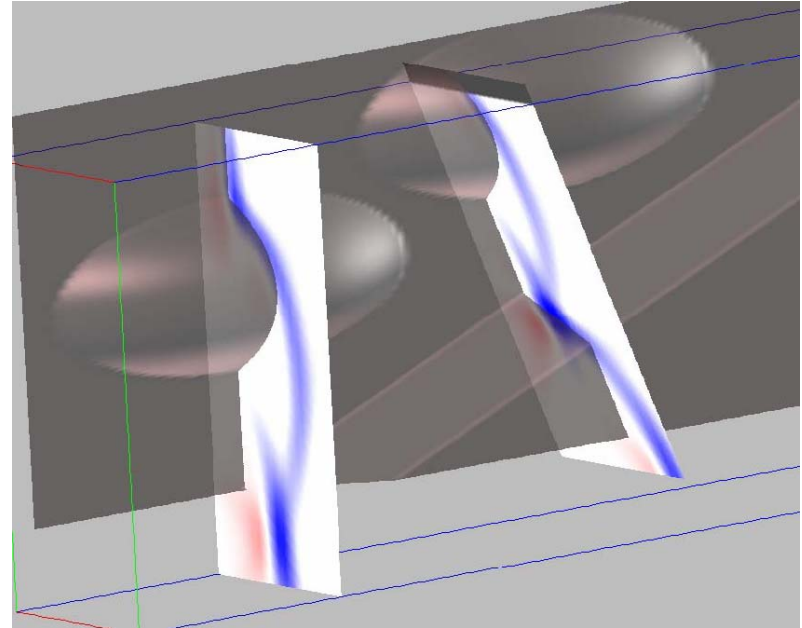




## Turning-ray migration of Vertical Object

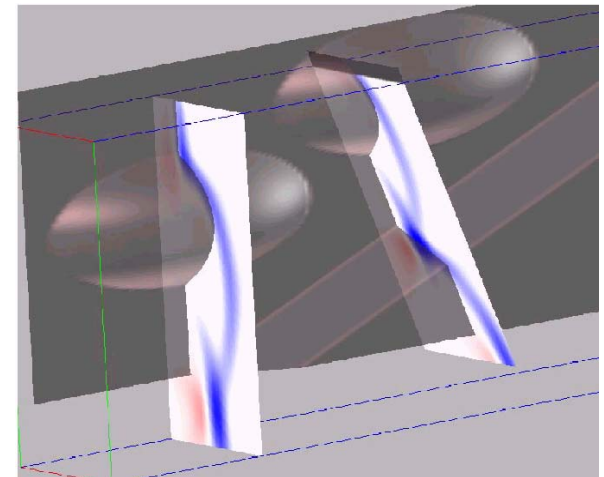
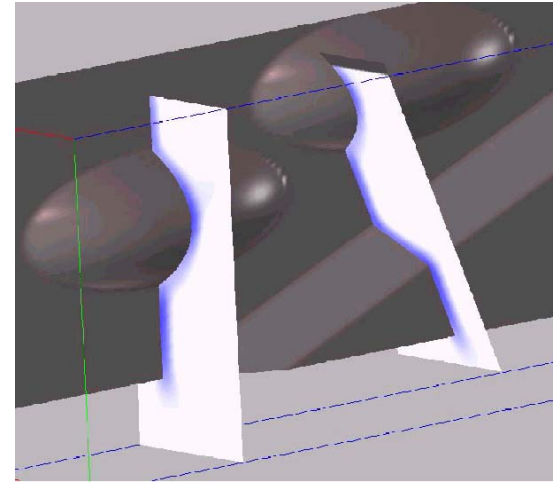
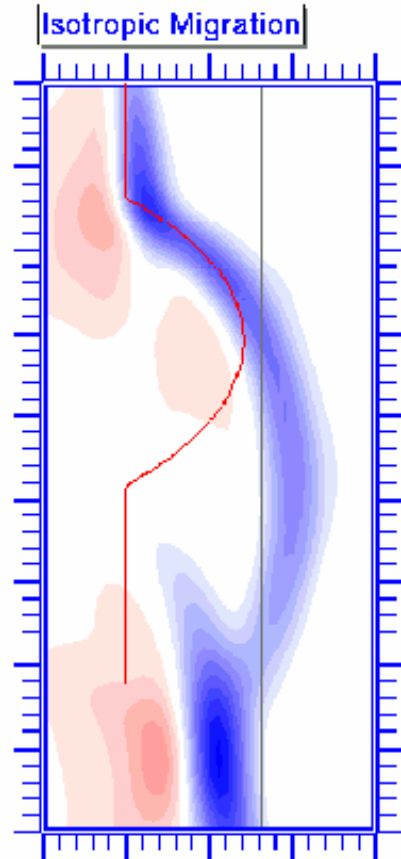
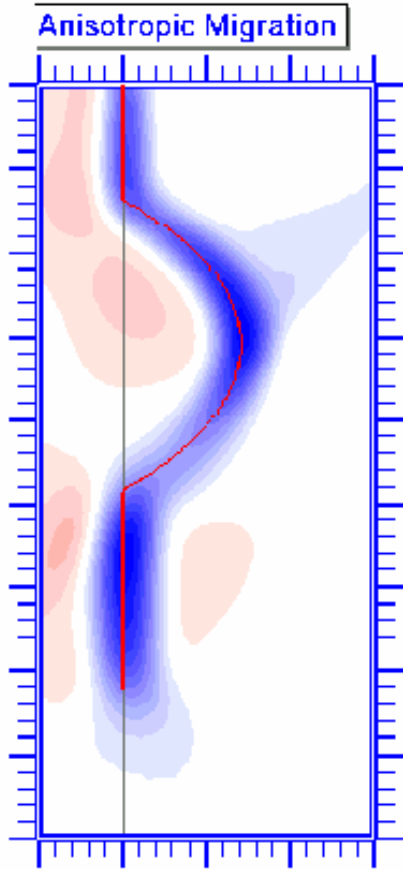


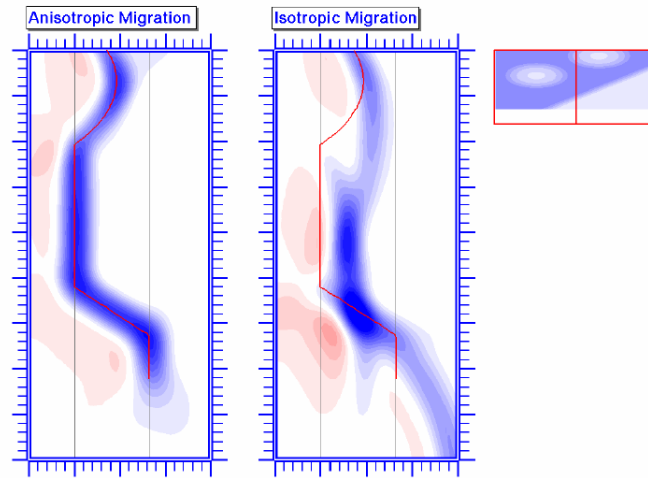
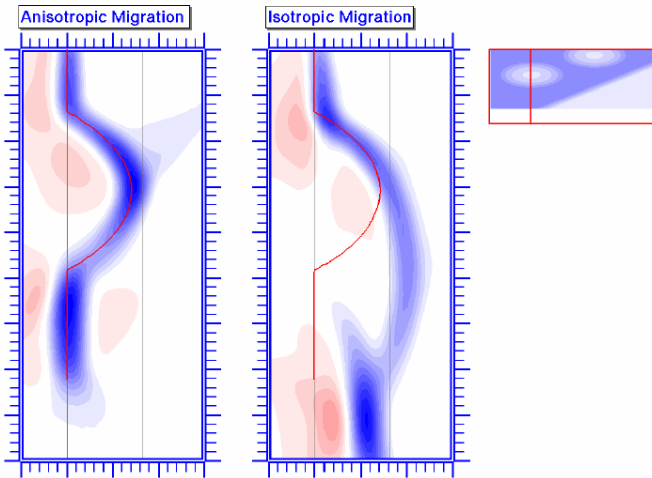
Anisotropic



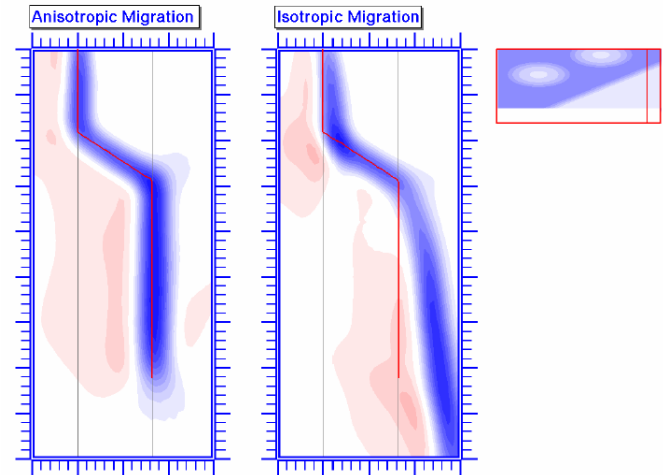
Isotropic  
(vertical velocities)

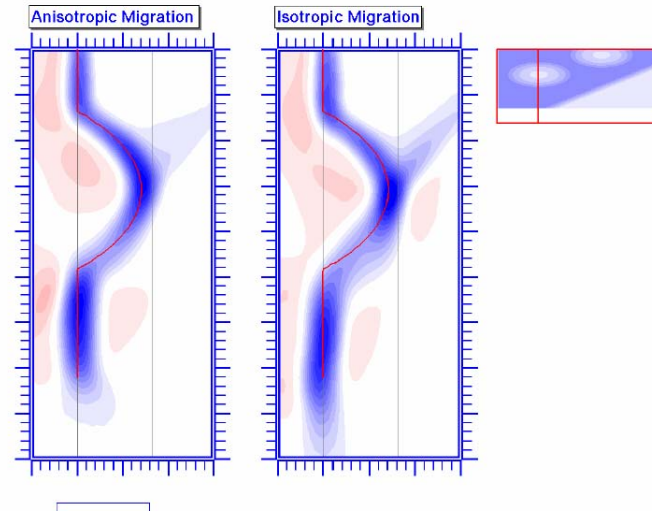
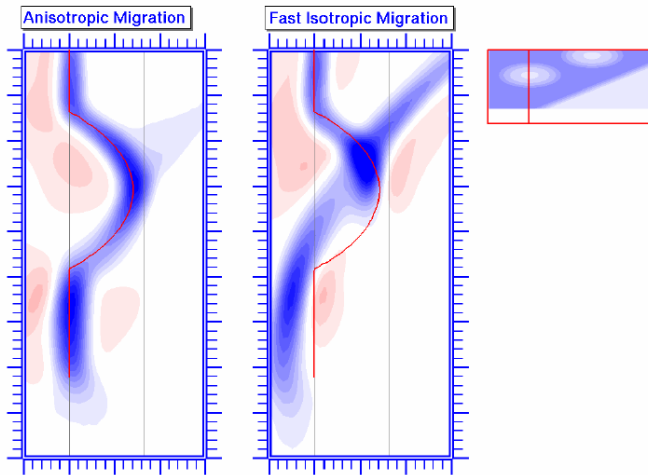
# Turning Ray Images



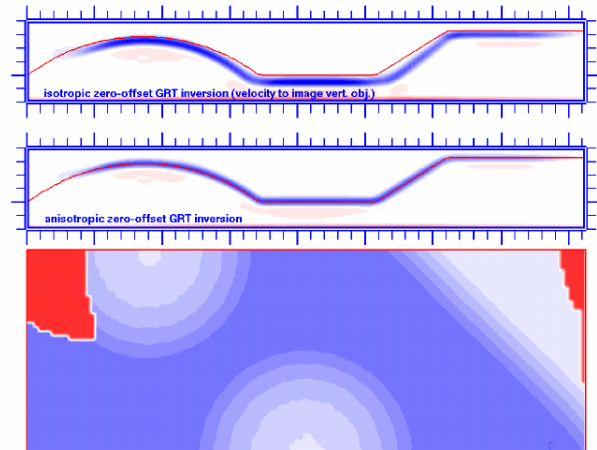


Isotropic Migration using vertical velocity profile systematically defocuses and mislocates vertical object





Isotropic Migration using a velocity profile that focuses the vertical object mislocates the horizontal object.



# Local, interval VTI estimation

Phase method (Gaiser, 1990; Miller and Spencer, 1993)

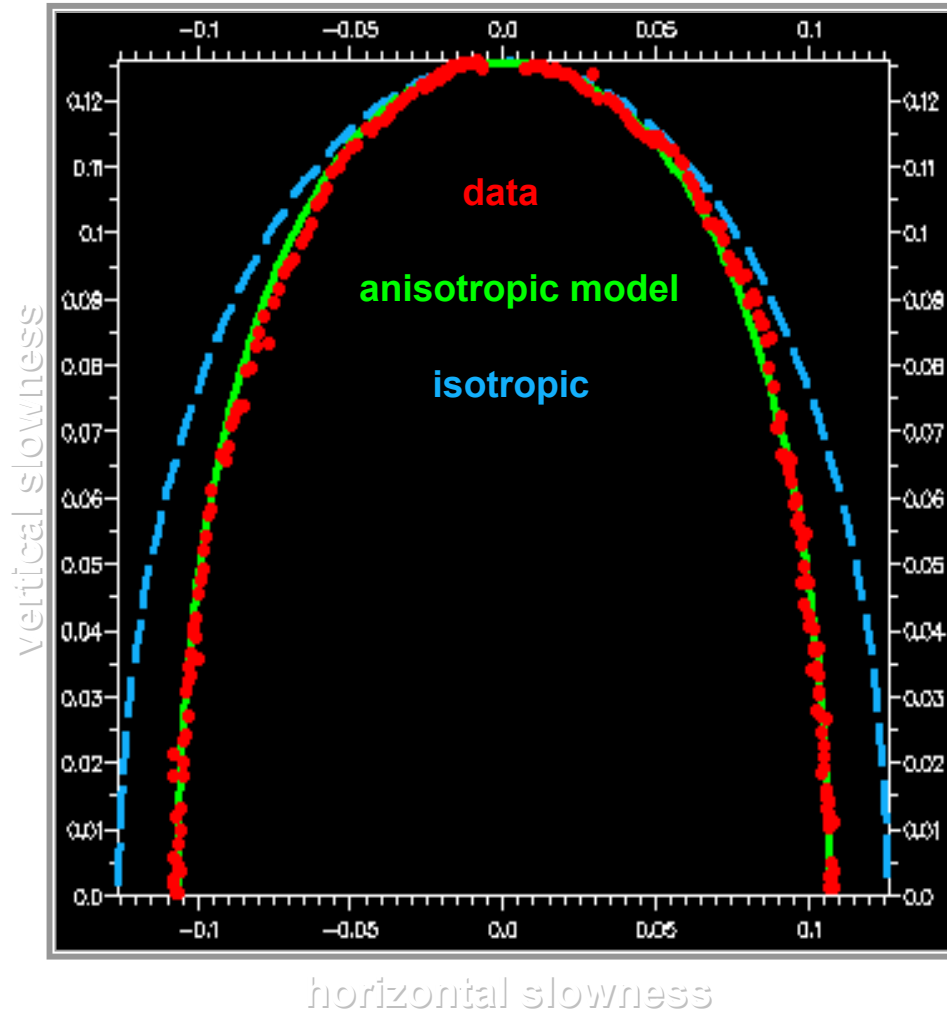
- Vertical and horizontal direct time derivatives yield phase slowness crossplot, fitting yields moduli
- Assumptions about overburden simplicity

Apparent Slowness + polarization method (de Parscau and Nicoletis, 1987; Hsu and Schoenberg, 1989; Horne and Leaney, 2000)

- Extraction of  $S_v$  and reflected parameters required picking
- Parametric waveform inversion (Leaney and Esmersey, 1989) and downhole tools with sufficient vector fidelity have made it a commercially viable method.

# Local VTI anisotropy:

## Phase method



horizontal slowness

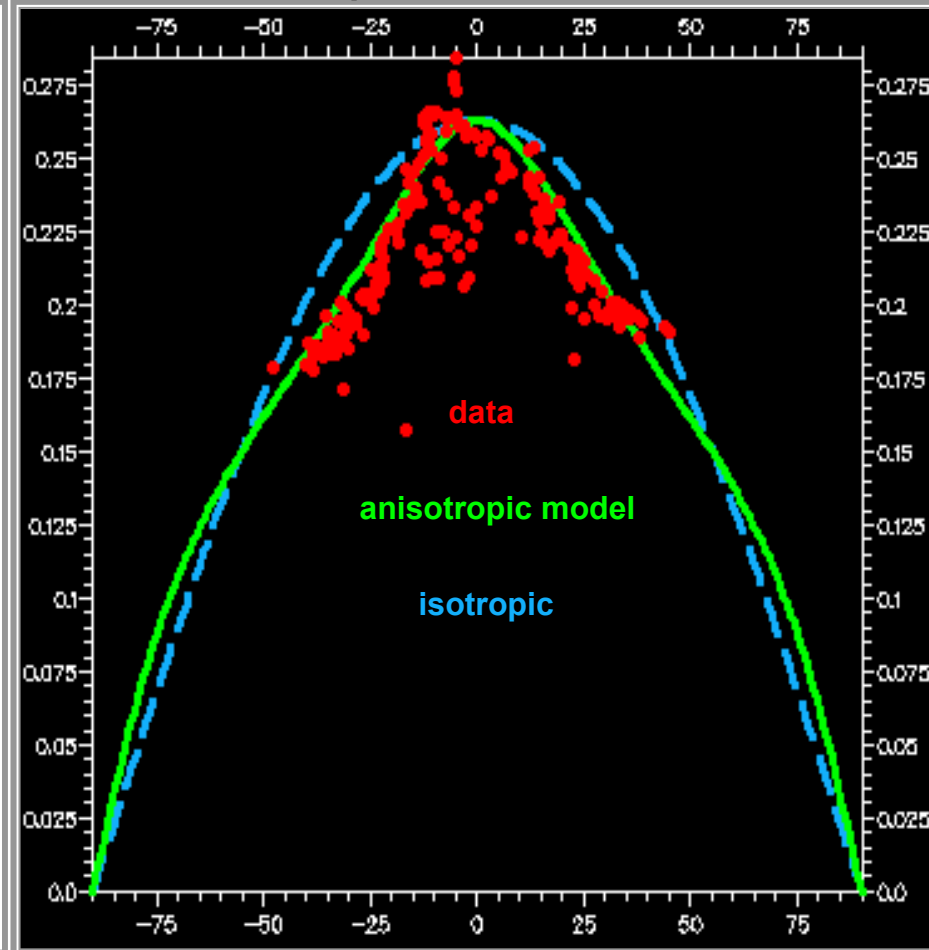
37

DM

21 Oct 05

*Better sensitivity to  $\varepsilon$ , ellip.*

## Slowness+polarization method



polarization

*Better sensitivity to  $\eta$ ,  $\sigma$  anellip.*

Schumberger



# Comparison: phase slowness versus slowness+polarization

